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# NAVAL POSTGRADUATE SCHOOL

## Monterey, California



INITIAL VALIDATION OF AN AMBIENT  
AIR QUALITY MODEL  
FOR  
NAVAL AIR OPERATIONS

by

T. S. Douglas and D. W. Netzer

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NAVAL POSTGRADUATE SCHOOL  
Monterey, California

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was conducted to obtain detailed data over a one-week period. Much of the measured pollution concentration data (including all of the suspended particulate data) was lost due to instrument and measurement technique problems. This severely limited the validation effort. Comparison of model predictions with the limited initial measured concentration data indicated that: (1) predicted CO concentrations were in good agreement with measurement, (2) predicted NOX concentrations from aircraft idle/taxi operations were too low, and (3) predicted total hydrocarbons and particulate concentrations were too high for aircraft idle/taxi operations and too low for environ sources. Model predictions were significantly improved by increasing engine RPM settings to above idle for all modes normally specified as idle. Model validation efforts would be improved if one-half integer stability categories could be measured and used in the model.

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## I. INTRODUCTION

In recent years several mathematical models have been developed to predict the atmospheric dispersion of pollutants emitted from aircraft-related activities at and around airports. These models have used the steady state Gaussian plume formulation. The Gaussian formulation is used because it is adaptable to distances and pollutant travel times associated with airports. An early contract sponsored by the U.S. Environmental Protection Agency (EPA) resulted in a model being developed by the Northern Research and Engineering Corporation (Ref. 1). This model was later modified by GEOMET, Inc. (Ref. 2), and dealt specifically with civilian airport operations. A more recent model has been developed by Argonne National Laboratory (ANL) for the USAF and was termed the Air Quality Assessment Model for Air Force Operations (AQAM) (Ref. 3). This computer model was based upon an earlier TRW model, the Air Quality Display Model (Ref. 4).

Each of the models utilizes a method for solution of diffusion equations assuming Gaussian dispersion in both the horizontal and vertical directions. Gaussian formulation in air quality model calculations requires meteorological inputs including stability of the atmosphere, mixing layer height, and wind direction and speed. Detailed pollution source data are also required. The resultant models consisted of emission and dispersion programs. AQAM included three major parts, a Source Inventory model which yields annual emission at an

activity by source, a Short Term dispersion model which performs hourly-averaged calculations using input dispersion parameters and a Long Term dispersion model. The models predict average steady-state concentrations during the specified time interval over a specified grid surrounding the airport.

Model verifications have to be conducted to test the algorithms and plume dispersion equations. Initial efforts to validate AQAM were begun by the Air Force at Williams AFB, Arizona. Williams AFB was chosen because it was a high traffic-volume, military airfield where accurate statistics would be available. These statistics included aircraft type, mix, and activity schedules from which emissions input data could be calculated (Ref. 5). The objectives of the validation effort were three-fold:

1. Collect a data base of airport-related air quality measurements to evaluate the Air Force AQAM model.
2. Determine the impact (if any) of airport-related activity on local (5 km radius) air quality.
3. Conduct a series of special studies to provide information on horizontal and vertical dispersion to supplement any model revision by ANL (Ref. 6).

The Navy became interested in the Argonne model capabilities relative to Naval Air operations. Under sponsorship of the Naval Air Propulsion Center (NAPC) Trenton, N.J., the Naval Postgraduate School (NPS), Monterey, Ca., obtained copies of both the Source Inventory and the Short Term models of AQAM

for evaluation and adaptation to Navy operations. Upon completion of modifications, a validation effort similar to the one at Williams AFB was planned at NAS Miramar, California.

The Source Inventory Program, as originally received from ANL, computes annual emissions of three types of sources: aircraft, airbase (non-aircraft) and environment (off-airbase). Each of these types is further reduced by geometric configuration to either a point, line or area source. Data are input to the Source Inventory program relative to the type and size of source, location of the emission plume in three-dimensional space and the mass emission rate of each pollutant emitted by the source. The model input is often comprehensive and voluminous, leaving a great margin for possible error. The program calculates annual emissions and provides a qualitative ranking of the contributions to the ambient air pollution of any individual source. It also prepares a data bank containing source characteristics, annual emission rates and temporal distribution activity for utilization by the Short Term program.

The Short Term program receives the above compiled annual results and calculates the dispersion of generated pollutants over a specified receptor grid during a given hour, day and month utilizing average meteorological data input for that hour (Ref. 7). For point and area sources this is accomplished by using initial source dimensions and meteorological stability criteria to project a pseudo-upwind point source. Line sources are generated along the route of travel of the source vehicles.

The Short Term model utilizes a line dispersion theory developed by ANL. The line of finite cross-section is segmented into shorter lines, or "puffs", which are then dispersed from pseudo-upwind line sources in much the same manner as point and area sources (Ref. 3,8).

Principal modifications to AQAM were required by the Navy due to differences in flight operations between the Navy and Air Force. Subroutines were added to AQAM to account for Visual Flight Rule (VFR) approaches including aircraft entry break above the runway, Navy touch-and-go cycles, field carrier landing practices (FCLP), takeoff delays, and hot refueling (refueling of aircraft while engines are operating). Also AQAM was expanded to handle helicopter operations. It should be noted that modifications were only made to subroutines involving aircraft sources. Airbase and environ source data remain relatively consistent from base to base whether Navy, Air Force or civilian. The Short Term portion of AQAM was modified to calculate dispersion of pollutants over 412 grid receptors rather than the Air Force's 312 receptors. This was done so that a larger off airbase area could be included in the analysis. Finally, Navy aircraft engines and fuel types are often different than those of the Air Force and, consequently, aircraft performance data and emissions data had to be input to reflect the changes. A plot routine was also incorporated into AQAM so that predicted pollutant distribution patterns could be more readily observed (Ref. 9).



The aforementioned model verification performed by the Air Force at Williams AFB involved 13 months of continuous air monitoring during the period June 1976 through June 1977. Air quality data were collected at five ground stations and meteorological data were taken routinely at the base weather station. Aircraft operations data and airbase and environ source information were then input to AQAM and predicted values of pollutant concentrations were compared with observed, or measured data from the monitoring stations. Preliminary results have indicated that a reasonable correlation exists between predicted and observed hourly pollutant levels (Ref. 10).

The Air Force effort included a wide range of meteorological conditions collected over a long period of time. It was decided to concentrate the Navy validation effort on a specific meteorological "window" which would be reasonably stable for several days and which would occur when a large amount of aircraft activity occurred. The latter was necessary in order to minimize the problem inherent with high background pollution levels. Specifically, it was desired to perform the validation effort at NAS Miramar, CA and to obtain more detailed data relative to (1) aircraft taxi and refueling operations, (2) hourly aircraft flight activity, and (3) meteorology.

Once the Navy modifications were completed and input data were obtained for NAS Miramar, it was necessary to determine

the sensitivity of the model predictions to the input meteorological and operational conditions and to certain dispersion model parameters. An initial model sensitivity study was performed using the Navy version of AQAM and 1975 activity at NAS Miramar as a representative data base (Ref. 9).

The purposes of the present study were (1) to update the data in the Source Inventory program of AQAM in order to represent 1978/1979 operations at NAS Miramar and (2) to compare the predicted and measured levels of pollutant concentrations for the purpose of validating the Short Term program of AQAM. A necessary component of the validation effort was the conducting of an updated model prediction sensitivity study.

## II. OVERALL MODEL VALIDATION EFFORT

The Navy version of the AQAM model validation effort was initiated by the Naval Air Propulsion Center (NAPC). NAPC provided the funding and necessary program coordination as well as technical assistance in selection of the monitoring site locations and the required data acquisition. NAS Miramar was chosen because it had the largest number of flight operations of any NAS and because it had been used in previous work performed by the Naval Postgraduate School in developing the Navy version of AQAM.

The overall objectives of the NAPC program were to:

- a. validate the AQAM model,
- b. document the effects of aircraft operations on air quality, and



- c. assess the possibility of using AQAM (as an alternative to an expensive monitoring program) to determine the effects of aircraft operations on air quality at other NASs (Ref. 11).

The program was divided into two related parts. The first part was to consist of a one year continuous monitoring study. In late 1979 - early 1980 air quality was being measured 24 hours a day using an automated data acquisition system. This effort was directed primarily at objective (b) noted above. The second part was to consist of two special studies, each one-week in duration. The latter studies were to be intensive in nature with detailed operational, meteorological and pollution concentration data being collected. These studies were to be directed primarily at objectives (a) and (c) above. The first special study took place in August 1979 and data received from that week were used in the model validation discussed herein. The second special study was scheduled for the spring of 1980 but was subsequently cancelled. The two periods were chosen to occur during distinctly different meteorological conditions, especially lid height and stability category. Organizations involved in the special study and individual responsibilities of each included:

- a. Northrup Services Incorporated (NSI) contracted by EPA: Air quality monitoring and data reduction to provide hourly averaged pollutant levels.
- b. Pacific Missile Test Center (PMTTC): Meteorological measurements and data reduction to provide hourly

averaged weather conditions throughout the receptor grid.

- c. NAPC/NPS: Aircraft activity monitoring.
- d. NPS: Reduction of aircraft activity data for input into AQAM, model predictions using items b. and c. above, and comparison of predictions with measured values.

### III. NAS MIRAMAR INTENSIVE DATA ACQUISITION

Planning the special study for validation of AQAM began with identifying both the emittants to be monitored to best characterize dispersion and, as previously mentioned, locating appropriate monitoring stations.

The major pollutants in aircraft engine exhausts include particulates/smoke (PT), carbon monoxide (CO), unburned hydrocarbons (HC) and oxides of nitrogen (NOX). The relative amounts emitted depend primarily upon the engine thrust setting. In addition, sulfur oxide emissions (SOX) are often significant from industrial and domestic furnaces. Therefore, CO, HC, NOX, PT and SOX were selected as the pollutants to characterize emissions of both aircraft and airbase related activity. Figure 1 identifies the grid system used to locate the receptors in AQAM. The grid spacing was 1 km. and the x-y coordinates varied from (0,0) to (24,15) representing 400 separate receptor locations.



Locating measuring stations where continuous-air-monitoring instruments would be placed was of prime importance in the validation effort. The behavior of the model predictions at a particular receptor will depend to a great extent on its location relative to numerous sources throughout the receptor grid, especially those located upwind. To validate the model, it was important to compare air quality samples at locations where the airbase and aircraft contributions were large relative to background levels of pollution. Ultimate placement of the stations assumed a dominant wind from the WNW (292°) as advised by PMTC.

Up to 12 special receptor locations can be input to the Short Term program. Special receptor locations were assigned to each of the four pollution monitoring stations as indicated in Table I. They are also identified in Figure 1.

TABLE I  
MONITORING STATION LOCATIONS

TRAILER NUMBER	GRID COORDINATES	SPECIAL RECEPTOR NUMBER IN AQAM
1	10.01, 8.24	401
2	10.52, 8.46	402
3	11.24, 8.35	406
4	12.82, 7.31	410

The intended use of trailer 1 was to determine background levels of pollution upwind of aircraft/airbase sources. Trailer 2 was located just downwind of the hot refueling site.

Trailer 3 was situated just upwind of the hot refueling pits. It was also downwind of the hot refueling area. Trailer 4 was located well downwind at the outer boundary of NAS Miramar.

During the planning stage, NSI made equipment preparations for each trailer site for the air quality monitoring experiment. PMTC analyzed the meteorological history for the San Diego area to determine the best time period for the special study. Optimum weather conditions for validation were considered to consist of a moderate wind coming from the 290 degree direction, a Turner stability category of 2-3, and a moderate lid height (mixing layer depth) of 400-500 meters. It was desirable to have relatively constant weather conditions for the week of intensive data acquisition. This would allow the dispersion model to be validated with multiple tests in which aircraft operations varied but weather remained approximately fixed. The week of 1-7 August 1979 was chosen as the most feasible for meeting these objectives for the first intensive study.

Operating procedures for the week proceeded on a previously planned routine. Specific tasks performed by NSI (pollution monitoring) and PMTC (meteorological monitoring) will be presented by those activities under separate cover. NPS and NAPC personnel monitored the detailed aircraft activity in accordance with the time schedule listed in Table II.



TABLE II  
AIRCRAFT ACTIVITY MONITORING TIMES (LOCAL)

1 AUG	1300 - 1600
2 AUG	1000 - 1230 1400 - 1700
3 AUG	0800 - 1230
6 AUG	0900 - 1230 1330 - 1630
7 AUG	0830 - 1100 1330 - 1630

Observation of aircraft activity was performed/recorded from three locations -- the control tower, the hot refueling site (octagon) and the refueling pits.

The functions performed in the control tower involved (1) timing the sequences of every aircraft on departure from initial startup to takeoff, (2) timing the sequences of every aircraft on recovery from entry into the airport traffic area (defined here as having a three-mile radius) to landing and taxi to the refueling area. Also, the parking areas and taxiways used by each aircraft and the type of landing performed (VFR, IFR) were monitored. Data sheets used to record the aircraft activities observed from the control tower are presented in figures 2 and 3.

Data collected at the hot refueling sites (octagon) and refueling pits included time-in-mode, amount of fuel taken, and aircraft type (see data sheets in figures 4 and 5).



TAKEOFF DATA SHEET

DUTY RUNWAY \_\_\_\_\_ WIND \_\_\_\_\_ TIME \_\_\_\_\_

register/time

Side number \_\_\_\_\_ Aircraft type \_\_\_\_\_

Parking area \_\_\_\_\_

Commence sequence 0/0

Start complete \_\_\_\_\_ / \_\_\_\_\_

Taxi complete \_\_\_\_\_ / \_\_\_\_\_  
(holding at runway)  
(engine check complete)

Takeoff complete \_\_\_\_\_ / \_\_\_\_\_

EVOLUTION (check one)

Takeoff and depart area \_\_\_\_\_

FCLP \_\_\_\_\_ number \_\_\_\_\_

Touch and go \_\_\_\_\_ number \_\_\_\_\_

FIGURE 2

LANDING DATA SHEET  
(full stop landings only)

DUTY RUNWAY \_\_\_\_\_ WIND \_\_\_\_\_ TIME \_\_\_\_\_

register/time

Side number \_\_\_\_\_ Aircraft type \_\_\_\_\_

Commence sequence \_\_\_\_\_ 0/0  
(enter break or 3 mi. on IFR approach)

Landing complete \_\_\_\_\_  
(clear of runway)

Taxi complete \_\_\_\_\_  
(pits/hot refuel holding area)

Fuel commence \_\_\_\_\_  
(enter pits/hot refuel area)

Fuel complete \_\_\_\_\_  
(depart pits/hot refuel area)

Shutdown \_\_\_\_\_

Parking area \_\_\_\_\_  
(hot refuel aircraft only)

FIGURE 3

HOT REFUEL SEQUENCE DATA SHEET  
(OCTAGON)

TIME \_\_\_\_\_

A/C Type (circle one)

Side number \_\_\_\_\_

Arrival time  
at  
holding area \_\_\_\_\_

Arrival time  
into  
octagon \_\_\_\_\_

Departure time  
from  
octagon \_\_\_\_\_

Pounds fuel  
received \_\_\_\_\_

Fuel spilled yes/no

F-4  
F-5  
F-8  
F-14  
A-4  
E-2  
Transient

FIGURE 4

PIT REFUEL SEQUENCE DATA SHEET

TIME \_\_\_\_\_

A/C Type (circle one)

Side number \_\_\_\_\_

Arrival time  
at  
holding area \_\_\_\_\_

Arrival time  
into  
refuel pit \_\_\_\_\_

F-4  
F-5  
F-8  
F-14  
A-4  
E-2  
Transient

Shutdown

(circle one)

Hot refuel

Pounds fuel  
received \_\_\_\_\_

Fuel spilled yes/no

Departure time  
from  
refuel pit \_\_\_\_\_

Pounds fuel  
received \_\_\_\_\_

Fuel spilled yes/no

FIGURE 5

The aircraft/airbase operational data that were collected were used as input to the Source Inventory program. Air quality measurements (by NSI) and meteorological data (by PMTC) were also being collected during the entire period of observation.

#### IV. AQAM MODIFICATIONS AND SENSITIVITY STUDY

##### A. MODEL MODIFICATIONS

In order to perform a model validation, the data input to the Source Inventory program must reflect, as closely as possible, conditions and emittant sources as they exist at the time of validation. Therefore, one of the purposes of this study was to update the data in AQAM to represent 1978/1979 operations at NAS Miramar.

Changes made to the input routines of the AQAM program included data input on the E-2 aircraft -- an addition at NAS Miramar since 1975. Parking area coordinates, taxiway usage and aircraft landing and take-off operational cycle time-in-mode (LTO) were all modified to accept E-2 aircraft activity. All data were input in accordance with guidelines stipulated in Refs. 7 - 9 and 12. Averaged meteorological data were changed to reflect 1978 figures. The annual amount of aircraft activity for 1978, including arrivals, departures, touch-and-go cycles, and FCLP's was entered according to aircraft type. The specific parking areas and taxiways used by each aircraft were modified. Other emissions information

(specifically; fuel spillage, training fires, environ land use area factors, and off base vehicle miles per year) was either added or updated. Airbase, non-aircraft activity modifications included changes in test cell and run-up stand usage.

#### B. SENSITIVITY STUDY PARAMETERS AND PREDICTIONS

With the update completed and reflecting conditions as they existed at the time of the first intensive study, an investigation was performed to determine the sensitivity of the model predictions to meteorological and operational conditions anticipated for 1-7 August 1979 (special study). Sensitivity results indicate under what conditions and at what receptor locations the model can best be validated. In addition, these results are needed before conclusions can be drawn from the comparison of measured and predicted pollution levels. In a model validation effort, predicted concentrations are compared to measured values at specific receptor locations. When making these comparisons it is necessary to know how sensitive the model predictions are to the uncertainties in the specified meteorological and operational input data. For example, stability category is normally specified as an integer value between one and six; if the hourly averaged value can only be specified as two or three, what effect would this variation have on the model predictions? In addition, it is necessary to know whether the monitoring stations are located in regions where there are large horizontal gradients in pollution concentrations.



Twelve special receptors were used to examine the sensitivity of predicted pollution levels in the vicinity of the four monitoring stations to various meteorological conditions and model parameters. A previous model sensitivity study had been conducted by Netzer (Ref. 9) using 1975 operational data and different nominal meteorological conditions. Table III describes the special receptor locations used in AQAM for both the sensitivity study and the validation effort. Locations relative to runways, taxiways and refueling areas are depicted in Figure 1.

TABLE III  
SPECIAL RECEPTOR LOCATIONS

AQAM RECEPTOR NUMBER	DESCRIPTION/LOCATION
401	trailer 1
402	trailer 2
403	100 m downwind of trailer 2
404	100 m crosswind (south) of trailer 2
405	100 m crosswind (south- east) of trailer 2
406	trailer 3
407	100 m downwind of trailer 3
408	100 m crosswind (south) of trailer 3
409	approach end of runway 1
410	trailer 4
411	500 m upwind of trailer 4
412	100 m crosswind (north) of trailer 4

In order to perform the sensitivity study it was necessary to establish a reference or nominal case meteorologically and operationally. The anticipated weather conditions for the intensive study period, listed in Section III, were used as the reference weather. Meteorological parameters were varied independently, with aircraft activity kept constant. Table IV indicates the meteorology data input for each of nine computer runs.

TABLE IV  
METEOROLOGY FOR SENSITIVITY STUDY

Run Number	Turner Stability	Wind Speed (m/s)	Wind Direction (deg)	Temperature (°F)	Lid Height (m)
1 (Reference)	2	4.12	290	80	400
2	1	4.12	290	80	400
3	3	4.12	290	80	400
4	2	4.12	290	80	300
5	2	4.12	290	80	500
6	2	2.06	290	80	400
7	2	6.18	290	80	400
8	2	4.12	270	80	400
9	2	4.12	310	80	400

Run number 1 was the reference case. The ambient air temperature was not varied because previous results (Ref. 9) had shown it to have little effect on predicted pollution levels.

The aircraft activity data input to the Source Inventory program were representative of one hour of daytime flight operations. In addition, airbase and environ sources were kept constant with updated 1978 data. In the normal mode of utilization of AQAM, annual totals are input and frequency factors are used to determine the total operations in any one month, week, day, and hour. For the present effort, the "desired" one hour input data had to be scaled up to annual operations in order that the Short Term and Source Inventory programs would function properly. The "scale-up" factor used was:

$$12 \text{ hr/day} \times 31 \text{ day/mo (Aug)} \times 12 \text{ mo/yr} = \underline{\underline{4464}} \text{ hr/yr (1)}$$

(12 hr/day represents no night operations)

Table V presents the aircraft activity values which were held constant for the entire sensitivity study.

TABLE V  
AIRCRAFT ACTIVITY FOR SENSITIVITY STUDY

1 HOUR OPERATIONS					
AIRCRAFT	ARRIVALS	DEPARTURES	TOUCH & GO'S	VFR ARRIVALS	FCLP'S
F-4	3	3	2	2	6
F-8	1	1	1	1	0
E-2	1	1	1	1	0
F-14	3	3	2	2	6
A-4	2	2	1	1	0
F-5	1	1	0	1	0
TRANSIENT	1	1	0	0	0
H-3	0	0	0	0	0

1 YEAR OPERATIONS					
AIRCRAFT	ARRIVALS	DEPARTURES	TOUCH & GO'S	VFR ARRIVALS	FCLP'S
F-4	13392	13392	8928	8928	26784
F-8	4464	4464	4464	4464	0
E-2	4464	4464	4464	4464	0
F-14	13392	13392	8928	8928	26784
A-4	8928	8928	4464	4464	0
F-5	4464	4464	0	4464	0
TRANSIENT	4464	4464	0	0	0
H-3	0	0	0	0	0

As explained in Section I, the results from the Source Inventory program are used along with the meteorological data as input to the Short Term program. Output from the Short Term program was arranged in seven tables. Four tables consisted

of pollutant levels in micrograms per cubic meter from environ, airbase, aircraft and total sources at all specified grid receptors. Each table listed, for all receptors, the receptor number and x-y coordinate location, and the concentrations for all five pollutants. The remaining three tables expressed the same results in terms of fractions of the total emissions from environ, airbase and aircraft sources.

The receptors of interest in the sensitivity study were the twelve special receptors (401-412) and that one where the maximum concentrations existed.

To compare the expected effects of the meteorological variables on the predicted ground level ( $z=0$ ) concentrations, the Gaussian dispersion formula for point sources can be used (Ref. 13).

$$\chi(x,y,z=0;H) = \frac{Q}{\pi\sigma_y\sigma_z\bar{U}} \exp\left[-\frac{1}{2}\left(\frac{y}{\sigma_y}\right)^2\right] \exp\left[-\frac{1}{2}\left(\frac{H}{\sigma_z}\right)^2\right] \quad (2)$$

where:

$\chi$  = concentration, g/m<sup>3</sup>

$Q$  = uniform emission rate, g/sec

$\sigma_y, \sigma_z$  = standard deviations of plume concentrations  
in the horizontal and vertical directions  
respectively, m

$\bar{U}$  = mean wind speed, m/sec

$H$  = initial plume height, m

$y = 0$  along plume centerline

When vertical diffusion is limited by a stable layer at height  $h_{lid}$  the diffusion equation is modified as follows:

$$\chi(x,y,z;H) = \frac{Q}{\sqrt{2\pi} \sigma_y h_{lid} \bar{U}} \exp \left[ -\frac{1}{2} \left( \frac{y}{\sigma_y} \right)^2 \right] \quad (3)$$

For infinite line sources Turner (Ref. 13) utilized:

$$\chi(x,y,z=0;H) = \frac{2q}{\sin \phi \sqrt{2\pi} \sigma_z \bar{U}} \exp \left[ -\frac{1}{2} \left( \frac{H}{\sigma_z} \right)^2 \right] \quad (4)$$

where:

$q$  = source strength per unit distance, g/sec-m

$\phi$  = angle between line source and wind direction,  
 $45^\circ < \phi < 90^\circ$

Major variations of the Short Term program predictions under different meteorological conditions should follow equations (2), (3), or (4), depending upon the receptor location relative to the dominant emission sources (Ref. 9).

#### C. EFFECT OF METEOROLOGICAL PARAMETERS ON MAXIMUM RECEPTOR CONCENTRATIONS

Table VI presents the predicted maximum concentrations of four of the five pollutants and the location of each for the reference case. Also shown are the maximum predicted CO and PT from aircraft sources for each of the other conditions investigated. The meteorological variable is listed in each case.

The reference case indicated that the maximum contributions from the environ sources occurred south of the airbase (at receptors (9,2) and (11,2)). However, high levels of environ pollution (background) also were predicted to occur throughout



TABLE VI  
MAXIMUM RECEPTOR CONCENTRATIONS  
(GRID LOCATION, CONCENTRATION ( $\mu\text{g}/\text{m}^3$ ), FRACTION OF TOTAL

RUN NUMBER	AIRCRAFT			AIRBASE			ENVIRON		
	CO	HC	NOX	CO	HC	NOX	CO	HC	PT
1	11,8	11,8	11,8	11,8	11,8	11,8	9,2	11,2	11,2
REFERENCE CASE	101	31	14	5	2	3	313	110	29
	.61	.74	.74	.04	.05	.22	1.0	1.0	1.0

1 REFERENCE CASE	TOTAL			PT		
	CO	HC	NOX	CO	HC	PT
	9,2	11,2	11,2	11,8	11,8	
	313	110	29	141		

RUN NUMBER	AIRCRAFT		
	CO	HC	PT
2	11,8	11,8	
STAB CAT = 1	60	61	
	.50	.97	
3	13,8	11,8	
STAB CAT = 3	194	255	
	.69	.99	
4	11,8	11,8	
LID HT = 300m	103	150	
	.59	.99	
5	11,8	11,8	
LID HT = 500m	101	139	
	.66	.99	

RUN NUMBER	AIRCRAFT		
	CO	HC	PT
6	11,8	11,8	
WIND SPD = 2.06 m/sec	272	321	
	.63	.99	
7	11,8	11,8	
WIND SPD = 6.18 m/sec	71	94	
	.63	.99	
8	10,8	10,8	
WIND DIR = 270°	131	121	
	.61	.98	
9	11,8	11,8	
WIND DIR = 310°	96	106	
	.66	.98	

the airbase. On the airbase, the contribution from airbase sources was generally negligible, whereas aircraft sources of PT were dominant. Maximum concentrations from aircraft sources occurred for CO and PT at receptor (11,8), near the intersection of the runways. This was generally the case for all the conditions investigated.

### 1. Stability Category

Increasing the stability category (more stable conditions) decreases  $\sigma_y$  and  $\sigma_z$ , and therefore should increase the predicted ground level concentration along the wind vector downwind of the source (see equation (2)). At the peak concentration receptors (Table VI), which are necessarily near the plume centerline, the increase in stability category increased the concentration and shifted the maximum concentration receptor downwind.

### 2. Lid Height

As a plume develops downwind of a source it will spread in a vertical, as well as horizontal, direction. The ground and lid height (elevated inversion layer) act as reflectors of the plume. Increasing the lid height would decrease the concentration only at receptors which are far enough downwind from the source for reflections to occur (see equation (3)). For the maximum receptor location (11,8), lid height had negligible effect on the predicted aircraft concentrations of CO and PT (Table VI) since it was located near the major aircraft sources. However the aircraft contributions increased with lid height since concentrations from environs decreased.

### 3. Wind Speed

Increasing the wind speed should decrease predicted concentrations along the plume centerline for a single source (equations (2), (3) and (4)). This behavior was apparent for the maximum concentration receptors (Table VI, run nos. 6, 1 and 7).

### 4. Wind Direction

Changing wind direction changes the orientation of the plume dispersion. As a result, the receptor where concentrations were a maximum from aircraft sources was predicted to shift to receptor (10,8) when the wind direction became  $270^{\circ}$  (Table VI, run no. 8).

## D. EFFECT OF METEOROLOGICAL PARAMETERS ON CONCENTRATIONS AT SPECIAL RECEPTORS

Short Term output for each of the nine sensitivity runs is presented in Appendix A for the special receptors. The reference case (run no. 1) output includes receptor concentrations for environ, airbase, aircraft, and total sources in  $\mu\text{gm}/\text{m}^3$  as well as fractional values for aircraft sources. Receptor concentrations for aircraft sources (run nos. 2-9) are included in  $\mu\text{gm}/\text{m}^3$  and fraction of total. In order to visualize variations in pollutant concentration, the overall grid system was mapped with contour levels for the sensitivity study in Appendix B. Contours for the reference case are included for CO and PT concentrations from airbase, aircraft, and total sources. Contours for run nos. 2-9 are included for CO and PT concentrations from aircraft sources.

Tables VIIa-d summarize the special receptor concentrations of CO and PT for each of the nine sensitivity runs. In general, the comments relating to the maximum receptor concentrations pertain to the special receptor concentrations. From a modeling standpoint special receptor 401 (trailer 1) proved to be well located for the purpose of measuring background pollutants. As can be seen in Tables VIIa-d, very little CO and PT due to aircraft exist at receptor 401. When finite values did occur (run nos. 2, 3, 7, 8 and 9) they resulted from the aforementioned method of projecting area sources (in this case -- the hot refueling area) upwind to pseudo-point sources.

#### 1. Stability Category

An increase in stability category increases the downwind concentration along the plume centerline from a single source since the plume spreads more slowly. Table VIIa indicates that the area around trailer 1 (receptors 402-405) receives emittants from multiple sources since the concentrations of CO and PT first decreased and then increased with increasing stability category. These receptors are also located very near large sources.

CO and PT concentrations around trailer 3 (receptors 406-408) were significantly higher than those around trailer 2 due to the effect of an increased number of plumes overlapping downwind. Some multiple/near source effects were also evident at this location. The receptor concentrations around trailer 4 (receptors 410-412) changed only slightly with variations

TABLE VIIa  
SPECIAL EXERCISE CONCENTRATIONS  
(STABILITY CATEGORY VARIATION)

RUN NUMBER	AIRCRAFT EMITTANT	401 TRAILER 1	402 TRAILER 2	403 100m DOWNWIND	404 100m CROSSWIND	405 100m DOWN AND CROSS	406 TRAILER 3	407 100m DOWNWIND	408 100m CROSSWIND	410 TRAILER 4	411 500m UPWIND	412 100m CROSSWIND	409 APPROACH END OF RW
2 STAB CAT = 1	CO PT	3 20 .05 .92	55 53 .47 .97	81 54 .58 .97	85 123 .59 .98	62 65 .51 .97	121 77 .65 .97	283 294 .83 .99	270 286 .81 .99	21 23 .22 .92	21 25 .26 .93	24 25 .24 .92	927 572 .94 .99
1 REFERENCE	CO PT	0 0 0	3 13 .05 .87	30 25 .32 .93	49 106 .44 .98	45 178 .41 .99	98 78 .59 .97	314 331 .83 .99	225 241 .77 .99	22 26 .27 .93	25 30 .30 .95	26 29 .30 .94	3575 2706 1.0
3 STAB CAT = 3	CO PT	5 28 .06 .93	98 195 .55 .99	141 174 .64 .98	141 325 .64 .99	119 228 .60 .99	246 162 .75 .98	444 424 .85 .99	366 306 .82 .99	38 50 .33 .96	53 68 .47 .97	43 52 .35 .86	1074 660 .94 .99

Concentration,  $\mu\text{gm}/\text{m}^3$

Fraction of Total

KEY = Concentration,  $\mu\text{gm}/\text{m}^3$

Fraction of Total



TABLE VIIb  
SPECIAL RECEPTOR CONCENTRATIONS  
(LID HEIGHT VARIATION)

RUN NUMBER	AIRCRAFT EMISSION	401 TRAILER 1	402 TRAILER 2	403 100m DOWNWIND	404 100m CROSSWIND	405 100m DOWN AND CROSS	406 TRAILER 3	407 100m DOWNWIND	408 100m CROSSWIND	410 TRAILER 4	411 500m UPWIND	412 100m CROSSWIND	409 APPROACH END OF RW
4 LID HT = 300 m	CO PT	0 0	3 13	30 25	49 106	45 178	95 78	320 331	221 240	29 34	30 38	32 37	3512 2710
1 REFERENCE	CO PT	0 0	3 13	30 25	49 106	45 178	98 78	314 331	225 241	22 23	25 30	26 29	3575 2706
5 LID HT = 500 m	CO PT	0 0	3 13	30 25	49 106	45 178	98 78	314 331	225 240	19 22	23 28	23 25	3575 2706

Concentration,  $\mu\text{g}/\text{m}^3$   
Fraction of Total  
KEY = Concentration,  $\mu\text{g}/\text{m}^3$   
Fraction of Total

TABLE VIIc  
SPECIAL RECEPTOR CONCENTRATIONS  
(WIND SPEED VARIATION)

RUN NUMBER	AIRCRAFT INSTANT	401 TRAILER 1	402 TRAILER 2	403 100m DOWNWIND	404 100m CROSSWIND	405 100m DOWN AND CROSS	406 TRAILER 3	407 100m DOWNWIND	408 100m CROSSWIND	410 TRAILER 4	411 500m LWIND	12 100m CROSSWIND	409 APPROACH END OF RW
6	CO	0	88	110	147	170	240	831	675	46	49	55	2151
WIND SPD = 2.03 m/sec	PT	0	221	160	408	265	187	956	734	50	57	57	1376
		0	0	.97	.99	.98	.97	1.0	.99	.93	.94	.94	1.0
1	CO	0	3	30	49	45	98	314	225	22	25	26	3575
REFERENCE	PT	0	13	25	106	178	78	331	241	26	30	29	2706
		0	0	.83	.44	.41	.59	.83	.77	.27	.30	.30	.98
7	CO	2	42	52	76	44	78	204	153	15	17	17	623
WIND SPD = 6.18 m/sec	PT	12	17	.54	.64	.51	57	218	162	17	20	19	378
		.91	.93	.94	.98	.97	.98	.99	.99	.92	.94	.93	1.0

Concentration,  $\mu\text{g}/\text{m}^3$   
Fraction of Total  
Concentration,  $\mu\text{g}/\text{m}^3$   
Fraction of Total

KEY =

TABLE VIId  
SPECIAL JET/PUR CONCENTRATIONS  
(WIND DIRECTION VARIATION)

RUN NUMBER	AIRCRAFT EMITTANT	401 TRAILER 1	402 TRAILER 2	403 100m DOWNWIND	404 100m CROSSWIND	405 100m DOWN AND CROSS	406 TRAILER 3	407 100m DOWNWIND	408 100m CROSSWIND	410 TRAILER 4	411 500m UPWIND	412 100m CROSSWIND	409 APPROACH END OF JET
8 WIND DIR = 270°	OO PT	0 0 .11	27 143 .98	22 52 .95	125 357 .99	72 132 .98	152 135 .98	536 610 1.0	226 260 .99	7 9 .76	10 12 .81	9 11 .80	973 517 .92 .99
1 REFERENCE	OO PT	0 0 0	3 13 .87	30 25 .93	49 106 .98	45 178 .99	98 78 .97	314 331 .99	225 241 .99	22 26 .93	25 30 .95	26 29 .94	3575 2706 1.0
9 WIND DIR = 310°	OO PT	3 18 .93	2 1 .44	5 4 .74	14 30 .95	54 89 .98	4 5 .76	71 38 .95	51 30 .95	41 34 .93	1 29 .94	48 30 .93	1692 1192 .96 1.0

Key =  
Concentration,  $\mu\text{gm}/\text{m}^3$       Fraction of Total  
Concentration,  $\mu\text{gm}/\text{m}^3$       Fraction of Total

in meteorological conditions due to the large downwind distance from the primary sources. Concentrations at receptor 409 were high as expected due to its close proximity to runway and taxiway line sources.

## 2. Lid Height

At trailers 2 and 3 lid height had no effect (Table VIIb). This was expected since these locations are very near the sources of pollution. At trailer 4, which is far downwind, increasing lid height decreased concentrations.

## 3. Wind Speed

As indicated in Table VIIc, an increase in wind speed decreased the concentration downwind at trailers 3 and 4. Again, however, at trailer 2 the behavior was more random.

## 4. Wind Direction

Changing the wind direction from the reference  $290^{\circ}$  to  $310^{\circ}$  (run no. 9) resulted in the expected reduction in aircraft CO and PT at trailers 2 and 3 (Table VIId). In this case the plumes from the major upwind aircraft sources miss receptors 402 and 406. However, when the wind direction was changed to  $270^{\circ}$  (run no. 8), the concentrations increased significantly. This indicates that trailer 2 was apparently outside the plume from the hot refueling area when the wind was from  $290^{\circ}$ . Further evidence of this was that receptors 404 and 405 (crosswind to 402) had significantly higher concentrations than receptors 402 and 403.

The trailer 4 receptor exhibited an increase in concentration with an increase in wind direction. This was expected

since most aircraft source plumes (including the maximum receptor location at coordinate (11,8) are located upwind of trailer 4, from the  $290^{\circ}$ - $310^{\circ}$  direction.

#### 5. Special Receptor Locations

As discussed above, for model validation efforts it is necessary to know whether the monitoring stations are located in regions where there are large horizontal gradients in pollution concentration or where the concentrations are very sensitive to the specified hourly-averaged meteorological conditions. Table VIII presents a summary of the effects of distance from the monitoring stations on the predicted pollution concentrations. Concentrations are presented for each of the nine cases for conditions 100m downwind and 100m crosswind. As a receptor is moved toward a specific plume centerline, the concentration would increase. When a receptor is located downwind from several sources, horizontal movement of the receptor may increase or decrease the receptor pollution level, depending on the multiple plume effects.

Increases in concentration varied by factors of two to sixteen at trailers 2 and 3 for the reference case as a result of moving the receptor 100m downwind or closer to plume centerline. No appreciable horizontal gradients in concentration existed around trailer 4. In almost every case (variation of meteorological parameters), concentrations increased as expected, since the receptors were moved closer to the centerlines of the major aircraft-related plumes for the  $290^{\circ}$  wind. In run no. 8,

TABLE VIII

## DIFFERENCE FACTORS IN SPECIAL RECEPTOR CONCENTRATIONS

RUN NO.		<u>Trailer 2</u>		<u>Trailer 3</u>		<u>Trailer 4</u>
		100m down- wind 403/402	100m cross- wind 404/402	100m down wind 407/406	100m cross- wind 408/406	
1 Reference	CO	inc 10	inc 16	inc 3	inc 2.3	No change
	PT	inc 2	inc 8	inc 4.3	inc 3	
2 Stability Category	CO	inc 1.5	inc 1.5	inc 2.5	inc 2.3	No change
	PT	no change	inc 2.5	inc 3.8	inc 3.3	
3	CO	inc 1.5	inc 1.5	inc 1.8	inc 1.5	
	PT	dec 1.1	inc 1.7	inc 2.5	inc 2.3	
4 Lid Height	CO	inc 10	inc 16	inc 3	inc 2.3	No change
	PT	inc 2	inc 8	inc 4.3	inc 3	
5	CO	inc 10	inc 16	inc 3	inc 2.3	
	PT	inc 2	inc 8	inc 4.3	inc 3	
6 Wind Speed	CO	inc 1.3	inc 1.7	inc 3.8	inc 2.8	No change
	PT	dec 1.5	inc 1.8	inc 5	inc 4	
7	CO	inc 1.3	inc 1.8	inc 2.5	inc 2	
	PT	inc 1.5	inc 4.5	inc 3.8	inc 2.8	
8 Wind Direction	CO	dec 1.3	inc 5	inc 3.5	inc 1.5	No change
	PT	dec 2.8	inc 2.5	inc 4.5	inc 2	
9	CO	inc 2.5	inc 7	inc 18	inc 13	
	PT	inc 4	inc 30	inc 7.5	inc 6	



where the wind direction was changed from  $290^{\circ}$  to  $270^{\circ}$ , the concentration at the 100m downwind location decreased at trailer 2.

These results again indicate that comparison between measurements and predictions will be most difficult at trailer 2. Not only do multiple plume effects and the close proximity to ground aircraft sources cause unusual variations in concentration with changing meteorology but also the horizontal gradients are quite large.

#### E. EFFECT OF SPECIFIED AREA SOURCE SIZE ON RECEPTOR CONCENTRATIONS

When large sources are input into AQAM they are normally modeled as area sources. The dimensions of the area sources have to be specified and some judgement is required to pick the most representative dimensions of these "uniform concentration sources." To determine what effect the specified size of aircraft area sources had on concentrations at various receptors, the lengths of the sides of three prime sources were both increased and decreased by forty percent. The specific sources included the hot refueling area, the hot refueling delay area and the pit refueling delay area. The length of the sides of each area source in the reference case was 500 meters. This length was changed to 300 meters and then to 700 meters.

Increasing the size of an area source effectively moves the pseudo-upwind point source further upwind. Keeping the

emittants and meteorology constant, the plume would spread at the same rate. At a specific receptor, the concentration can increase or decrease, depending on its location relative to the area sources. For this study, the variations in concentrations at trailers 2, 3, and 4 never exceeded six percent.

#### F. VARIATION OF JET PENETRATION LENGTH AND HORIZONTAL AND VERTICAL DISPERSION PARAMETERS

In AQAM, turbojet exhausts during taxi and takeoff are treated as finite line sources. Initial line source dimensions and locations have to be specified and these are somewhat arbitrary. Currently in AQAM the jet is assumed to "penetrate 140 meters" (i.e., approximately 140 jet diameters) before coming to rest relative to the ambient air. Default values for the line source cross-sectional size are 8m high by 20m wide. No plume rise is considered to occur. These line sources are then treated as pseudo-upwind lines which disperse in a Gaussian manner with the same empirical dispersion parameters ( $\sigma_y, \sigma_z$ ) as used for elevated point sources.

In a recent study at the Naval Postgraduate School (Ref. 14) jet characteristics were measured in a simulated, neutrally stable atmosphere. It was found that jet penetration length was considerably less than 140 jet diameters; being more nearly 35 jet diameters. Initial plume dimensions were found to vary significantly with jet orientation to the ambient wind direction and some plume rise was observed. Jet dispersion rates were also found to be more rapid than currently used in AQAM.

In order to determine whether the above findings would have any significant effects on the predicted concentrations from aircraft sources, AQAM was modified in sequential steps as follows:

- (1) decrease the jet penetration length from 140 to 35 meters.
- (2) step (1) and specification of initial aircraft line source (taxiway and runway) dimensions as a function of orientation to the wind (per fig. 40, Ref. 14).
- (3) steps (1) and (2) and decrease the stability category by one to increase the jet plume spreading rate.

Decreasing the penetration length was found to have little effect. This was somewhat expected since the aircraft line sources at NAS Miramar have lengths up to 3.7 km. The reduction in jet penetration length was but three percent of the longest line source. In step (2) the angle of incidence formed by the wind with each line source was determined, and using the  $\sigma_y$  and  $\sigma_z$  versus angle of incidence relationship determined by Brendmoen and Netzer, new horizontal and vertical dispersion parameters were input to the Short Term program. In general, the changes involved increases in initial line source dimensions. At the maximum concentration receptor and at trailers 3 and 4, a nominal reduction in concentrations of up to a maximum of 16 percent was predicted.

In step (3) the above changes were kept in AQAM and the stability category was decreased from 3 to 2 (more unstable conditions). Output indicated a decrease in concentration of up to a factor of two at the maximum concentration receptor and at trailers 3 and 4. It should be noted that in its present form AQAM only allows variation of stability category for all dispersions as opposed to variation of aircraft sources alone. This decrease was expected as previously determined in the meteorological sensitivity study.

#### G. CONCLUSIONS

Stability category and wind speed were the two meteorological parameters that most affected maximum receptor concentrations. Model predictions will therefore be most sensitive to uncertainties in the hourly-averaged values of these parameters which are input into AQAM. Wind direction had a large effect on the concentrations at trailer 2. Trailer 2 is apparently located in an area where large horizontal gradients of pollutant concentrations exist, i.e., near the edges of the plumes from large aircraft sources.

Trailer 1 appears to be a good location for measurement of background pollution levels.

Variations in aircraft area source sizes did not appreciably affect concentration levels at specific receptors.

Variations of the specified jet penetration length and initial horizontal and vertical dispersion parameters of aircraft exhaust plumes during taxi, takeoff and landing modes

changed concentrations by a maximum of only 16 percent. The data of Brendmoen and Netzer (Ref. 14) indicated that turbo-jet exhausts spread more rapidly than elevated point sources. This result, when incorporated into AQAM, significantly affected predicted concentration levels (by a factor of 2) at the monitoring trailer locations.

## V. COMPARISON OF AQAM PREDICTIONS WITH DATA FROM THE INTENSIVE STUDY

### A. VALIDATION REQUIREMENTS

As previously stated, model validation consists of comparing predicted hourly-averaged pollutant concentrations to hourly-averaged measured values at specific receptor locations. A determination of model accuracy must be made within the context of the accuracy of the input operational data and of the hourly-averaged meteorology and measured concentrations. It is important to note that although the meteorology and pollutant concentrations may be constantly varying, only hourly-averaged values are used. Comparisons between measured and predicted concentration values in areas where large horizontal gradients exist (trailer 2) are likely to exhibit widely-varying results. Because of these factors, a need exists for a vast amount of accurate data with which to conduct model validation.

Prior to the comparison of measured and predicted values, background levels/local air quality must be determined in order



to be able to separate the contributions of aircraft, airbase and environ sources throughout the receptor grid. The Source Inventory program allows for input of environ sources. If these data are not available, approximate inputs can be included through the use of land-use factors. The factors (Ref. 12) distinguish between city center, urban, rural, park areas, etc. Input for off-base line sources (roadways) requires appropriate vehicle mileage and speed values. The selection of appropriate land-use factors used in this study was somewhat judgemental. The roadway line source values used were based on actual average daily traffic volumes for 1978 as provided by the Comprehensive Planning Organization of the San Diego Region. One method for determining actual concentrations from aircraft/airbase sources is to subtract values from an upwind measurement (i.e., trailer 1 data) from values obtained at each of the other special receptors.

Comparison of weekend measured data at each special receptor with weekday data should also provide a good indication of background/envIRON pollutant levels due to the reduction in aircraft activity at NAS Miramar on weekends. The measured data indicated a wind speed varying from calm to five knots on Saturday and Sunday approximately 90% of the time. The wind direction also varied up to  $180^{\circ}$  throughout the two-day period. This slight-to-stagnant air motion apparently caused an accumulation of pollutants at NAS Miramar from environ (local San Diego) sources. Unfortunately, this behavior



invalidated any comparison between weekday and weekend concentrations for the purposes of validating weekday background levels on the airbase. Therefore, a need exists for additional weekend data when the meteorological conditions are more representative of those experienced during the period of intensive measurement.

## B. DATA REDUCTION AND MODEL INPUTS

Measured data for CO, NOX and THC were provided by NSI in parts per million (ppm). Comparison of these values to AQAM predictions requires conversion to micrograms per cubic meter ( $\mu\text{gm}/\text{m}^3$ ). An accurate conversion exists for CO under standard conditions;  $1111.11 \times \text{ppm CO} = \mu\text{gm}/\text{m}^3 \text{ CO}$ . The most often used conversion for NOX is based upon  $\text{NO}_2$ :  $2000 \times \text{ppm NOX} = \mu\text{gm}/\text{m}^3 \text{ NOX}$ . Measured data were obtained for THC and  $\text{CH}_4$ .  $\text{CH}_4$  often is the major portion of THC concentration in urban atmospheres of North American latitudes. Typical concentrations are 1.25-1.5 ppm (Ref. 6). The  $\text{CH}_4$  conversion is  $666.67 \times \text{ppm CH}_4 = \mu\text{gm}/\text{m}^3 \text{ CH}_4$ . However, aircraft generated hydrocarbons may be significantly heavier than  $\text{CH}_4$ . The only PT data available were measured by a nephelometer in terms of the scattering coefficient, b (bscat). Air samples were also taken to determine total particulates (TP), but the data were invalidated as a result of a filter preparation error by contractors at U. C. Davis. This loss of the TP data severely affected the model validation effort. Particulate concentrations on the airbase had the best chance to be dominated by aircraft sources and therefore provided one of the best means for comparing predictions with measurements. For the bscat data,

an average conversion factor was employed (Ref. 15);  $46.15 \times \text{Neph (bscat)} \approx \mu\text{gm/m}^3 \text{ PT}$ . The latter conversion factor may be in considerable error.

The AQAM model was run over ten one-hour time periods as listed in Table IX. The type of aircraft activity varied considerably throughout the ten AQAM runs. When different from normal operations, remarks of the activity are included in Table IX. The chosen periods of time were primarily in the afternoon when the wind speed and lid height are greatest.

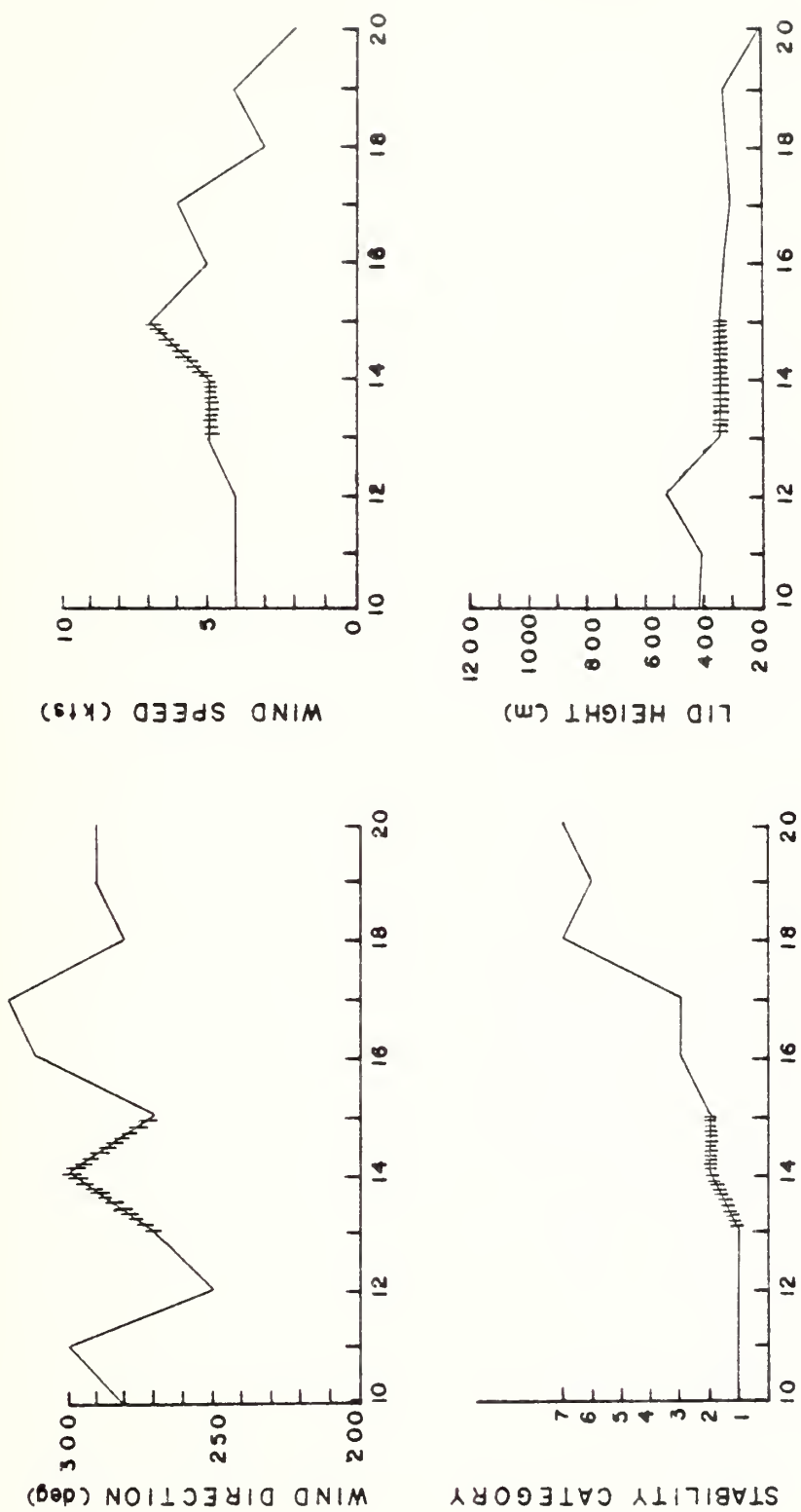
Figures 6a-e present the meteorological conditions at NAS Miramar (obtained from NAS, Pt. Mugu investigators) for the days of intensive measurements and detailed observation of aircraft activity. The values are hourly-averaged and plotted over the 1000-2000 time period for each day. All weather conditions were averaged over the applicable time periods shown cross-hatched in Figures 6a-e.

Runs 5 and 9 were performed to determine whether or not transit time of emittants affected predicted concentration levels relative to runs 4 and 8. A fifteen minute emittant travel time was chosen due to the wind speed and average distance from source to monitoring station. It should be noted that the final runs (6-7 August) had significantly higher wind speed, temperature and lid height. This variation in meteorology was not anticipated and was somewhat undesirable from a model validation viewpoint.

Due to variations in meteorology within the calculated dispersion times, it is generally agreed that the values of

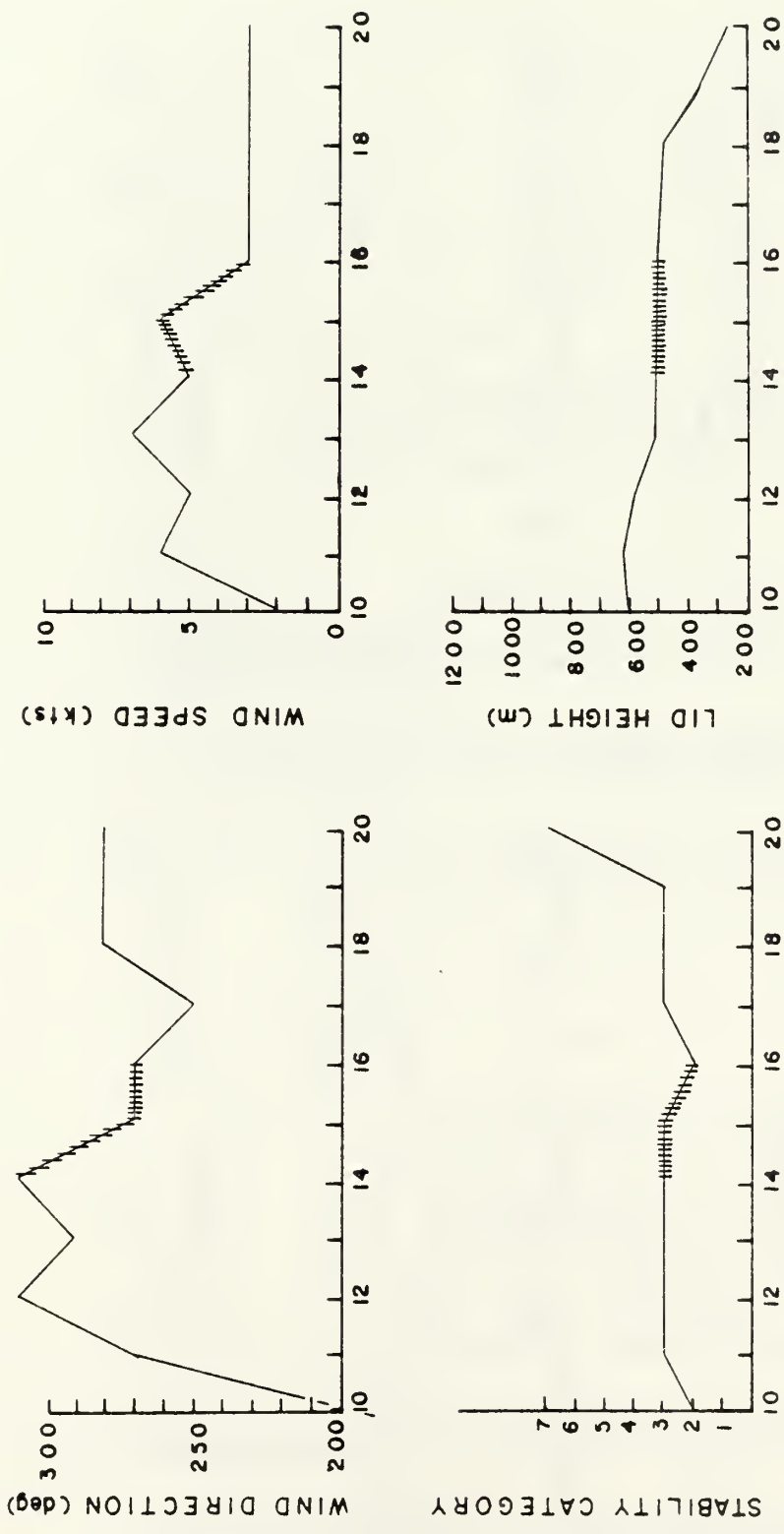
TABLE IX  
AQAM RUNS MADE FOR INTENSIVE STUDY

RUN NUMBER	DATE AND TIME PERIOD	WEATHER CONDITIONS					AIRCRAFT ACTIVITY REMARKS
		TURNER STABILITY CATEGORY	WIND SPEED (m/s)	WIND DIRECTION (DEG)	TEMP (°F)	LID HEIGHT (m)	
1	1 AUG 1300-1400	2	2.57	290	81	353	--
2	1400-1500	2	2.57	290	81	353	--
3	2 AUG 1400-1500	3	2.57	290	77	522	--
4	1500-1600	3	2.57	270	77	517	HI T/O, HI LDG
5	1515-1615	2	1.54	270	76	515	HI T/O, HI LDG
6	3 AUG 1100-1200	1	2.57	230	77	586	--
7	6 AUG 1400-1500	3	3.60	270	91	1287	LO T/O, LO LDG, LO FCPL
8	1500-1600	3	3.09	270	90	1229	HI T/O, LOW LDG
9	1515-1615	3	3.09	270	90	1229	HI T/O, NORMAL
10	7 AUG 1500-1600	3	3.09	300	82	539	LDG LO T/O, NORMAL LDG, FCPL



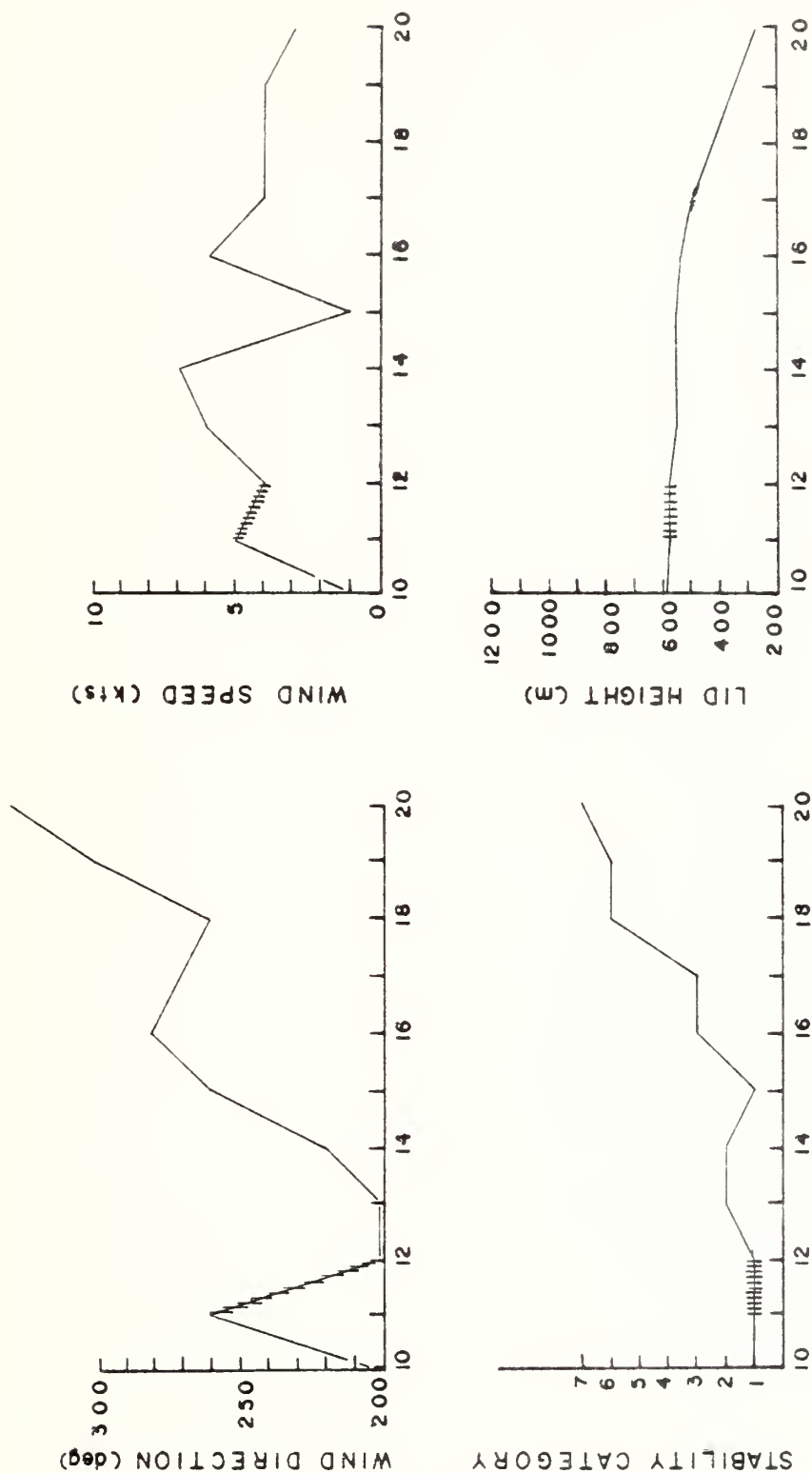
METEOROLOGICAL CONDITIONS AT NAS MIRAMAR VS. TIME OF DAY (1 AUG)

Figure 6a



METEOROLOGICAL CONDITIONS AT NAS MIRAMAR VS. TIME OF DAY (2 AUG)

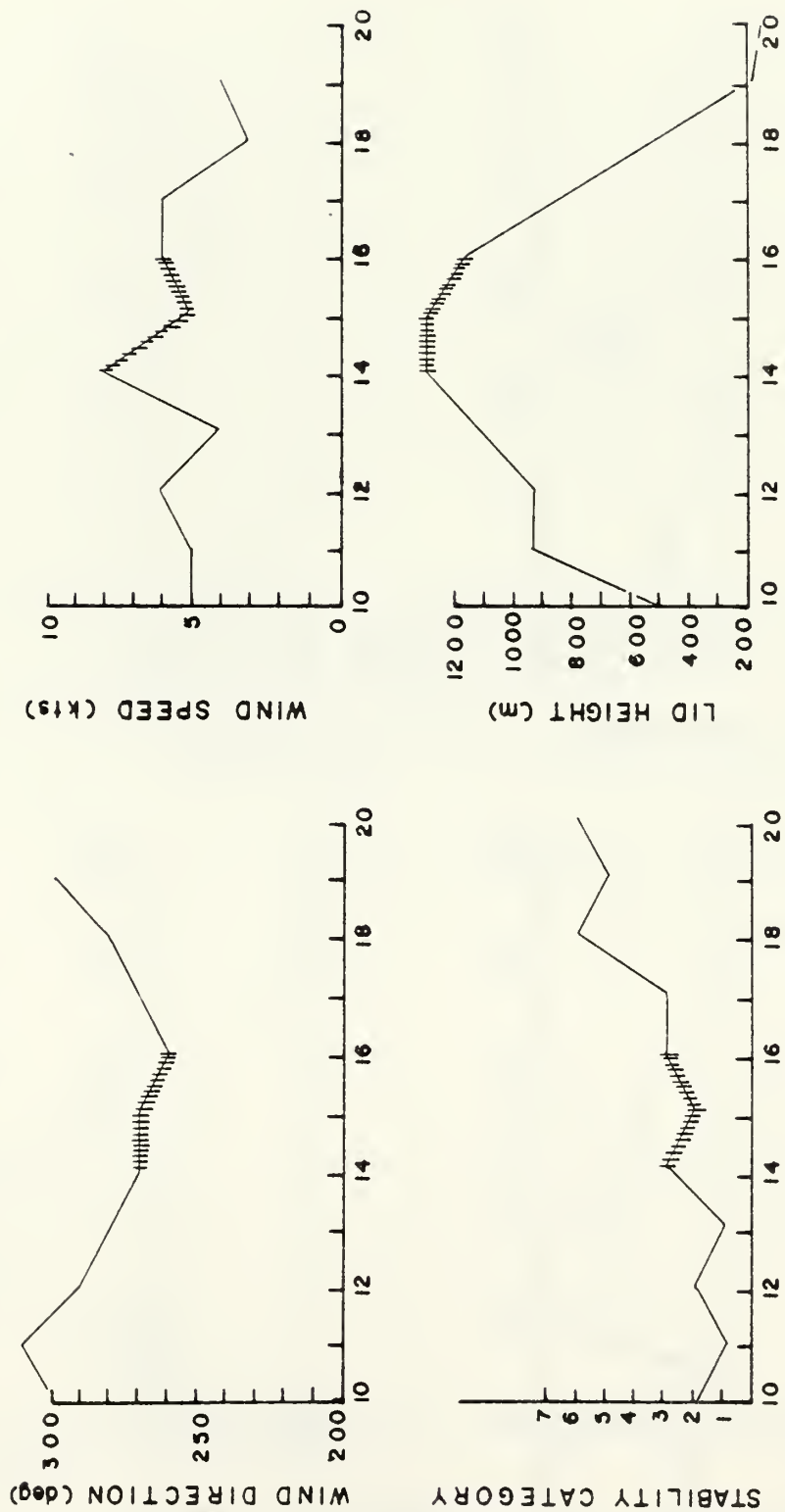
Figure 6b



METEOROLOGICAL CONDITIONS AT NAS MIRAMAR VS. TIME OF DAY (3 AUG)

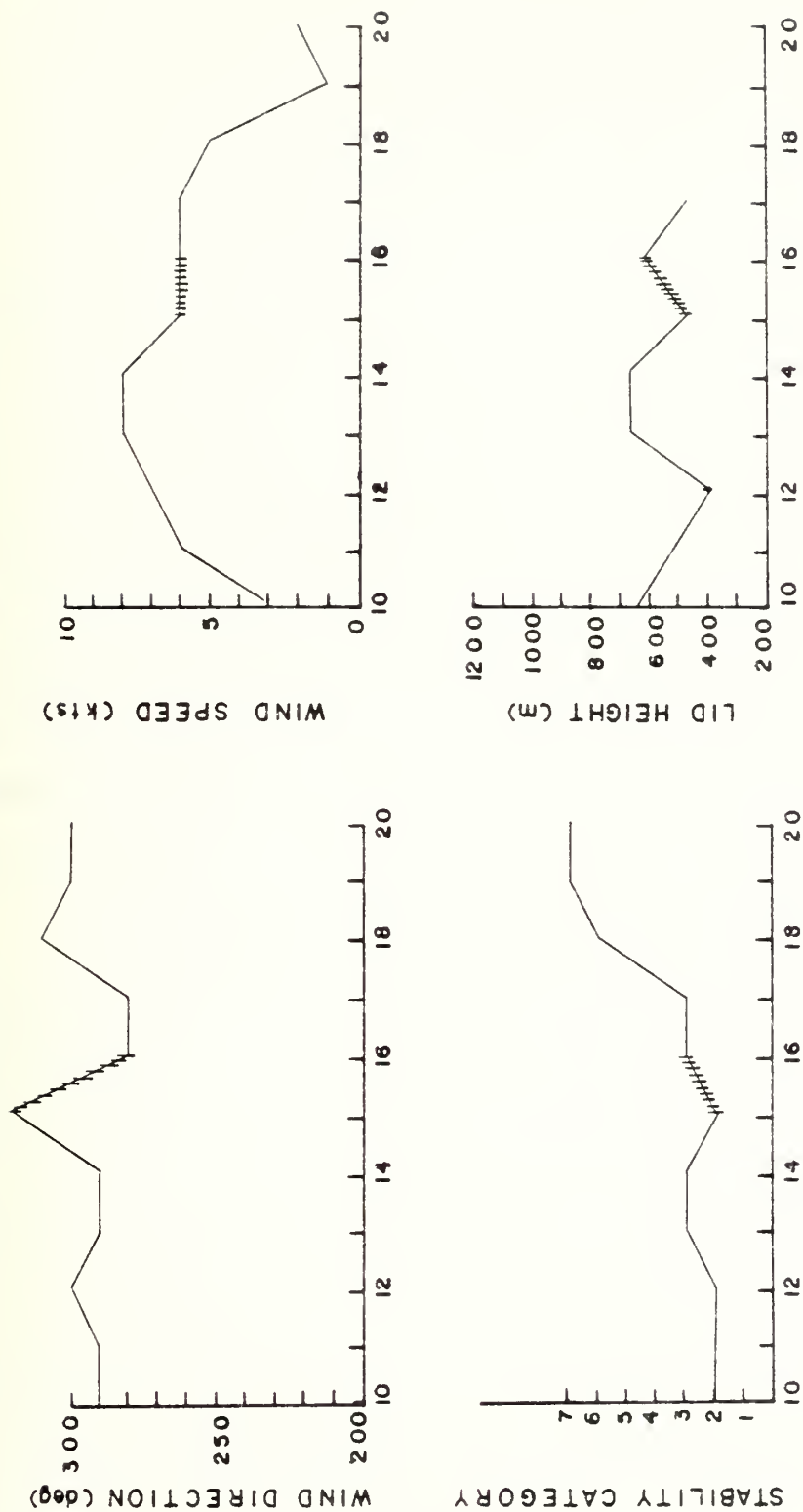
Figure 6c





METEOROLOGICAL CONDITIONS AT NAS MIRAMAR VS. TIME OF DAY (6 AUG)

Figure 6d



METEOROLOGICAL CONDITIONS AT NAS MIRAMAR VS. TIME OF DAY (7 AUG)

Figure 6e

$\sigma_y$  and  $\sigma_z$  cannot be more accurate than a factor of 2. In addition to this uncertainty, model predictions are sensitive to the average meteorology used as input as discussed above. For example, consider the data presented in Fig. 6a for the period 1300-1400 hrs. During this period the wind direction changed from  $270^\circ$  to  $300^\circ$  and the stability category changed from 1 to 2. The lid height and wind speed were steady. Values employed for wind direction and stability category for this period (Table IX, run no. 1) were  $290^\circ$  and 2, respectively. The sensitivity study of section IV has shown that a decrease in wind direction of  $20^\circ$  and a decrease in stability category from 2 to 1 can increase the predicted concentrations at trailer 3 by factors of 1.5 and 1.3 respectively. Thus, measured data and predictions could be different by a factor of approximately 2 due to uncertainty in model meteorological input alone.

### C. DISCUSSION OF RESULTS

This discussion is divided into four sections -- one for each of the pollutants measured. The included figures are scatter plots of measured CO, NOX, THC and nephelometer readings versus predicted concentrations. The diagonal lines drawn in these figures enclose predictions that are within a factor of two of the corresponding measurements. These lines were found to enclose greater than 50% of all the plotted points. Much of the measured data were invalidated by NSI and were therefore not available for plotting. This is the reason for the differences in numbers of

plotted points from graph to graph and was a major limitation in the validation effort. In fact, only approximately 45% of the pollution data taken during the intensive study were considered acceptable. None of the data taken during the first three days of the intensive study met the validation criteria in the EPA quality plan. However, those data had to be used in order to have even a minimum of data to compare with model predictions.

Variations in predicted pollutant concentrations over the airbase were mapped with contour levels for the intensive study and are presented in Appendix C. Contours for run no. 4 (2 Aug, 1500-1600) are included for CO and PT concentrations from airbase, aircraft and total sources. Contours for the other nine runs are included only for CO and PT concentrations from aircraft sources.

#### 1. Carbon Monoxide (CO) Emissions

A comparison of the CO emitted each weekday with the CO emitted during the weekend (period of reduced aircraft activity) was performed to better determine the CO background level. It was found that on Saturday afternoon the level was higher than that on Monday by a factor of two, possibly due to heavy traffic conditions on the surrounding roadways. Also, on Sunday, when the winds were mostly calm or from the south, a high level of CO was measured at trailer 1. As previously stated, weather conditions for the weekend during the period of intensive measurement were not representative of

weather conditions during the weekdays. Therefore, no conclusions could be drawn from this comparison regarding the validity of using trailer 1 measurements as indicators of background CO levels.

Figure 7 indicates that measured concentrations agreed with predicted total concentrations within a factor of two at trailers 1 and 4. The agreement was within a factor of approximately three for trailer 3 data. (No measured CO data for trailer 2 was available during the ten one-hour time periods used in this study.) However, the good agreement may be chance since the environ input (land-use factors, vehicle mileage data, etc.) was only estimated. In other words, what if the high levels of CO concentration at trailer 1 were due to aircraft, but the model did not have properly input aircraft operations or did not correctly determine dispersion rates? AQAM predicted that the CO concentration due to aircraft at trailer 1 was essentially zero. To check this, the Source Inventory program was modified so that all aircraft climb angles on takeoff were decreased. This maximized the near ground emissions from aircraft in the area near trailer 1. This change had no effect on CO at trailer 1. Also, the sensitivity study discussed above indicated no effect from increasing the hot refueling area and hot refueling delay area source sizes. In other words, some inaccuracy in aircraft source specification near trailer 1 would not cause increased concentrations at that receptor. Therefore, it appears to be a valid assumption that trailer 1 was a good

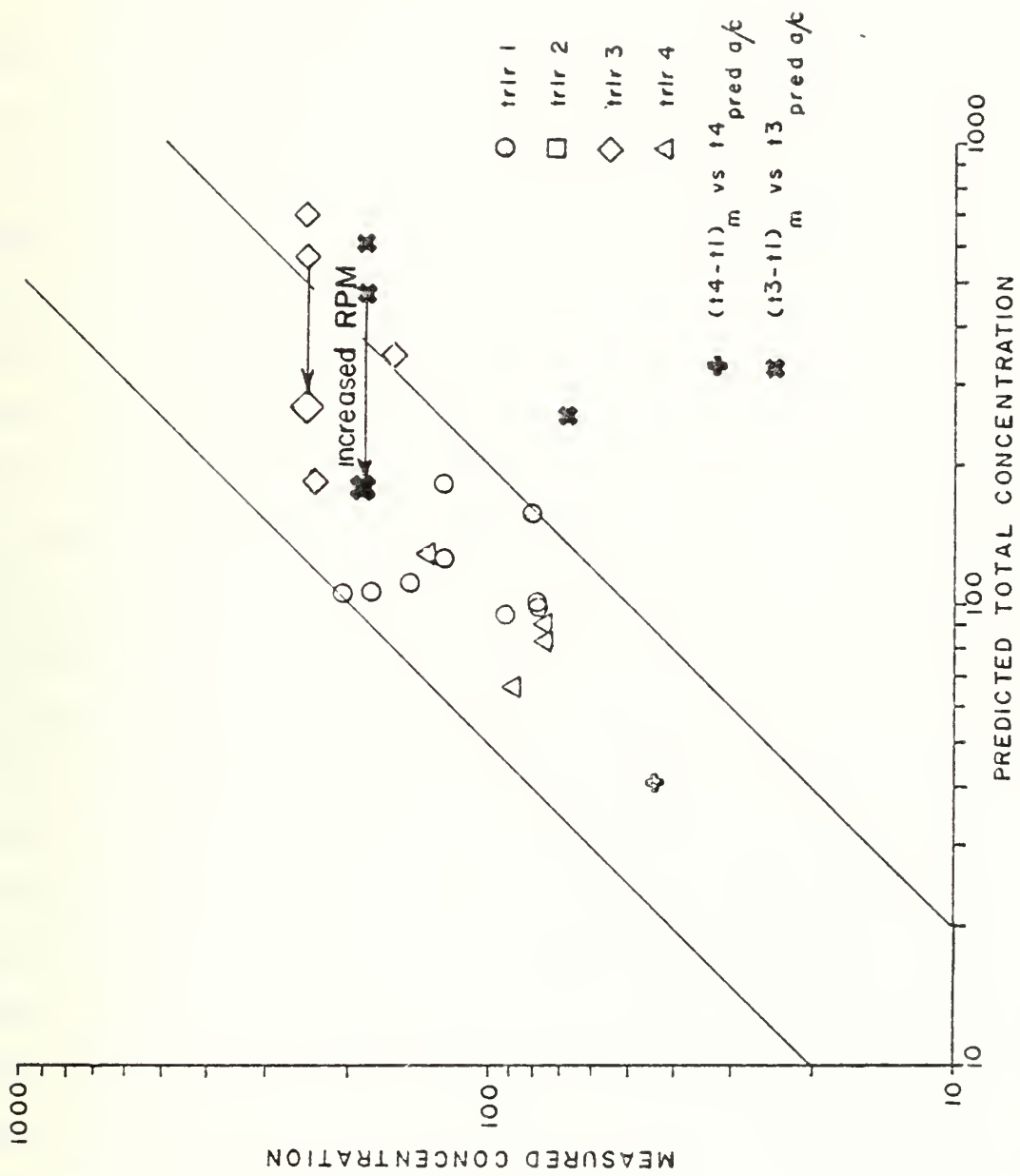


FIGURE 7  
Measured vs. Predicted Hourly Average CO Concentrations for Intensive Study



background level indicator when a westerly wind prevailed, and the AQAM environ input for CO was reasonable. The model predicted that CO concentrations due to environ sources were nearly constant over the entire airbase.

To check the validity of AQAM predictions for CO emissions due to aircraft, trailer 1 measured concentrations (now assumed to be reasonable background CO) were subtracted from the measured concentrations at trailers 3 and 4. Figure 7 shows good agreement for the very limited data available. The higher predicted aircraft CO values at trailer 3 may result either from inaccurate specification of aircraft idle CO emissions in the hot refueling area or from a too slowly-spreading plume. It was observed at NAS, Miramar that many times aircraft were operated at above idle RPM in modes traditionally input into the model as "idle". To briefly examine the effect of the specified engine RPM on the model predictions, all "idle" operations were changed to "normal". For most engines this decreases the relative amounts of CO and UHC while increasing NOX and PM. However, total emittants increase since the fuel flow rate increases. In reality the "normal" setting is far too high to be realistic. This high throttle setting is more realistic for CO and UHC (since they generally decrease rapidly with RPM at low speed and then level off) than for NOX and PT (which generally increase in a linear manner with RPM). A more accurate method would have been to use " $\frac{1}{2}$  idle +  $\frac{1}{2}$  normal", or etc. The increased power setting improved the comparison with measured CO at trailer 3 (Fig. 7). A change of 1 in stability category input to AQAM could also

significantly change the predicted concentrations at trailer 3.

In addition to predicting reasonably accurate concentrations at specific receptors, a model should also correctly predict concentration profiles across the receptor grid. A CO concentration profile across the airbase was constructed (Figure 8) to illustrate the variation in predicted concentration along the wind direction. In the two cases plotted, the wind was from  $270^{\circ}$  and the stability category was 3. The two profiles were plotted along the 8 km. y-coordinate since this y-coordinate most nearly passed through the trailer 1-4 locations. Predicted and measured trailer data that were available were also plotted. "Trailer profiles" were sketched only to indicate general trends and do not necessarily represent actual variations. The comparison shows, as expected, that the predicted trailer 1-4 variation had a much larger gradient than the 8 km. profile due to closer proximity to aircraft ground operations (taxiways, hot refueling areas, parking areas). The measured profiles for both 2 Aug and 6 Aug were similar to the predicted profiles, peaking between trailers 2 and 3. The higher predicted values at trailer 3 were discussed above. Also shown in Figure 8 is the improved "trailer profile" obtained when engine RPM was increased from "idle" to "normal" as discussed above.

## 2. NOX Emissions

Comparison of weekend/weekday data again permitted no significant conclusions regarding the validity of using trailer 1 as an indicator of background NOX.

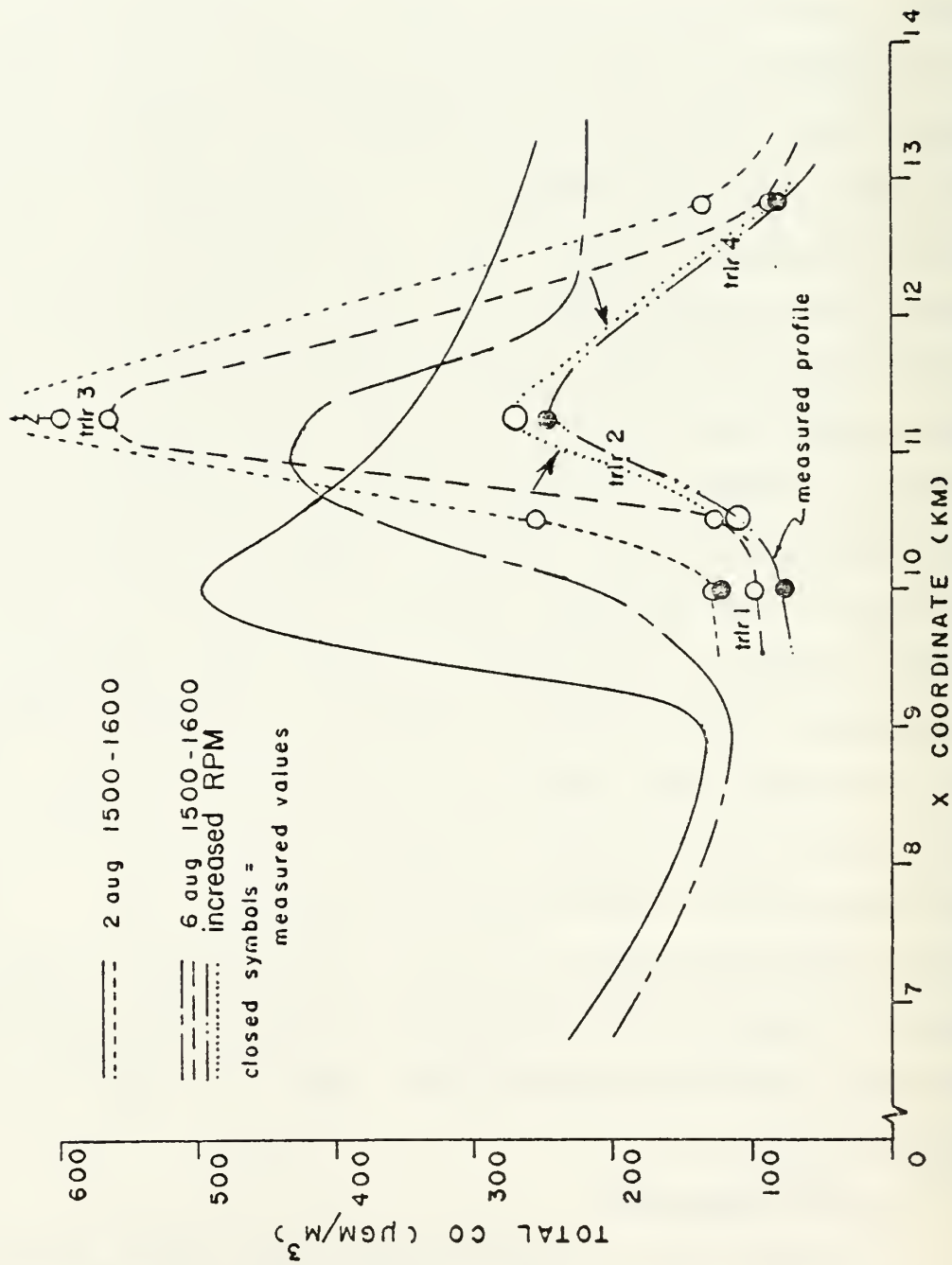


FIGURE 8  
Predicted CO Concentration Profiles Along 8 km. y-coordinate

Figure 9 presents measured versus predicted hourly-average NOX concentrations for trailers 1, 2, and 4. (No measured data were available for trailer 3 during the ten one-hour time periods selected for validation efforts). As previously stated, the comparison was based upon an NO<sub>2</sub> conversion factor for ppm to  $\mu\text{gm}/\text{m}^3$ . Predicted concentrations from both aircraft sources alone and total sources are plotted to indicate their relative magnitudes. Predicted total concentrations at trailers 1 and 4 agreed with measured concentrations within a factor of approximately three. It should be noted that the predicted concentrations were all very small and varied much less than the measured data. Also, the measured data at trailer 2 were much greater than predicted NOX concentrations.

Because of the general agreement between trailer 1 measured and predicted concentrations, it appears that trailer 1 again provided a good representation of background concentrations. Therefore, trailer 1 measured concentrations were subtracted from those measured at trailers 2 and 4 and compared to predicted aircraft NOX emissions. Again, at trailer 2 the measured (difference) values were much greater than predicted aircraft concentrations. At trailer 4 the measured (difference) data agreed reasonably well with predicted aircraft data (both were very small). Since trailer 4 and trailer 1 concentrations were nearly the same for both measured and predicted data, and only approximately one-half of

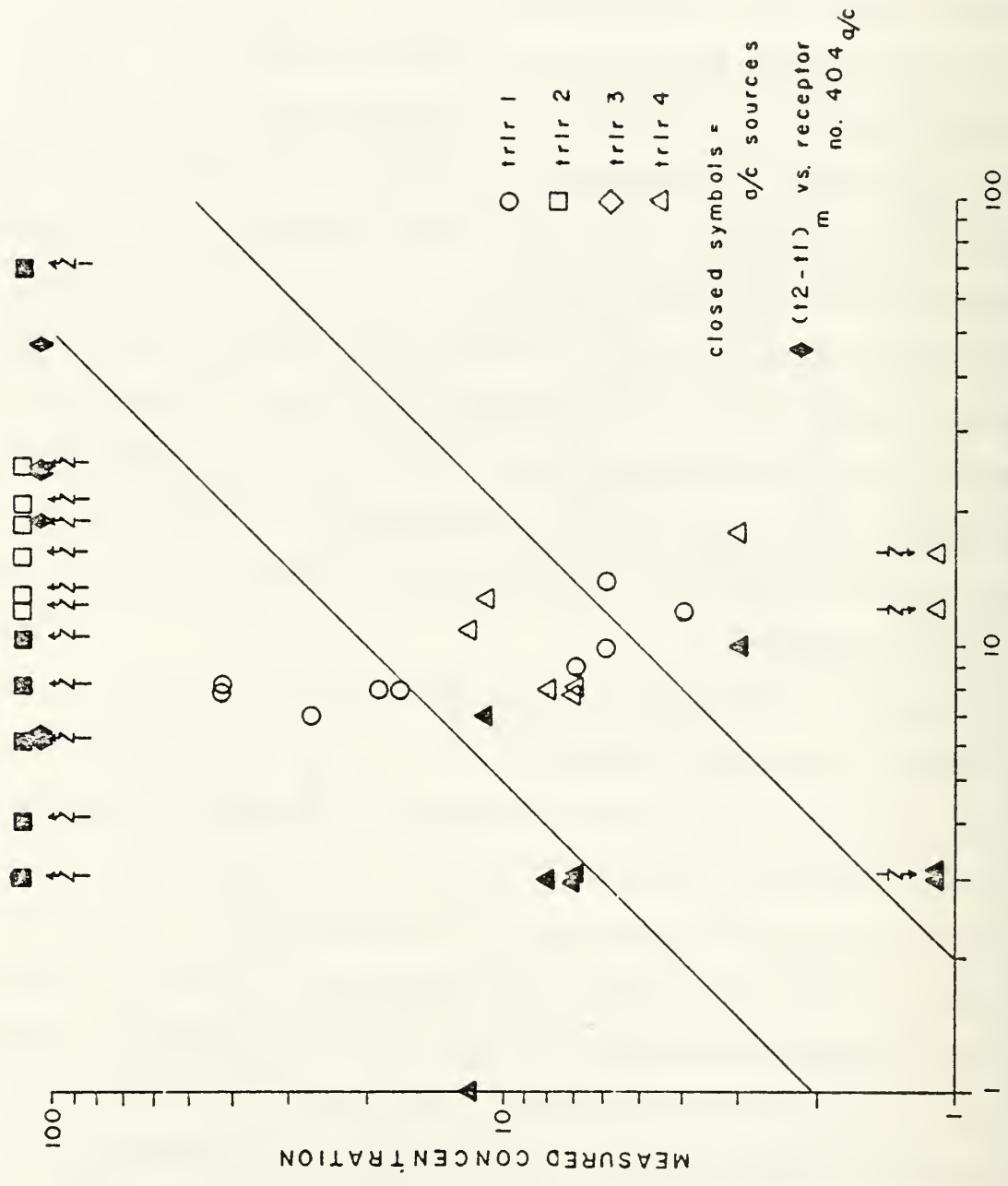


FIGURE 9

Measured vs. Predicted Hourly Average NOx Concentrations For Intensive Study

the predicted trailer 4 values were due to aircraft, trailer 4 was probably outside most of the aircraft plumes for the existing wind conditions.

Because trailer 2 was located in a near-source region where lateral concentration gradients were large, comparisons were also made to crosswind receptor concentrations. The (trailer 2 - trailer 1)<sub>measured</sub> concentrations were compared to the predicted concentrations from aircraft at special receptor 404 (100m crosswind/south of trailer 2). The predicted concentrations were still much less than measured concentrations, indicating that the predicted concentration gradients around trailer 2 were not enough to significantly improve the comparison between predictions and measurements.

These results indicate that the NOX emissions from aircraft engines specified in AQAM are too low for low power engine operations (idle and taxi). An alternative explanation is that the aircraft engine settings for aircraft located around trailer 2 (hot refueling area, taxiways, and parking areas) are well above idle, thus producing more NOX than assumed by AQAM. Increasing the engine settings from idle to normal as discussed above did greatly improve the comparison between (trailer 2 - trailer 1) predictions and measurements (from 10 to 136  $\mu\text{gm}/\text{m}^3$  vs. 190  $\mu\text{gm}/\text{m}^3$  measured for 2 Aug from 1400-1500 hrs).

### 3. Total Hydrocarbon (THC) Emissions

The measured versus predicted total hourly-averaged THC concentrations for trailers 1, 3 and 4 are plotted in



Figure 10. (No measured data were available for trailer 2). The conversion factor used for ppm to  $\mu\text{gm}/\text{m}^3$  was based on  $\text{CH}_4$  and was therefore only an approximation for total hydrocarbons. As can be seen from the figure, predicted data were significantly lower and varied much more than measured data. Measured trailer 1 concentrations were approximately 1.5 times greater than trailer 3 concentrations. This decrease is nearly the same as expected for downwind dispersion from far upwind sources (i.e., due to changes in  $\sigma_y$  in equation 3). These results indicate that almost all THC was probably from environ sources. AQAM predicted concentrations at trailer 3 were greater than those at trailers 1 and 4 due to aircraft ground activity. If most of the measured concentrations of THC are in fact due to environ sources and measured trailer 1 values are accurate, then either AQAM values for THC emittants due to environ sources are low (i.e., land-use factors are low) or the conversion factor to  $\mu\text{gm}/\text{m}^3$  is in significant error. The former would also imply that the values used in AQAM for THC emittants from aircraft sources are too high (at trailer 3 downwind of the hot refueling area). This particular observation could have been better clarified had measured data been available from trailer 2. Increasing engine RPM as discussed above in this case reduces THC from aircraft. When combined with increased environ sources of THC, this change would improve the agreement with measurements.

#### 4. Particulate (PT) Emissions

Figure 11 is a plot of the measured (converted bscat) versus predicted total hourly averaged PT concentrations. The

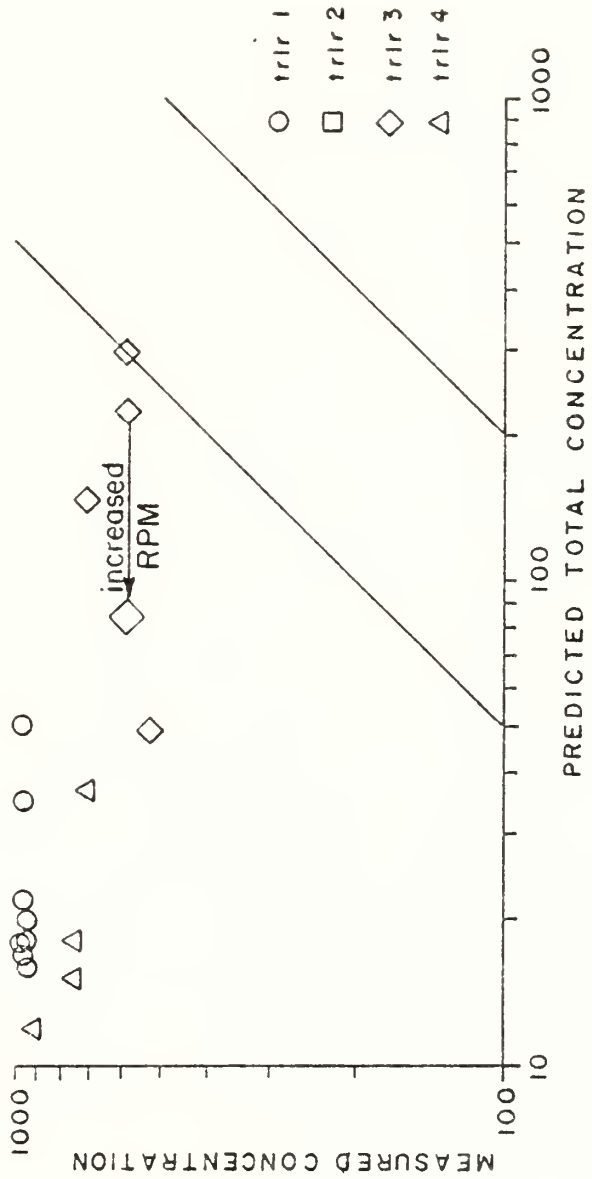


FIGURE 10  
Measured vs. Predicted Hourly Average THC Concentrations for Intensive Study

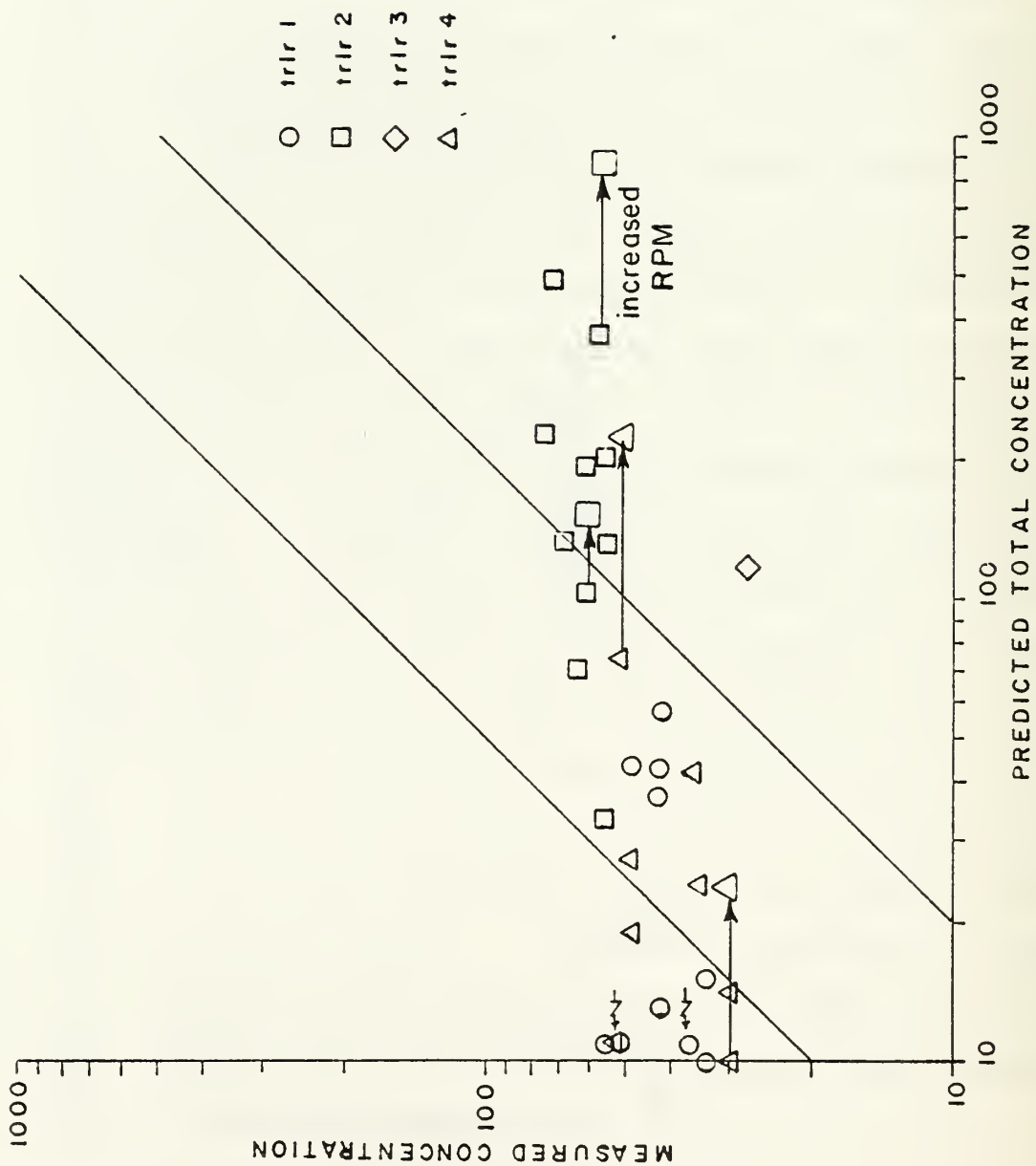


FIGURE 11

Measured vs. Predicted Hourly Average PT Concentrations for Intensive Study

measured data were within  $\pm 40\%$  of the mean value. The measured values at trailers 1 and 4 were essentially the same. The comparison is fairly good (within a factor of three for 70% of the data) at trailers 1 and 4 using the aforementioned conversion factor for bscat to  $\mu\text{gm}/\text{m}^3$ . The model, however, appears to overpredict PT concentrations at trailer 2. AQAM predicts that most of the PT concentration is from aircraft sources. Therefore, if trailer 1 data are good indicators of background PT concentration, then AQAM has low environ source PT input (land-use factors, vehicle mileage, etc.) and/or high aircraft source PT input. Increasing engine RPM as discussed above increases PT and makes the comparison generally less favorable.

#### C. CONCLUSIONS AND RECOMMENDATIONS

Approximately 50% of the predicted levels of concentration were found to agree with measured levels within a factor of two. The results also indicated that: (1) predicted CO concentrations agreed quite well with measured data; (2) model predictions were too low for NOX emissions from aircraft operating in the idle/taxi mode; and (3) predicted THC and PT concentrations were too high for aircraft operating in the idle/taxi mode and/or were too low for environ sources. The latter appears more reasonable. Agreement between model predictions and measured values was significantly improved by increasing engine RPM settings above idle in all modes normally specified at idle.

For a reasonably complete model validation to be accomplished much more measured data must be obtained during a specific time period of observed meteorological and operational activity. The conclusions from this intensive study were based on very limited data and can only be considered preliminary results. Accurate data for background levels/local air quality are important for determination of aircraft source contributions to total emittants. It would be most beneficial to obtain pollution measurements on weekends at a time when aircraft activity is low and meteorological conditions are very similar to weekday conditions. If at all possible, any additional intensive efforts should be conducted during a period with less variations in meteorology. Detailed data collection should begin several days before the detailed operational data are collected in order to ensure a more complete data set than was obtained in this initial effort.

Model predictions were very sensitive to the specified stability category. Model validation efforts could be improved if stability classes could be measured and specified to half-integer values.

Jet dispersion rate differences from those for elevated, low velocity sources and variations with orientation to the wind direction require further study. Plume rise of jet exhausts should also receive additional study.

# APPENDIX A

## Special Receptor Concentrations for Sensitivity Study

WIND = 4000 PERIOD = 0900 TO 1000 HOURS ON A WEEKDAY

RECEPTOR NUMBER	X (KILOMETERS)	Y (KILOMETERS)	CALCULATED DATA FROM UTM/LA SOURCE				EXPECTED AMBIENT MEAN			
			C1	C2	C3	C4	C1	C2	C3	C4
401	10.01	8.24	6.04E-01	1.00E-01	4.62E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
402	10.02	7.70	6.04E-01	1.11E-01	4.53E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
403	10.03	8.92	6.04E-01	1.11E-01	4.53E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
404	10.48	8.37	6.04E-01	1.00E-01	4.83E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
405	10.50	8.30	6.04E-01	1.00E-01	4.83E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
406	11.03	8.45	6.04E-01	1.17E-01	4.10E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
407	11.04	8.52	6.04E-01	1.00E-01	4.83E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
408	11.20	8.26	6.04E-01	1.11E-01	4.53E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
409	12.03	8.36	6.04E-01	1.00E-01	4.53E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
410	12.04	7.31	6.04E-01	1.00E-01	4.53E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
411	12.50	7.50	6.04E-01	1.00E-01	4.53E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
412	12.50	7.40	6.04E-01	1.00E-01	4.53E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01

WIND = 4000 PERIOD = 0900 TO 1000 HOURS ON A WEEKDAY

RECEPTOR NUMBER	X (KILOMETERS)	Y (KILOMETERS)	CALCULATED DATA FROM UTM/LA SOURCE				EXPECTED AMBIENT MEAN			
			C1	C2	C3	C4	C1	C2	C3	C4
401	10.01	8.24	6.04E-01	1.00E-01	4.62E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
402	10.02	7.70	6.04E-01	1.11E-01	4.53E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
403	10.03	8.92	6.04E-01	1.11E-01	4.53E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
404	10.48	8.37	6.04E-01	1.00E-01	4.83E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
405	10.50	8.30	6.04E-01	1.00E-01	4.83E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
406	11.03	8.45	6.04E-01	1.17E-01	4.10E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
407	11.04	8.52	6.04E-01	1.00E-01	4.83E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
408	11.20	8.26	6.04E-01	1.11E-01	4.53E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
409	12.03	8.36	6.04E-01	1.00E-01	4.53E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
410	12.04	7.31	6.04E-01	1.00E-01	4.53E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
411	12.50	7.50	6.04E-01	1.00E-01	4.53E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01
412	12.50	7.40	6.04E-01	1.00E-01	4.53E-01	1.00E-01	1.00E-01	1.00E-01	1.00E-01	2.60E-01

Run No. 1



MC644 = AUS 405 MIRAZAG  
PERIOD = 0000 TO 1000 HRS, ON A WEEKDAY

RECEPTOR CONCENTRATION DATA FROM TOTAL SURFACES									
RECEPTOR		LOCATION		EXPECTED APATHETIC REAR					
NUMBER		(KILOMETERS)	Y	CO	I	HC	FLX	ST	SD
401		17.01	9.27	6.047E 01	1	1.547E 01	7.037E 00	1	1.404E 00
402		16.93	8.76	6.809E 01	1	1.237E 01	5.225E 00	1	1.534E 01
403		17.02	9.42	9.382E 01	1	2.472E 01	6.612E 00	1	2.682E 01
404		16.98	8.37	1.124E 02	1	2.455E 01	8.046E 00	1	1.970E 02
405		17.05	8.56	1.062E 02	1	5.553E 01	2.852E 00	1	1.801E 02
406		17.24	8.79	1.670E 02	1	4.302E 01	1.134E 01	1	3.115E 00
407		17.33	8.32	3.732E 02	1	1.727E 02	2.217E 01	1	3.328E 02
408		17.30	3.26	2.717E 02	1	1.246E 02	1.773E 01	1	2.426E 02
409		17.02	8.36	3.550E 03	1	1.251E 03	4.215E 02	1	2.708E 03
410		17.07	7.81	8.307E 01	1	1.530E 01	9.266E 00	1	2.772E 04
411		17.06	7.50	6.408E 01	1	1.559E 01	1.652E 01	1	2.213E 01
412		17.06	7.40	5.613E 01	1	2.012E 01	1.011E 01	1	3.054E 01
									2.705E 00

Run No. 1

WENTH = 640 GAS AIRPAC POSITION = 0003 TO 1000 HOURS ON A WEEKDAY

RECEPTOR CONCENTRATION DATA FROM AIRCRAFT SOURCES									
RECEPTOR LOCATION									
RECEPTOR NUMBER	X	Y	CALCULATED WINDSPEED, METER						
			CO	HC	NOX	PT	CO2	EXPECTED ATMOSPHERIC WIND	
401	12.01	8.24	9.34E-03	2.55E-03	1.26E-03	5.37E-03	1.76E-03	1.76E-03	1.76E-03
402	12.02	8.40	1.17E-03	5.76E-03	2.03E-03	1.33E-03	3.62E-03	3.62E-03	3.62E-03
403	12.03	8.42	2.99E-03	1.22E-03	1.37E-03	2.50E-03	3.27E-03	3.27E-03	3.27E-03
404	12.04	8.37	4.30E-03	1.42E-03	3.92E-03	1.05E-03	2.55E-03	2.55E-03	2.55E-03
405	12.05	8.30	6.50E-03	1.36E-03	5.53E-03	1.71E-03	5.23E-03	5.23E-03	5.23E-03
406	12.06	8.35	9.34E-03	2.43E-03	6.13E-03	1.43E-03	2.81E-03	2.81E-03	2.81E-03
407	12.07	8.32	2.14E-03	1.55E-03	1.33E-03	3.46E-03	2.81E-03	2.81E-03	2.81E-03
408	12.08	8.35	2.24E-03	1.12E-03	1.26E-03	2.40E-03	6.73E-03	6.73E-03	6.73E-03
409	12.09	8.36	3.57E-03	1.38E-03	4.17E-03	2.70E-03	7.50E-03	7.50E-03	7.50E-03
410	12.10	7.31	2.21E-03	8.03E-03	4.07E-03	2.50E-03	6.76E-03	6.76E-03	6.76E-03
411	12.11	7.50	2.50E-03	8.06E-03	4.10E-03	3.03E-03	7.76E-03	7.76E-03	7.76E-03
412	12.12	7.40	2.55E-03	5.24E-03	5.50E-03	2.91E-03	7.44E-03	7.44E-03	7.44E-03

WENTH = 640 GAS AIRPAC POSITION = 0003 TO 1000 HOURS ON A WEEKDAY

RECEPTOR CONCENTRATION DATA FROM AIRCRAFT SOURCES									
RECEPTOR LOCATION									
RECEPTOR NUMBER	X	Y	CALCULATED WINDSPEED, METER						
			CO	HC	NOX	PT	CO2	EXPECTED ATMOSPHERIC WIND	
401	12.01	8.24	1.54E-03	2.81E-03	2.73E-03	2.03E-03	6.77E-03	6.77E-03	6.77E-03
402	12.02	8.40	4.20E-03	7.22E-03	5.43E-03	6.72E-03	1.51E-03	1.51E-03	1.51E-03
403	12.03	8.42	1.16E-03	4.93E-03	2.93E-03	7.27E-03	3.27E-03	3.27E-03	3.27E-03
404	12.04	8.37	4.22E-03	5.15E-03	4.24E-03	6.02E-03	3.46E-03	3.46E-03	3.46E-03
405	12.05	8.30	6.43E-03	2.80E-03	4.91E-03	5.93E-03	1.98E-03	1.98E-03	1.98E-03
406	12.06	8.35	9.05E-03	7.30E-03	5.91E-03	5.73E-03	3.01E-03	3.01E-03	3.01E-03
407	12.07	8.32	7.33E-03	8.27E-03	7.37E-03	9.42E-03	2.81E-03	2.81E-03	2.81E-03
408	12.08	8.35	7.70E-03	6.01E-03	7.13E-03	9.71E-03	1.51E-03	1.51E-03	1.51E-03
409	12.09	8.36	7.63E-03	7.21E-03	5.83E-03	9.25E-03	7.93E-03	7.93E-03	7.93E-03
410	12.10	7.31	2.67E-03	4.27E-03	4.06E-03	9.46E-03	2.51E-03	2.51E-03	2.51E-03
411	12.11	7.50	3.98E-03	4.90E-03	5.70E-03	9.93E-03	2.76E-03	2.76E-03	2.76E-03
412	12.12	7.40	2.96E-03	4.55E-03	5.40E-03	5.41E-03	2.72E-03	2.72E-03	2.72E-03

MONTH = AUG NAS MINNAH  
PERIOD = 0900 TO 1000 HOURS OF A WEEKDAY

RECEPTOR CONCENTRATION DATA FROM AIRCRAFT SOURCES											
RECEPTOR		RECEPTOR LOCATION		EXTRACTED ATMOSPHERIC MEAN							
NO	362	(KILOMETERS)		(MICROGRAMS/CU. METER)							
		X	Y	CO	I	HC	NIX	PT			
401		10.01	8.24	3.247E-00	1	1.000E-00	3.514E-01	1.963E-01	SO2		
402		10.52	8.46	5.451E-01	1	2.403E-01	2.569E-00	5.282E-01	1.362E-01		
403		10.62	8.42	8.355E-01	1	4.076E-01	4.951E-00	5.559E-01	3.753E-02		
404		10.43	8.37	8.477E-01	1	3.667E-01	3.421E-00	1.247E-02	3.029E-01		
405		10.56	8.35	6.181E-01	1	3.007E-01	3.166E-00	6.524E-01	1.565E-01		
406		11.24	8.35	1.205E-02	1	4.955E-01	7.763E-00	7.079E-01	4.854E-02		
407		11.34	8.32	2.877E-02	1	1.433E-02	1.017E-01	2.944E-02	8.804E-01		
408		11.20	8.26	2.694E-02	1	1.431E-02	1.471E-01	2.957E-02	9.669E-01		
409		12.05	8.36	9.287E-02	1	1.555E-02	1.903E-02	9.712E-02	2.277E-00		
410		12.82	7.31	2.084E-01	1	7.634E-00	4.454E-00	2.427E-01	6.014E-02		
411		12.36	7.50	2.053E-01	1	7.431E-00	4.753E-00	2.466E-01	6.186E-02		
412		12.66	7.40	2.367E-01	1	8.700E-00	4.753E-00	2.549E-01	6.618E-02		

MONTH = AUG NAS MINNAH  
PERIOD = 0900 TO 1000 HOURS OF A WEEKDAY

RECEPTOR CONCENTRATION DATA FROM AIRCRAFT SOURCES											
RECEPTOR NUMBER	RECEPTOR LOCATION		FRACTION OF TOTAL								
	X	Y	CD	I	HC	NIX	PT	SO2			
(KILOMETERS)											
401	10.01	8.24	5.505E-02	1	9.476E-02	1.264E-02	5.158E-01	2.449E-02			
402	10.52	8.46	4.749E-01	1	7.134E-01	3.676E-01	9.569E-01	4.773E-02			
403	10.62	8.42	5.769E-01	1	7.124E-01	4.668E-01	5.674E-01	3.244E-02			
404	10.43	8.37	5.677E-01	1	1.555E-01	5.250E-01	9.857E-01	1.057E-01			
405	10.56	8.35	2.076E-01	1	3.541E-01	4.036E-01	8.732E-01	5.776E-02			
406	11.24	8.35	6.536E-01	1	6.066E-01	6.138E-01	9.793E-01	1.709E-02			
407	11.34	8.32	8.294E-01	1	5.303E-01	7.812E-01	9.541E-01	2.983E-01			
408	11.20	8.26	8.112E-01	1	9.254E-01	7.544E-01	9.335E-01	2.556E-01			
409	12.05	8.36	9.367E-01	1	9.413E-01	5.765E-01	9.963E-01	9.675E-01			
410	12.82	7.31	2.234E-01	1	3.713E-01	4.663E-01	9.177E-01	1.959E-02			
411	12.36	7.50	2.551E-01	1	4.122E-01	5.115E-01	8.314E-01	2.255E-02			
412	12.66	7.40	2.455E-01	1	3.980E-01	4.637E-01	9.235E-01	2.185E-02			

$$A \cup B \cap C = A \cup B,$$

RECEPTOR CONCENTRATION DATA FROM ALCOHOL SPLICES									
RECEPTOR NUMBER	RECEPTOR LOCATION	INSTRUMENTAL DATA					EXPECTED ARITHMETIC MEAN		
		$\chi$	$\gamma$	CI	FC	IMAGINARIAN/CO. NUMBER	PT		
401									
402		10.04	8.24	4.59E-02	1.455E-01	4.540E-01	2.180E-01	3.777E-02	
403		16.52	9.16	5.7E-02	4.771E-01	5.773E-01	1.940E-02	5.777E-01	
404		10.62	8.32	1.413E-02	6.832E-01	7.550E-01	1.720E-02	4.350E-01	
405		16.38	8.37	1.410E-02	5.143E-01	9.250E-01	3.251E-02	9.250E-01	
406		17.55	8.38	1.150E-02	5.251E-01	7.050E-01	2.20E-02	5.551E-01	
407		11.24	8.39	2.45E-02	9.570E-01	1.537E-01	1.040E-02	1.160E-01	
408		11.31	8.39	2.60E-02	2.200E-02	2.432E-01	4.251E-03	1.139E-01	
409		11.70	8.26	3.665E-02	1.700E-02	2.050E-01	2.600E-02	7.600E-01	
410		12.05	8.36	1.370E-01	2.550E-02	1.560E-02	6.00E-02	2.550E-01	
411		12.32	7.31	5.22E-01	1.535E-01	1.603E-01	6.00E-01	1.230E-01	
412		12.56	7.50	5.22E-01	1.540E-01	1.565E-01	6.70E-01	1.802E-01	
413		12.96	7.40	5.302E-01	1.536E-01	9.620E-01	5.160E-01	1.334E-01	

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RECEIVER CONCENTRATION DATA FOR AIRCRAFT SOURCES		FRACTION OF TOTAL						
RECEIVER	RECEIVER LOCATION							
	(KILOPARS)	CJ	GC	FX	PT	SC2		
401	10.01	9.50E-01	1.56E-01	7.62E-02	9.55E-01	2.73E-02		
402	10.52	9.46E-01	7.63E-01		9.57E-01	1.97E-01		
403	10.62	1.37E-01	5.27E-01	5.66E-01	9.36E-01	1.15E-01		
404	10.93	6.44E-01	4.60E-01	6.02E-01	5.53E-01	2.19E-01		
405	10.96	5.53E-01	4.83E-01	5.34E-01	9.70E-01	1.64E-01		
406	11.27	7.49E-01	8.25E-01	7.03E-01	9.64E-01	2.76E-02		
407	11.34	8.51E-01	5.31E-01	6.03E-01	9.75E-01	2.57E-01		
408	11.50	4.19E-01	5.05E-01	4.08E-01	9.53E-01	2.12E-01		
409	12.05	9.37E-01	8.69E-01	6.72E-01	9.56E-01	4.51E-01		
410	12.37	3.69E-01	4.77E-01	5.29E-01	9.60E-01	4.13E-02		
411	12.56	4.68E-01	5.71E-01	7.47E-01	9.76E-01	6.63E-02		
412	12.86	5.68E-01	5.16E-01	6.16E-01	9.61E-01	5.41E-02		

WIND = 40G DIRECTION = 0900 TO 1000 HOURS ON A WEEKDAY

RECEPTOR CONCENTRATION DATA FROM AIRCRAFT SOURCES											
RECEPTOR NUMBER	RECEPTOR LOCATION	EXPLODED AMTHERIC MESH									
	(KILOMETERS)	X	Y	CZ	HC	(MICROGRAMS/CU. METER)	NOX	PT	SC2		
401	10.07	1	8.24	9.31E-05	2.59E-05	1.22E-05	5.56E-04	1	1.75E-06		
402	10.52	1	9.70	3.17E-05	3.54E-01	2.83E-01	1.33E-01	1	3.93E-02		
403	10.62	1	8.42	2.55E-01	1.42E-01	1.67E-04	2.03E-01	1	3.66E-02		
404	10.43	1	8.27	4.36E-01	1.42E-01	3.42E-01	1.05E-02	1	2.85E-01		
405	10.56	1	8.28	4.50E-01	1.36E-01	3.94E-01	1.76E-02	1	5.23E-01		
406	11.27	1	8.35	9.51E-01	3.22E-01	6.02E-01	7.80E-01	1	5.42E-02		
407	11.34	1	8.52	3.20E-02	1.62E-02	1.75E-01	3.34E-02	1	9.82E-01		
408	11.23	1	8.46	2.20E-02	1.05E-02	1.26E-01	2.40E-02	1	6.96E-01		
409	12.05	1	8.56	1.53E-02	1.38E-03	4.17E-02	2.71E-03	1	9.00E-01		
410	12.02	1	7.91	2.35E-01	1.04E-01	2.54E-01	3.37E-01	1	3.86E-02		
411	12.32	1	7.93	3.03E-01	1.09E-01	6.78E-01	3.75E-01	1	9.74E-02		
412	12.86	1	7.43	3.22E-01	1.17E-01	6.75E-01	3.71E-01	1	5.55E-02		

WIND = 40G DIRECTION = 0900 TO 1000 HOURS ON A WEEKDAY

RECEPTOR CONCENTRATION DATA FROM AIRCRAFT SOURCES											
RECEPTOR NUMBER	RECEPTOR LOCATION	FRACTION OF TOTAL									
	(KILOMETERS)	X	Y	CZ	HC	NOX	PT	SC2			
401	10.07	1	8.24	1.91E-05	2.54E-06	2.37E-06	2.91E-04	1	6.45E-07		
402	10.52	1	9.70	4.47E-02	6.92E-02	5.23E-02	8.77E-01	1	1.46E-02		
403	10.62	1	8.42	3.05E-01	4.35E-01	2.45E-01	9.29E-01	1	1.36E-02		
404	10.43	1	8.27	7.19E-01	5.77E-02	4.13E-01	5.32E-01	1	6.78E-02		
405	10.56	1	8.28	3.74E-01	2.47E-01	4.36E-01	9.35E-01	1	1.65E-01		
406	11.27	1	8.35	5.79E-01	8.85E-01	5.22E-01	9.75E-01	1	2.76E-02		
407	11.34	1	8.52	7.87E-01	9.03E-01	7.36E-01	9.27E-01	1	2.19E-01		
408	11.23	1	8.46	7.57E-01	3.67E-01	7.01E-01	5.51E-01	1	1.93E-01		
409	12.05	1	8.56	9.77E-01	9.37E-01	9.65E-01	9.99E-01	1	7.30E-01		
410	12.02	1	7.91	2.63E-01	4.23E-01	4.55E-01	9.33E-01	1	2.48E-02		
411	12.32	1	7.93	2.40E-01	4.47E-01	5.39E-01	9.47E-01	1	2.52E-02		
412	12.86	1	7.43	2.87E-01	4.51E-01	5.27E-01	9.35E-01	1	2.66E-02		

UNIT = 100 NPS MIRAMAR PERIOD = 0500 TO 1000 HOURS ON A WEEKDAY

RECEIVER CONCENTRATION DATA FROM AIRPORT SOURCES									
RECEIVER NUMBER	EXPECTED ARITHMETIC MEAN								
	(MILES)ERS	Y	CU	I	HC	(AIC TO A) SQU. MEAN	PT	FC	CS
	X					MAX			
401	12.04	8.37	7.33E-03	1	4.70E-03	1.30E-03	2.57E-04	1	1.77E-04
402	12.52	8.36	5.17E-03	1	6.51E-03	2.30E-03	1.55E-01	1	3.43E-02
403	10.62	8.32	2.95E-03	1	1.22E-03	1.67E-03	2.93E-01	1	2.64E-02
404	12.48	8.37	4.93E-03	1	1.42E-03	2.63E-03	1.35E-02	1	2.55E-01
405	12.50	8.36	4.50E-03	1	1.26E-03	3.55E-03	1.78E-02	1	5.23E-01
406	11.44	8.32	3.84E-03	1	3.43E-03	6.13E-03	7.83E-01	1	6.40E-02
407	11.31	8.32	3.19E-03	1	1.90E-03	1.33E-03	3.20E-02	1	2.51E-01
408	11.25	8.26	7.24E-03	1	1.15E-03	1.25E-03	2.40E-02	1	3.73E-01
409	12.09	8.32	3.57E-03	1	1.33E-03	5.17E-03	2.70E-02	1	7.00E-01
410	12.84	7.31	1.91E-03	1	6.83E-03	4.23E-03	2.49E-01	1	5.73E-02
411	12.34	7.20	2.35E-03	1	3.27E-03	6.00E-03	2.75E-01	1	7.65E-02
412	12.06	7.30	2.20E-03	1	6.12E-03	5.13E-03	2.32E-01	1	6.41E-02

UNIT = 100 NPS MIRAMAR PERIOD = 0500 TO 1000 HOURS ON A WEEKDAY

RECEIVER CONCENTRATION DATA FROM AIRPORT SOURCES									
RECEIVER NUMBER	EXPECTED ARITHMETIC MEAN								
	(MILES)ERS	Y	CU	I	HC	(AIC TO A) SQU. MEAN	PT	FC	CS
	X					MAX			
401	12.04	8.37	7.33E-03	1	4.70E-03	1.30E-03	2.57E-04	1	1.77E-04
402	12.52	8.36	5.17E-03	1	6.51E-03	2.30E-03	1.55E-01	1	3.43E-02
403	10.62	8.32	2.95E-03	1	1.22E-03	1.67E-03	2.93E-01	1	2.64E-02
404	12.48	8.37	4.93E-03	1	1.42E-03	2.63E-03	1.35E-02	1	2.55E-01
405	12.50	8.36	4.50E-03	1	1.26E-03	3.55E-03	1.78E-02	1	5.23E-01
406	11.44	8.32	3.84E-03	1	3.43E-03	6.13E-03	7.83E-01	1	6.40E-02
407	11.31	8.32	3.19E-03	1	1.90E-03	1.33E-03	3.20E-02	1	2.51E-01
408	11.25	8.26	7.24E-03	1	1.15E-03	1.25E-03	2.40E-02	1	3.73E-01
409	12.09	8.32	3.57E-03	1	1.33E-03	5.17E-03	2.70E-02	1	7.00E-01
410	12.84	7.31	1.91E-03	1	6.83E-03	4.23E-03	2.49E-01	1	5.73E-02
411	12.34	7.20	2.35E-03	1	3.27E-03	6.00E-03	2.75E-01	1	7.65E-02
412	12.06	7.30	2.20E-03	1	6.12E-03	5.13E-03	2.32E-01	1	6.41E-02



ACFT = 410 TAS MISSED = 0900 TO 1000 HOURS 11 A WEEKEND

RECEPTOR CONCENTRATION DATA FROM AIRCRAFT SOURCES									
RECEPTOR LOCATION									
RECEPTOR NUMBER	RECEPTOR LOCATION			EXPECTED ARITHMETIC MEAN					
	X	Y	Z (METERS)	CH	CL	MC	MTX	PT	SCZ
401	10.01	8.24	1	1.33E-04	1	1.34E-06	7.72E-03	1.35E-04	2.10E-01
402	10.82	8.46	1	8.84E-01	1	2.26E-01	2.21E-02	2.20E-02	8.11E-01
403	10.05	8.42	1	1.10E-02	1	5.42E-01	5.67E-00	1.55E-02	4.63E-01
404	10.43	8.57	1	1.97E-02	1	4.47E-01	1.10E-03	4.07E-02	1.05E-01
405	10.58	8.36	1	1.55E-02	1	8.01E-01	5.58E-03	2.65E-02	7.14E-01
406	11.24	8.35	1	2.03E-02	1	7.07E-01	1.45E-03	1.07E-02	1.97E-01
407	11.34	8.32	1	3.51E-02	1	4.85E-02	4.87E-01	9.56E-02	2.57E-03
408	11.21	8.26	1	6.74E-02	1	3.45E-02	2.65E-01	7.34E-02	2.25E-02
409	12.05	8.26	1	2.15E-03	1	5.10E-02	4.21E-02	1.37E-03	5.46E-00
410	12.82	7.31	1	4.32E-01	1	1.93E-01	5.69E-00	4.55E-01	1.25E-01
411	12.56	7.53	1	4.97E-01	1	1.74E-01	1.23E-01	5.69E-01	1.53E-01
412	12.88	7.40	1	5.46E-01	1	2.01E-01	1.10E-01	5.71E-01	1.48E-01

ACFT = 410 TAS MISSED = 0900 TO 1000 HOURS 11 A WEEKEND

RECEPTOR CONCENTRATION DATA FROM AIRCRAFT SOURCES									
RECEPTOR LOCATION									
RECEPTOR NUMBER	RECEPTOR LOCATION			FUNCTION OF TOTAL					
	X	Y	Z (METERS)	CH	CL	MC	MTX	PT	SCZ
401	10.01	8.24	1	1.33E-04	1	1.34E-06	7.72E-03	1.35E-04	2.10E-01
402	10.82	8.46	1	8.84E-01	1	2.26E-01	2.21E-02	2.20E-02	8.11E-01
403	10.05	8.42	1	1.10E-02	1	5.42E-01	5.67E-00	1.55E-02	4.63E-01
404	10.43	8.57	1	1.97E-02	1	4.47E-01	1.10E-03	4.07E-02	1.05E-01
405	10.58	8.36	1	1.55E-02	1	8.01E-01	5.58E-03	2.65E-02	7.14E-01
406	11.24	8.35	1	2.03E-02	1	7.07E-01	1.45E-03	1.07E-02	1.97E-01
407	11.34	8.32	1	3.51E-02	1	4.85E-02	4.87E-01	9.56E-02	2.57E-03
408	11.21	8.26	1	6.74E-02	1	3.45E-02	2.65E-01	7.34E-02	2.25E-02
409	12.05	8.26	1	2.15E-03	1	5.10E-02	4.21E-02	1.37E-03	5.46E-00
410	12.82	7.31	1	4.32E-01	1	1.93E-01	5.69E-00	4.55E-01	1.25E-01
411	12.56	7.53	1	4.97E-01	1	1.74E-01	1.23E-01	5.69E-01	1.53E-01
412	12.88	7.40	1	5.46E-01	1	2.01E-01	1.10E-01	5.71E-01	1.48E-01

Run No. 6

WIND = 10.0 HAZ PERIOD = 0900 TO 1000 HOURS ON A WEEKDAY

RECEPTOR CONCENTRATION DATA FROM AIRPORT STUDIES										
EXPECTED ARITHMETIC MEAN										
RECEPTOR LOCATION	Y	X	HC	CO	SO <sub>2</sub>	NO <sub>x</sub>	PM <sub>10</sub>	PM <sub>2.5</sub>	PT	502
401	3.24	13.01	9.937E-01	2.340E-01	2.143E-01	1.230E-01	1.230E-01	1.230E-01	1.230E-01	1.230E-01
402	3.56	10.52	2.351E-01	4.249E-01	1.754E-01	1.697E-01	1.697E-01	1.697E-01	1.697E-01	1.697E-01
403	3.62	10.52	2.782E-01	2.104E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01
404	3.37	10.52	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01
405	3.35	11.25	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01
406	3.35	11.25	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01
407	3.26	11.25	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01
408	3.36	12.02	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01
409	7.31	12.82	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01
410	7.50	12.82	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01
411	7.40	12.86	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01
412	7.40	12.86	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01

WIND = 10.0 HAZ PERIOD = 0900 TO 1000 HOURS ON A WEEKDAY

RECEPTOR CONCENTRATION DATA FROM AIRPORT STUDIES										
FRACTION OF TOTAL										
RECEPTOR LOCATION	Y	X	HC	CO	SO <sub>2</sub>	NO <sub>x</sub>	PM <sub>10</sub>	PM <sub>2.5</sub>	PT	502
401	3.24	13.01	9.937E-01	2.340E-01	2.143E-01	1.230E-01	1.230E-01	1.230E-01	1.230E-01	1.230E-01
402	3.56	10.52	2.351E-01	4.249E-01	1.754E-01	1.697E-01	1.697E-01	1.697E-01	1.697E-01	1.697E-01
403	3.62	10.52	2.782E-01	2.104E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01
404	3.37	10.52	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01
405	3.35	11.25	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01
406	3.35	11.25	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01
407	3.26	11.25	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01
408	3.36	12.02	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01
409	7.31	12.82	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01
410	7.50	12.82	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01
411	7.40	12.86	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01
412	7.40	12.86	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01	2.782E-01

TIME = 405 NAS MIRAMAR PERIOD = 0500 TO 1000 HOURS ON A WEEKDAY

RECEPTOR NUMBER	RECEPTOR LOCATION		EXPECTED ATMOSPHERIC WIND					
	(KILOMETERS)		(MICROGRAMS/CU. METER)					
	X	Y	CO	HC	NOX	PT	SO2	
401	10.01	8.24	4.960E-01	1.315E-01	4.353E-02	3.500E-01	5.205E-04	
402	10.52	8.76	2.717E-01	8.333E-01	2.693E-01	1.431E-02	4.522E-01	
403	10.02	8.42	2.160E-01	6.375E-01	1.700E-01	5.250E-01	1.355E-01	
404	10.54	8.57	1.450E-02	2.735E-01	1.010E-01	5.675E-02	9.590E-01	
405	11.50	8.36	7.189E-01	2.276E-01	5.175E-01	1.233E-02	3.005E-01	
406	11.24	8.35	1.521E-02	5.542E-01	5.545E-01	1.325E-02	2.199E-01	
407	11.34	8.32	5.351E-02	2.849E-02	2.580E-01	6.050E-02	1.507E-01	
408	11.20	8.26	2.250E-02	1.127E-02	1.363E-01	2.557E-02	7.353E-01	
409	12.02	8.36	3.735E-02	6.390E-01	2.491E-02	5.174E-02	2.035E-02	
410	12.82	7.31	7.395E-01	2.530E-01	2.575E-01	6.818E-01	2.187E-02	
411	12.35	7.50	1.020E-01	3.520E-01	3.500E-01	1.150E-01	3.644E-02	
412	12.02	7.40	8.675E-01	3.075E-01	2.528E-01	1.361E-01	2.644E-02	

TIME = 405 NAS MIRAMAR PERIOD = 0500 TO 1000 HOURS ON A WEEKDAY

RECEIVED CONCENTRATION DATA FROM AIRCRAFT SOURCES									
RECEPTOR NUMBER	RECEPTOR LOCATION	PROPORTION OF TOTAL							
		(KILOMETERS)		CO	HC	NOx	PT	SO2	
401	10.01	9.24	9.017E-03	6.800E-03	1.130E-01	1.301E-04			
402	10.52	9.66	3.447E-01	2.944E-01	9.311E-01	9.603E-02			
403	10.02	9.42	2.050E-01	3.031E-01	2.092E-01	9.502E-01	2.181E-02		
404	10.42	9.37	2.580E-01	2.545E-02	2.125E-01	9.920E-01	1.979E-01		
405	11.50	9.35	4.625E-01	1.150E-01	4.475E-01	9.757E-01	6.915E-02		
406	11.24	9.35	6.455E-01	7.552E-01	5.592E-01	5.301E-01	3.031E-02		
407	11.34	9.32	9.092E-01	9.315E-01	8.245E-01	5.525E-01	3.315E-01		
408	11.20	9.26	7.312E-01	8.205E-01	6.832E-01	9.355E-01	1.637E-01		
409	12.02	9.39	3.207E-01	3.103E-01	5.775E-01	9.547E-01	3.301E-01		
410	12.82	7.53	8.155E-02	1.450E-01	2.871E-01	7.035E-01	5.304E-03		
411	12.36	7.53	4.105E-01	1.579E-01	3.555E-01	8.141E-01	7.503E-03		
412	12.35	7.50	9.685E-02	1.759E-01	3.105E-01	7.947E-01	6.474E-03		

Run No. 8

NOTE = AUG WAS MEASUREMENT PERIOD = 0600 TO 1000 HOURS ON A WEEKDAY

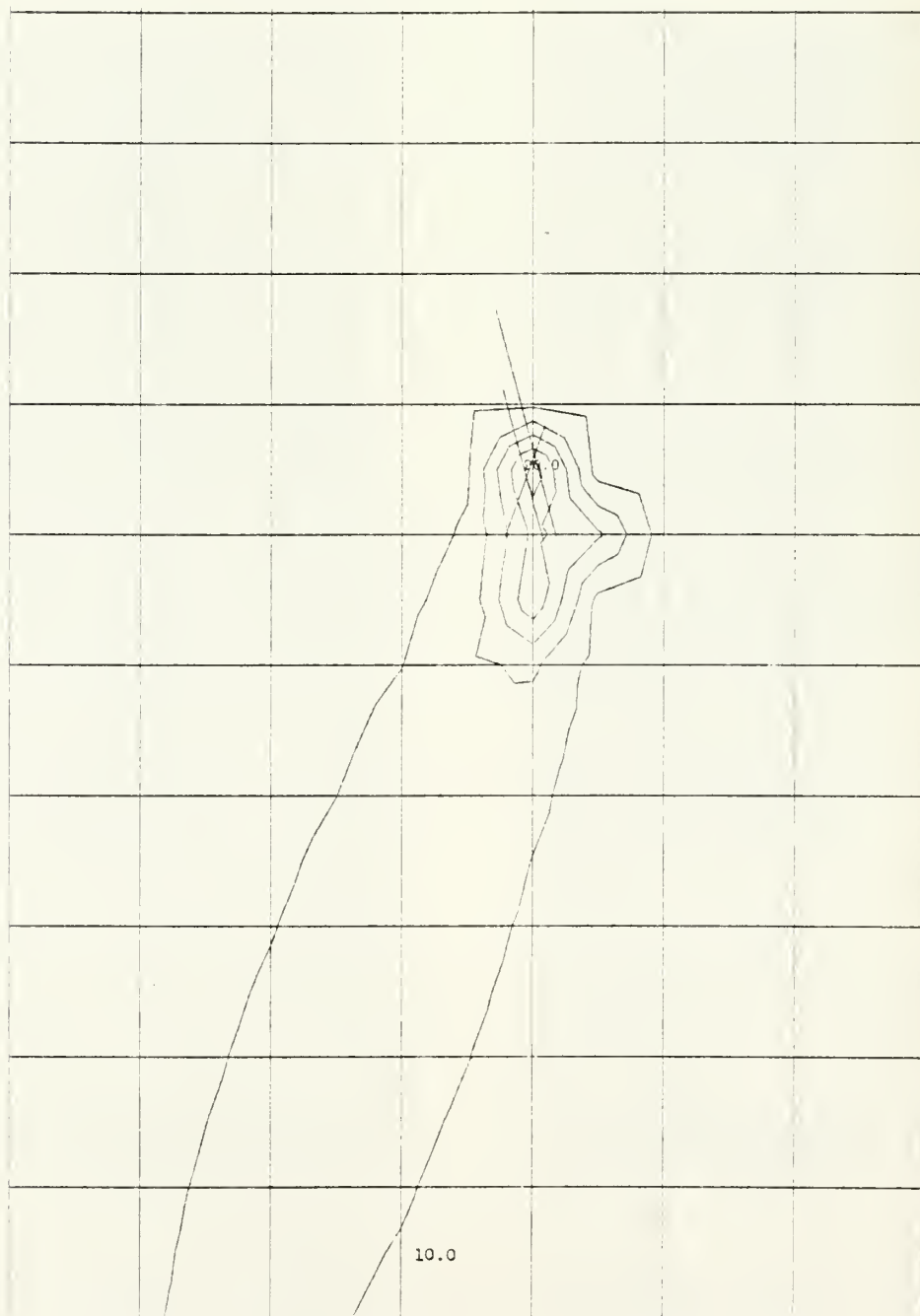
RECEPTOR CONCENTRATION DATA FROM AIRCRAFT SOURCES										
RECEPTOR LOCATION										
EXPECTED METHANE SPAN										
RECEPTOR NUMBER	X	Y	(MICROGRAMS/CO. METER)							
			CO	HC	NOX	PT	SC2			
401	10.01	8.24	3.54E-01	9.35E-01	3.00E-01	1.79E-01	1.79E-01	2.62E-02	2.72E-03	
402	10.52	8.49	1.59E-01	1.22E-01	2.37E-02	1.17E-01	1.17E-01	2.72E-03		
403	10.64	8.42	4.55E-01	9.61E-01	4.94E-01	4.35E-01	4.35E-01	2.58E-01	2.58E-01	
404	10.48	8.37	1.35E-01	3.50E-01	1.01E-01	3.00E-01	3.00E-01	2.58E-01	2.58E-01	
405	10.56	8.46	5.41E-01	2.89E-01	2.84E-01	8.38E-01	8.38E-01	2.62E-01	2.62E-01	
406	11.24	8.55	3.57E-01	1.52E-01	2.54E-01	3.55E-01	3.55E-01	1.77E-02	1.77E-02	
407	11.34	8.52	7.10E-01	3.23E-01	4.27E-01	3.76E-01	3.76E-01	1.06E-02	1.06E-02	
408	11.30	8.26	5.10E-01	2.15E-01	2.71E-01	3.23E-01	3.23E-01	2.62E-03	2.62E-03	
409	12.05	7.46	1.65E-01	3.53E-01	2.37E-01	1.12E-01	1.12E-01	4.20E-01	4.20E-01	
410	12.92	7.31	4.08E-01	1.53E-01	3.87E-01	3.35E-01	3.35E-01	2.37E-02	2.37E-02	
411	12.36	7.50	3.45E-01	1.19E-01	6.54E-01	2.37E-01	2.37E-01	7.54E-02	7.54E-02	
412	12.85	7.40	4.81E-01	1.63E-01	6.63E-01	3.65E-01	3.65E-01	1.10E-01	1.10E-01	

NOTE = AUG WAS MEASUREMENT PERIOD = 0600 TO 1000 HOURS ON A WEEKDAY

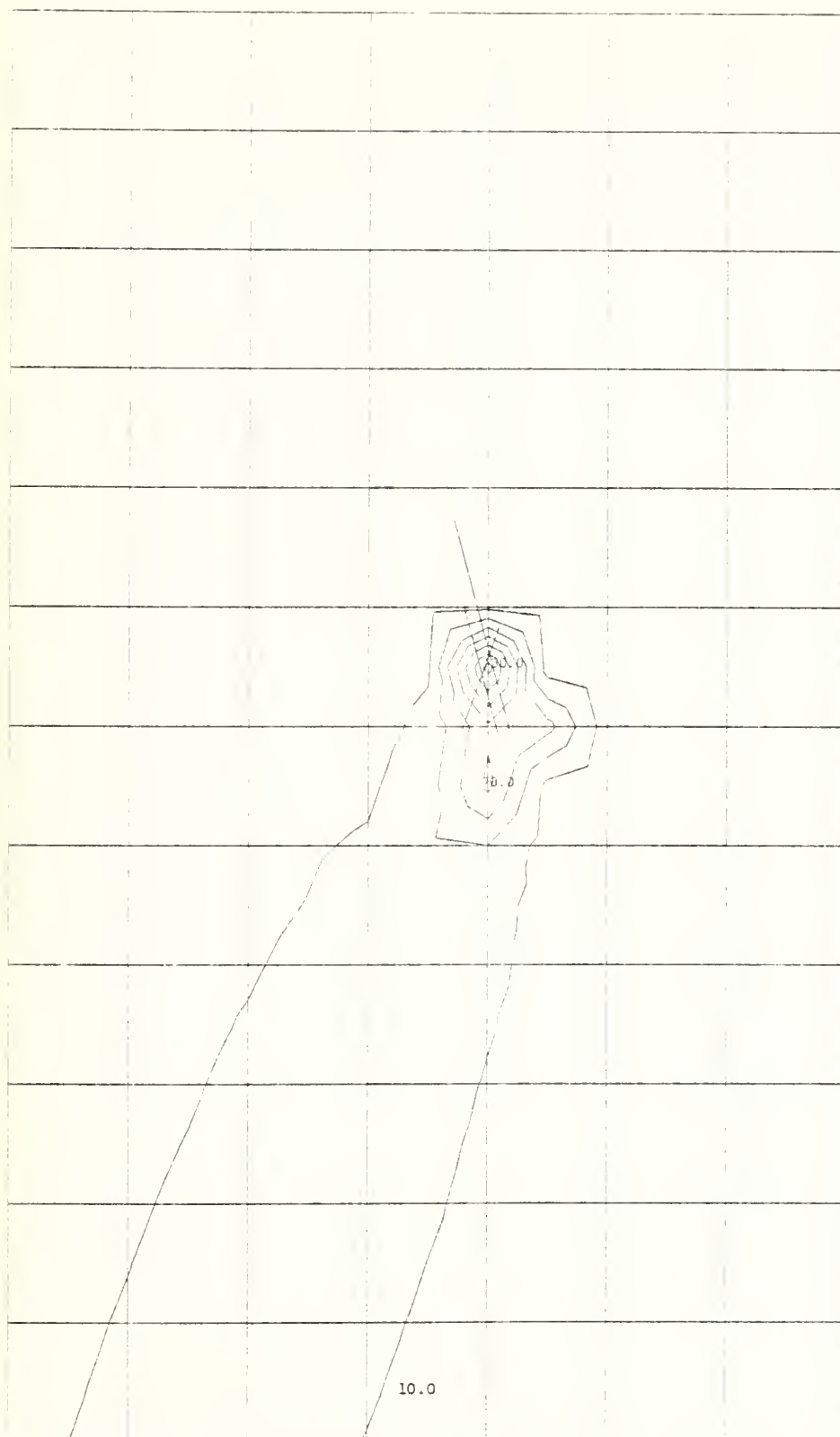
RECEPTOR CONCENTRATION DATA FROM AIRCRAFT SOURCES										
RECEPTOR LOCATION										
FRACTION OF TOTAL										
RECEPTOR NUMBER	X	Y	(MICROGRAMS/CO. METER)							
			CO	HC	NOX	PT	SC2			
401	10.01	8.24	3.54E-01	9.35E-01	3.00E-01	1.79E-01	1.79E-01	2.62E-02	2.72E-03	
402	10.52	8.49	1.59E-01	1.22E-01	2.37E-02	1.17E-01	1.17E-01	2.72E-03		
403	10.64	8.42	4.55E-01	9.61E-01	4.94E-01	4.35E-01	4.35E-01	2.58E-01	2.58E-01	
404	10.48	8.37	1.35E-01	3.50E-01	1.01E-01	3.00E-01	3.00E-01	2.58E-01	2.58E-01	
405	10.56	8.46	5.41E-01	2.89E-01	2.84E-01	8.38E-01	8.38E-01	2.62E-01	2.62E-01	
406	11.24	8.55	3.57E-01	1.52E-01	2.54E-01	3.55E-01	3.55E-01	1.77E-02	1.77E-02	
407	11.34	8.52	7.10E-01	3.23E-01	4.27E-01	3.76E-01	3.76E-01	1.06E-02	1.06E-02	
408	11.30	8.26	5.10E-01	2.15E-01	2.71E-01	3.23E-01	3.23E-01	2.62E-03	2.62E-03	
409	12.05	7.46	1.65E-01	3.53E-01	2.37E-01	1.12E-01	1.12E-01	4.20E-01	4.20E-01	
410	12.92	7.31	4.08E-01	1.53E-01	3.87E-01	3.35E-01	3.35E-01	2.37E-02	2.37E-02	
411	12.36	7.50	3.45E-01	1.19E-01	6.54E-01	2.37E-01	2.37E-01	7.54E-02	7.54E-02	
412	12.85	7.40	4.81E-01	1.63E-01	6.63E-01	3.65E-01	3.65E-01	1.10E-01	1.10E-01	

## APPENDIX B

### CO AND PT CONCENTRATION PROFILES FROM AIRCRAFT SOURCES (SENSITIVITY STUDY)

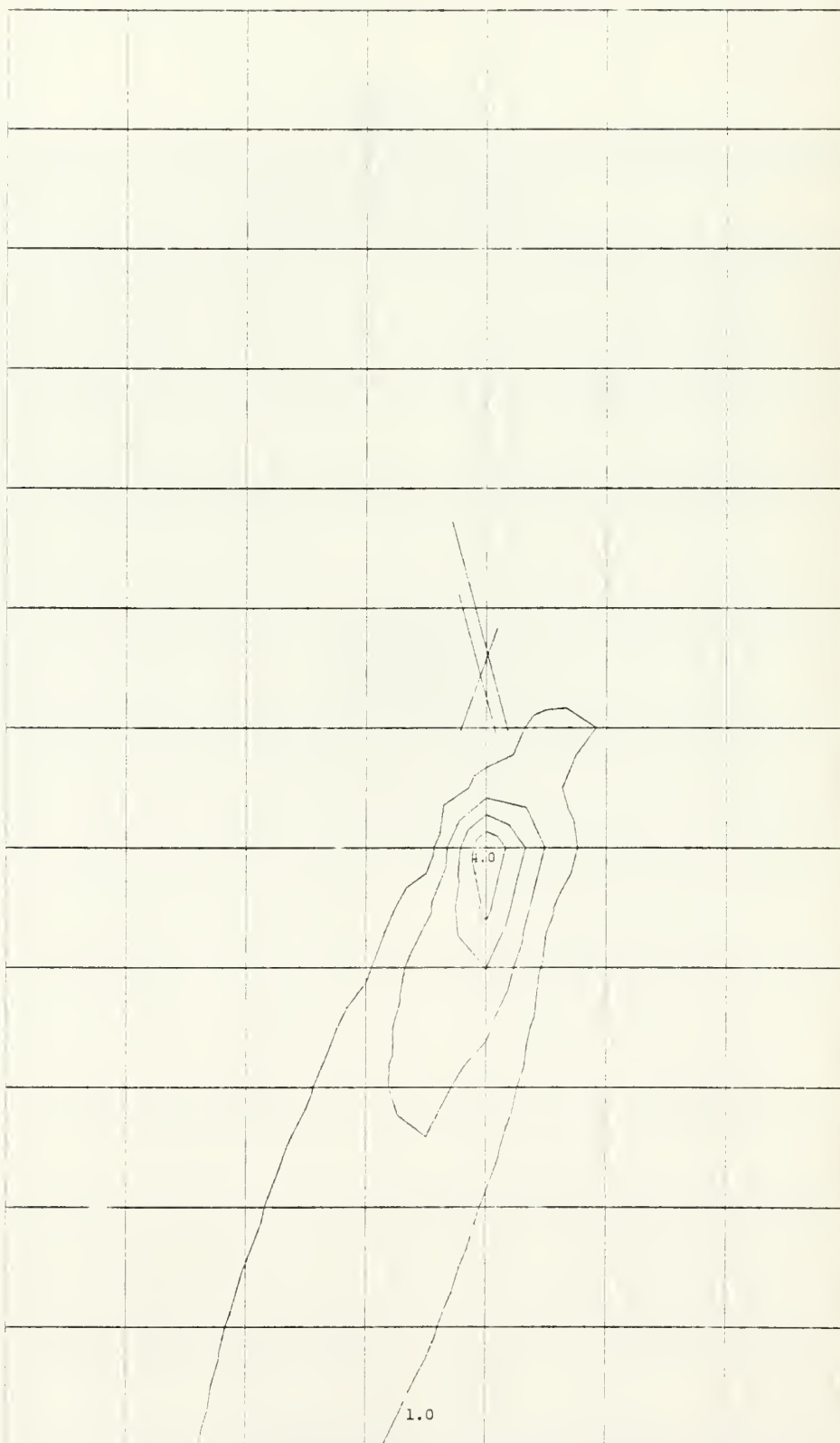


AIRCRAFT CO CONCENTRATION PROFILE (RUN NO. 1)  
(Scale =  $20 \mu\text{gm}/\text{m}^3$  per contour)

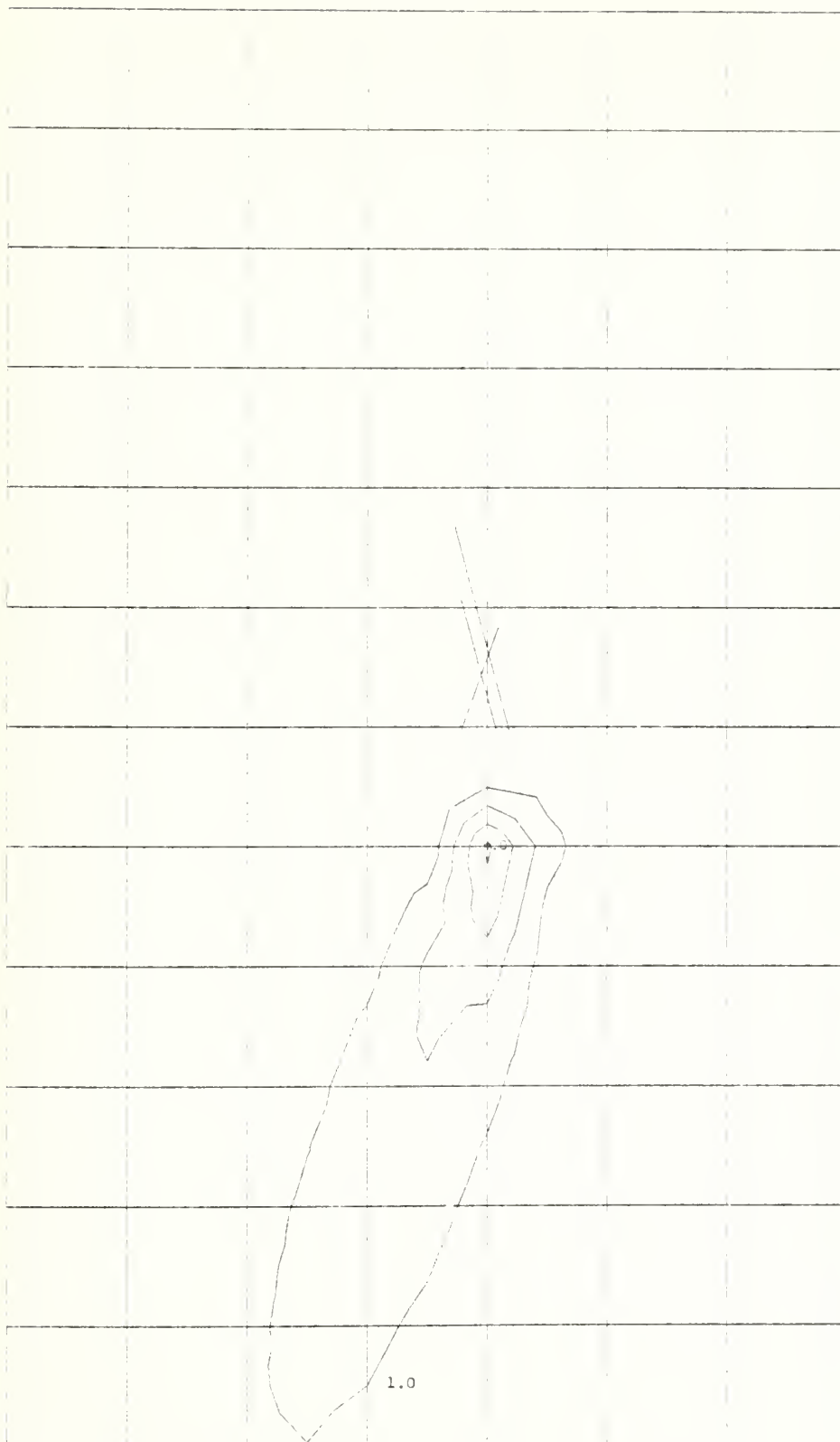


AIRCRAFT PT CONCENTRATION PROFILE (RUN NO. 1)  
(Scale =  $20 \mu\text{gm}/\text{m}^3$  per contour)

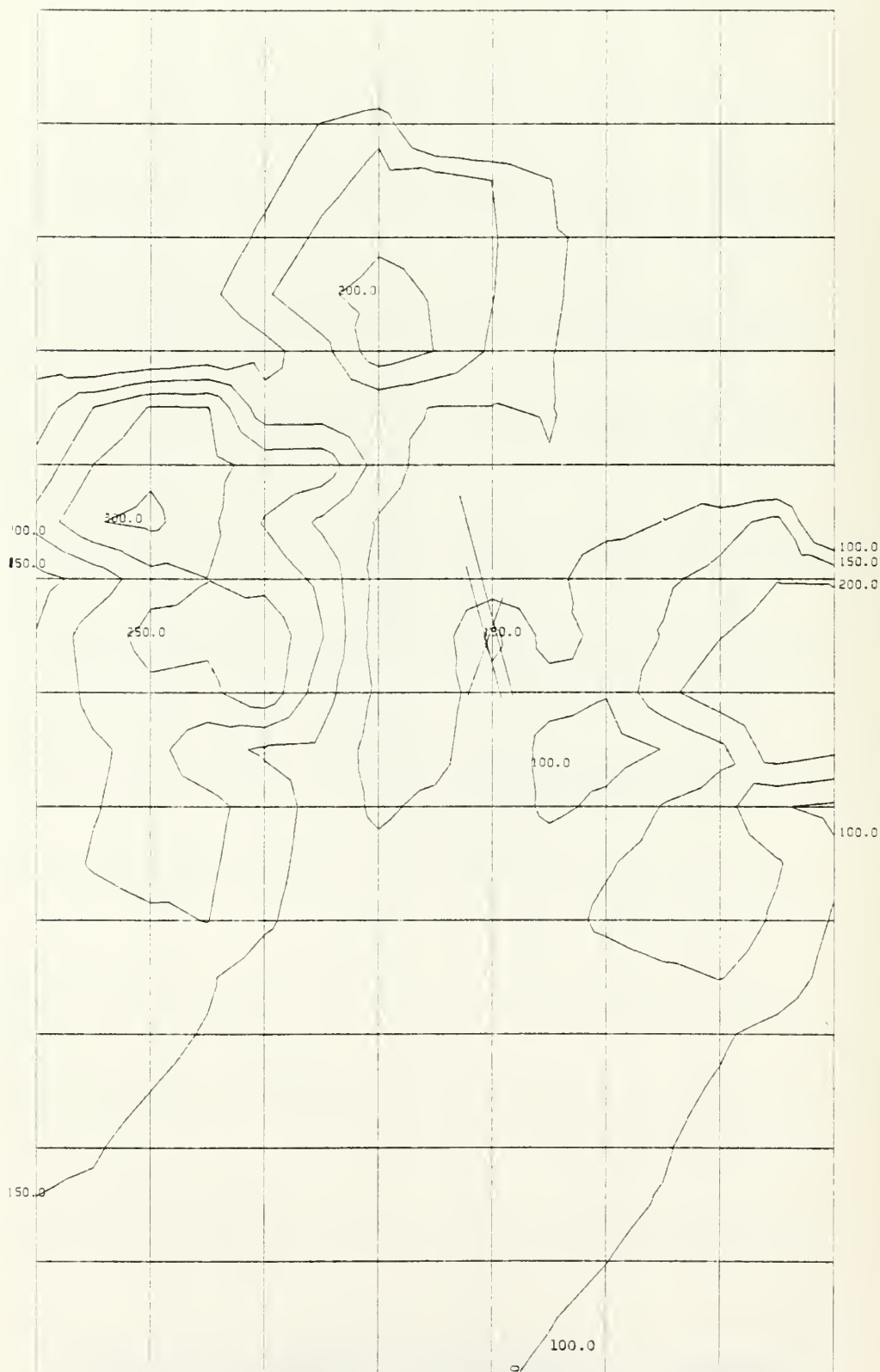




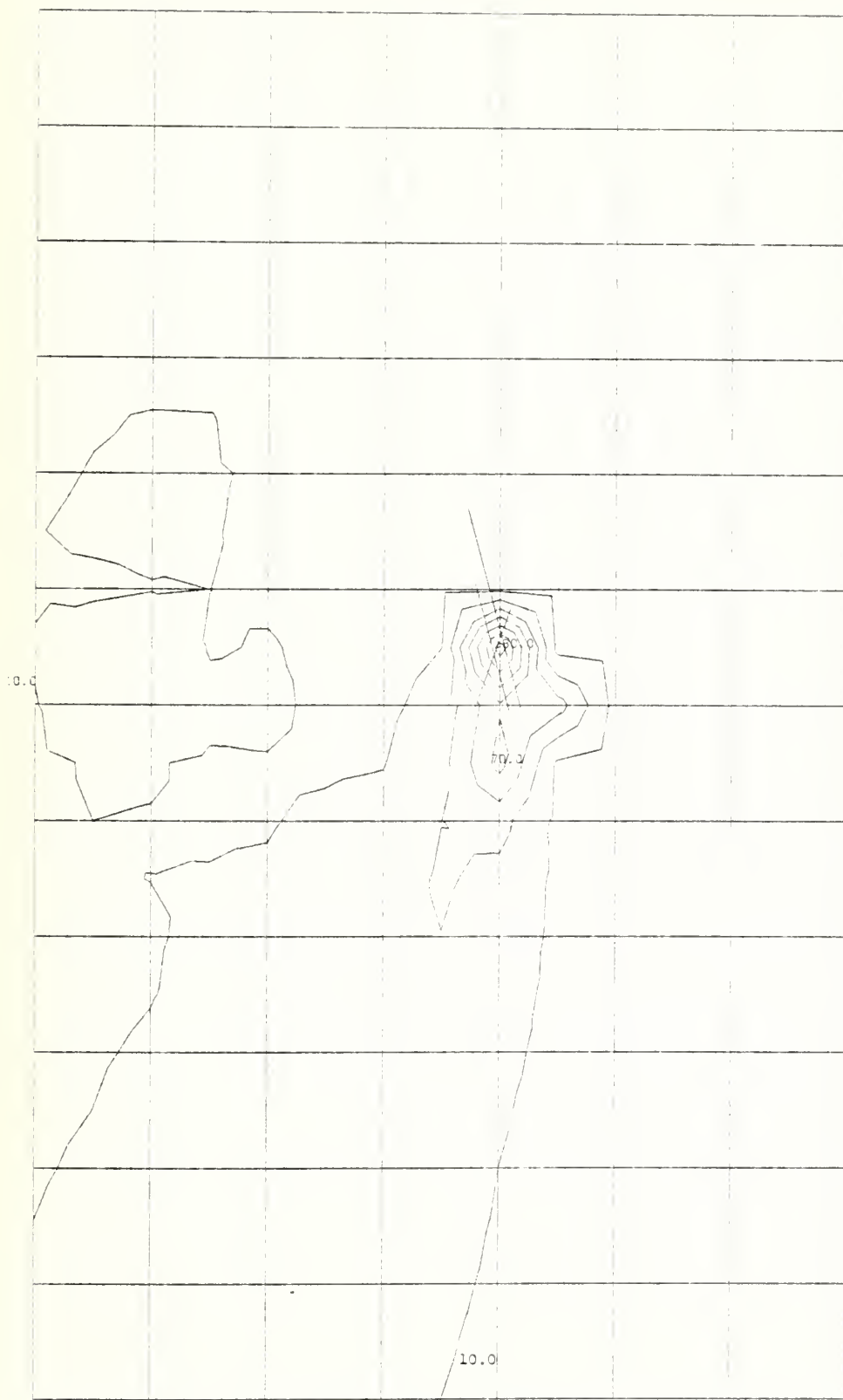
AIRBASE CO CONCENTRATION PROFILE (RUN NO. 1)  
(Scale =  $1 \mu\text{gm}/\text{m}^3$  per contour)



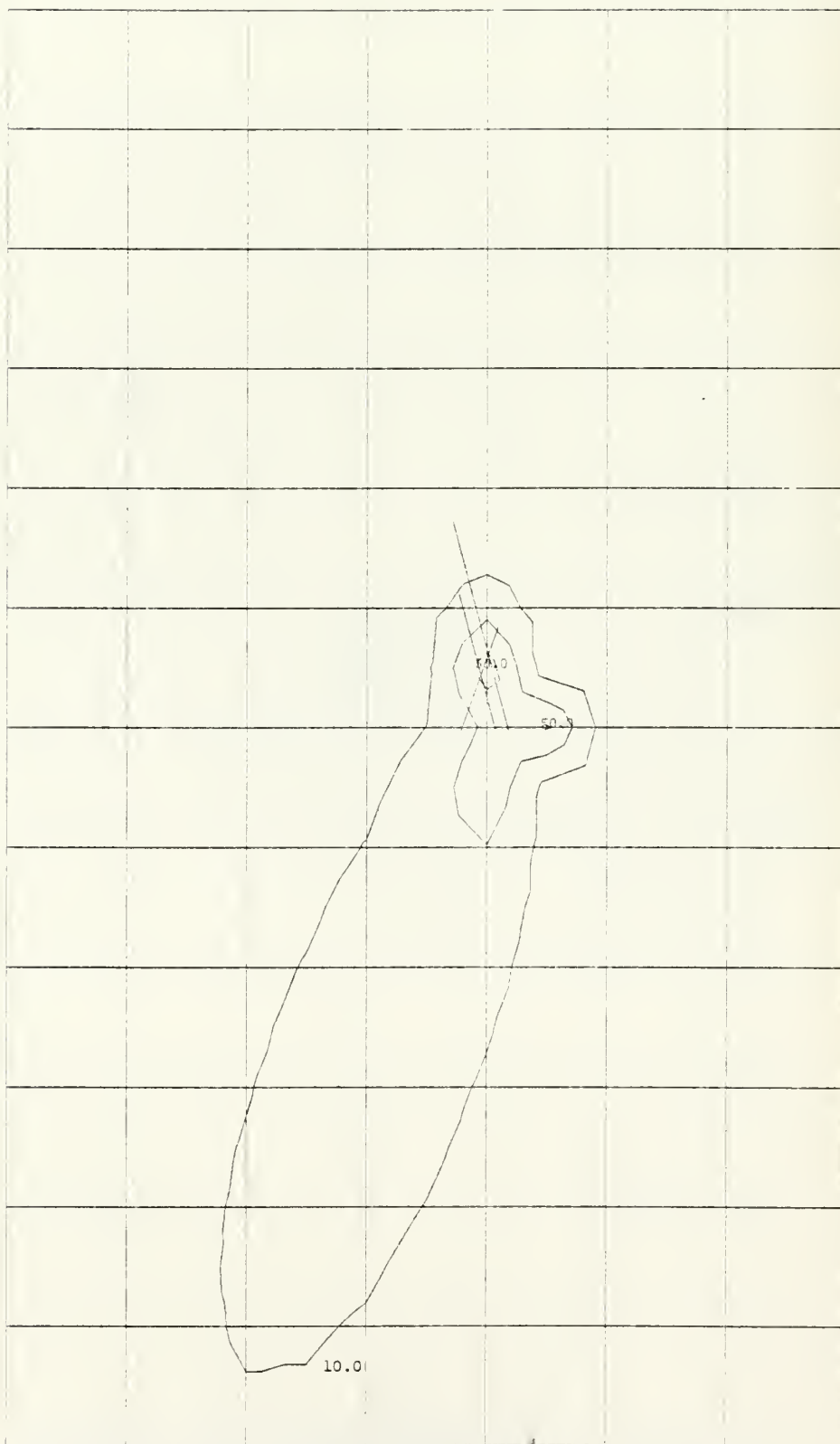
AIRBASE PT CONCENTRATION PROFILE (RUN NO. 1)  
(Scale = 1  $\mu\text{gm}/\text{m}^3$  per contour)



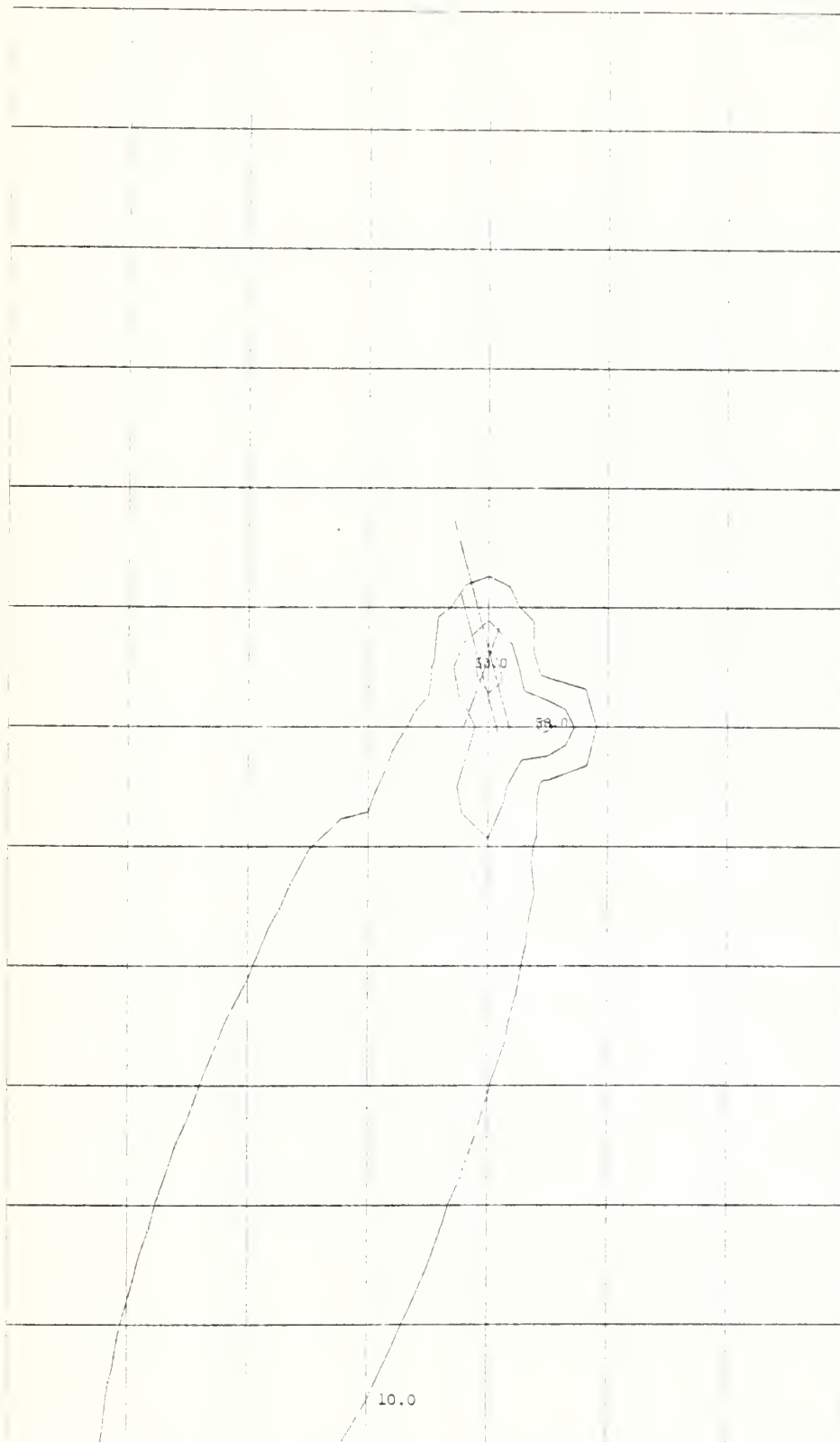
TOTAL CO CONCENTRATION PROFILE (RUN NO. 1)  
(Scale =  $50 \mu\text{gm}/\text{m}^3$  per contour)



TOTAL PT CONCENTRATION PROFILE (RUN NO. 1)  
(Scale =  $20 \mu\text{gm}/\text{m}^3$  per contour)

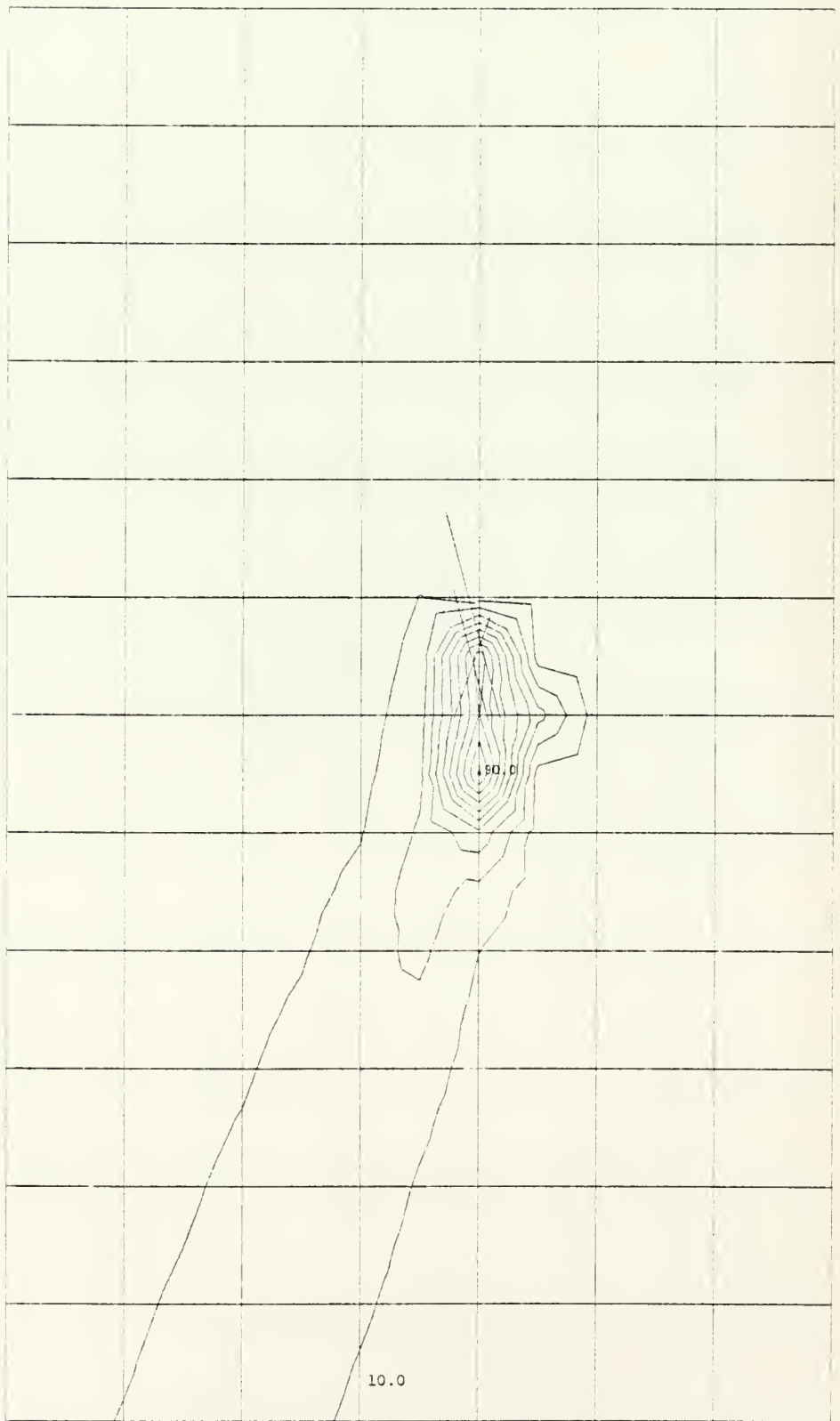


AIRCRAFT CO CONCENTRATION PROFILE (RUN NO. 2)

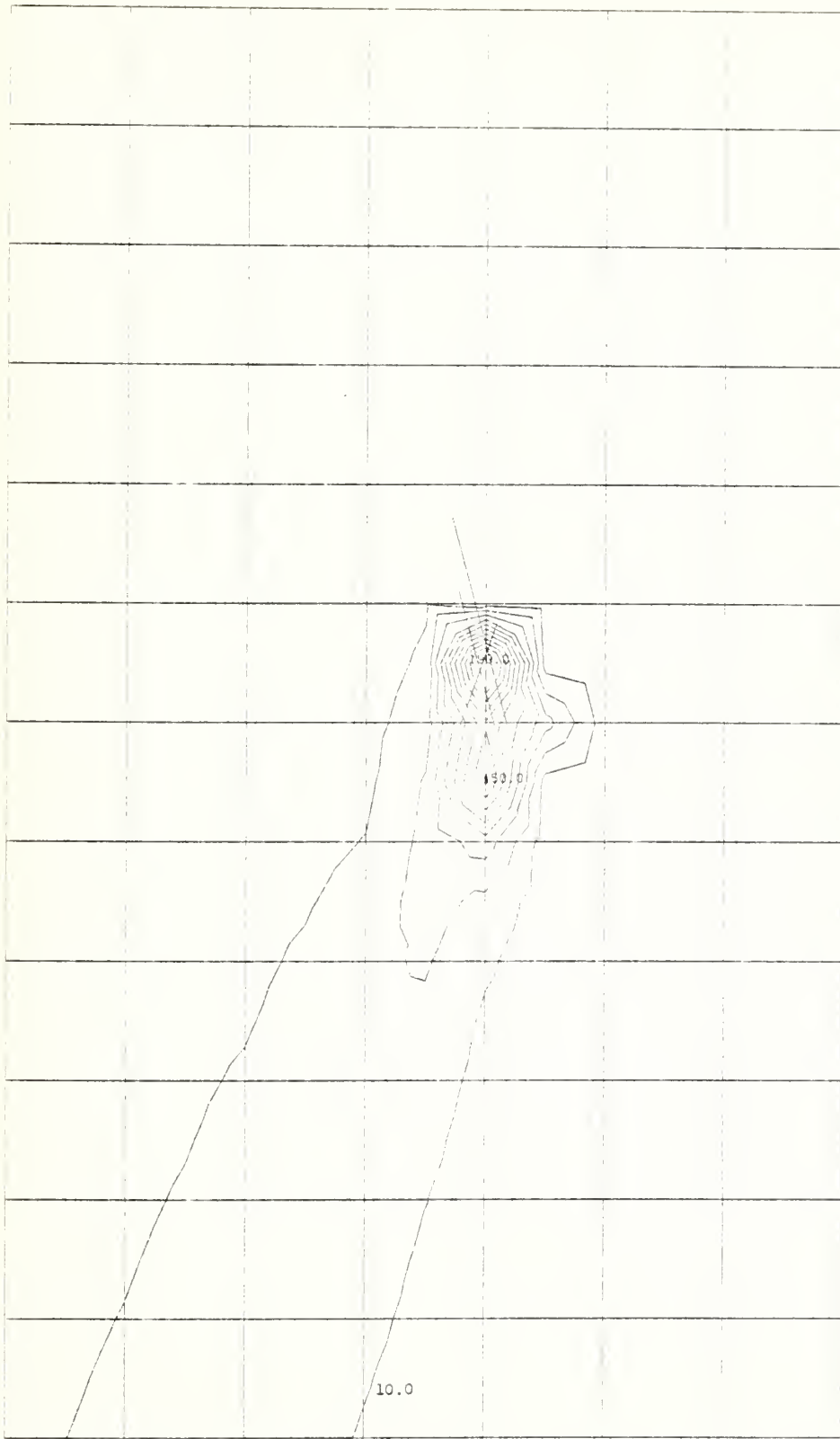


AIRCRAFT PT CONCENTRATION PROFILE (RUN NO. 2)

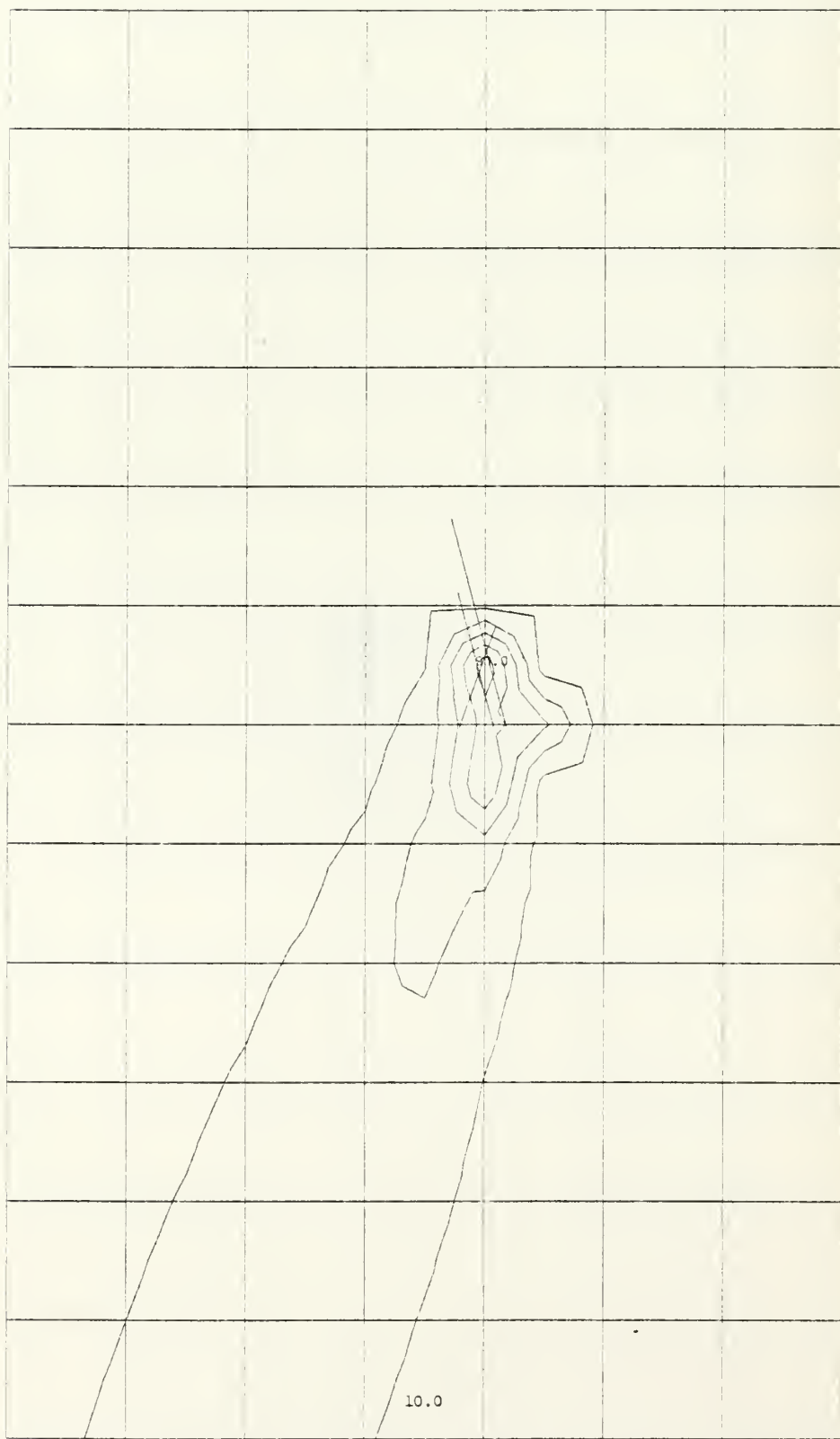




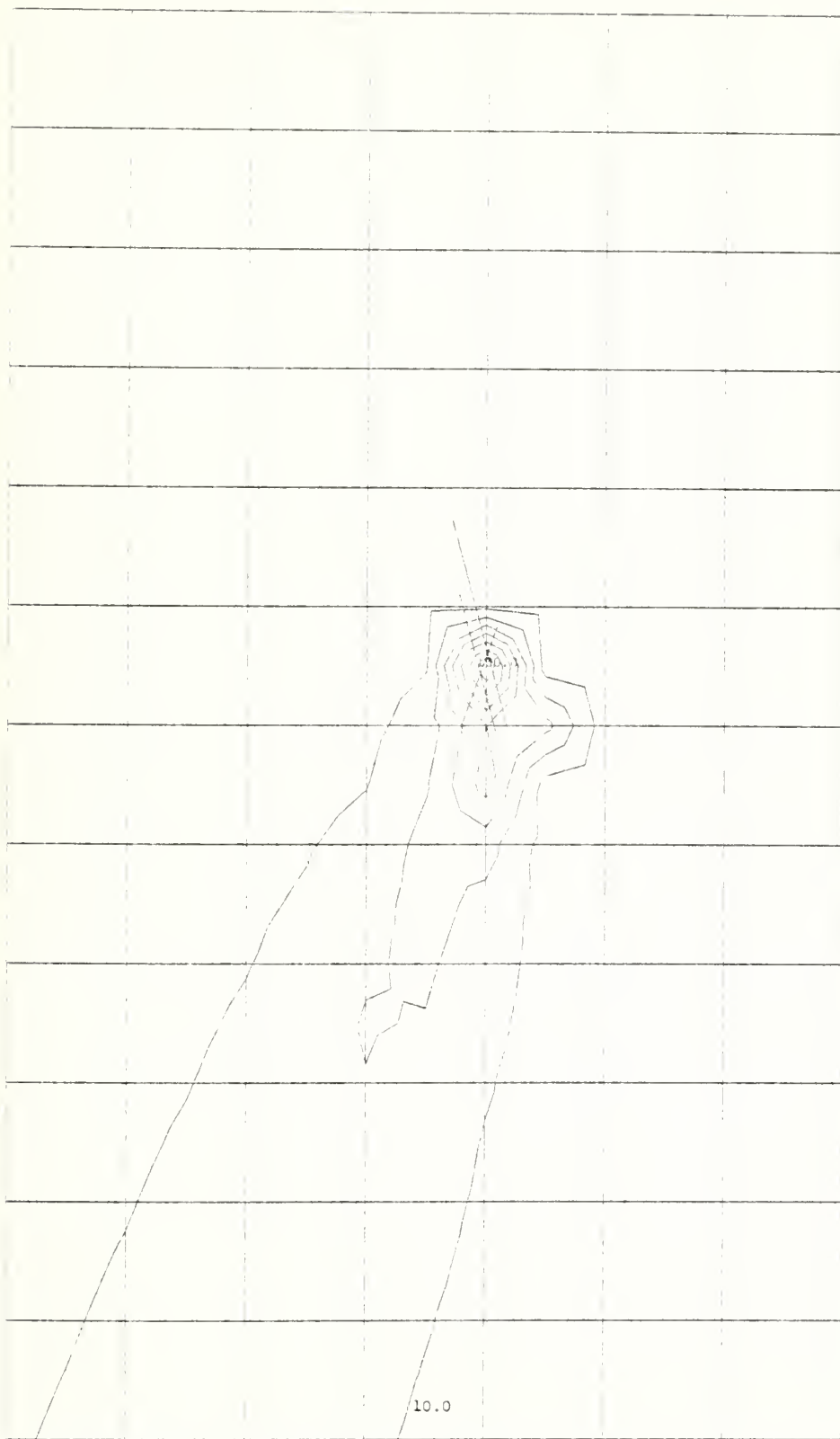
AIRCRAFT CO CONCENTRATION PROFILE (RUN NO. 3)



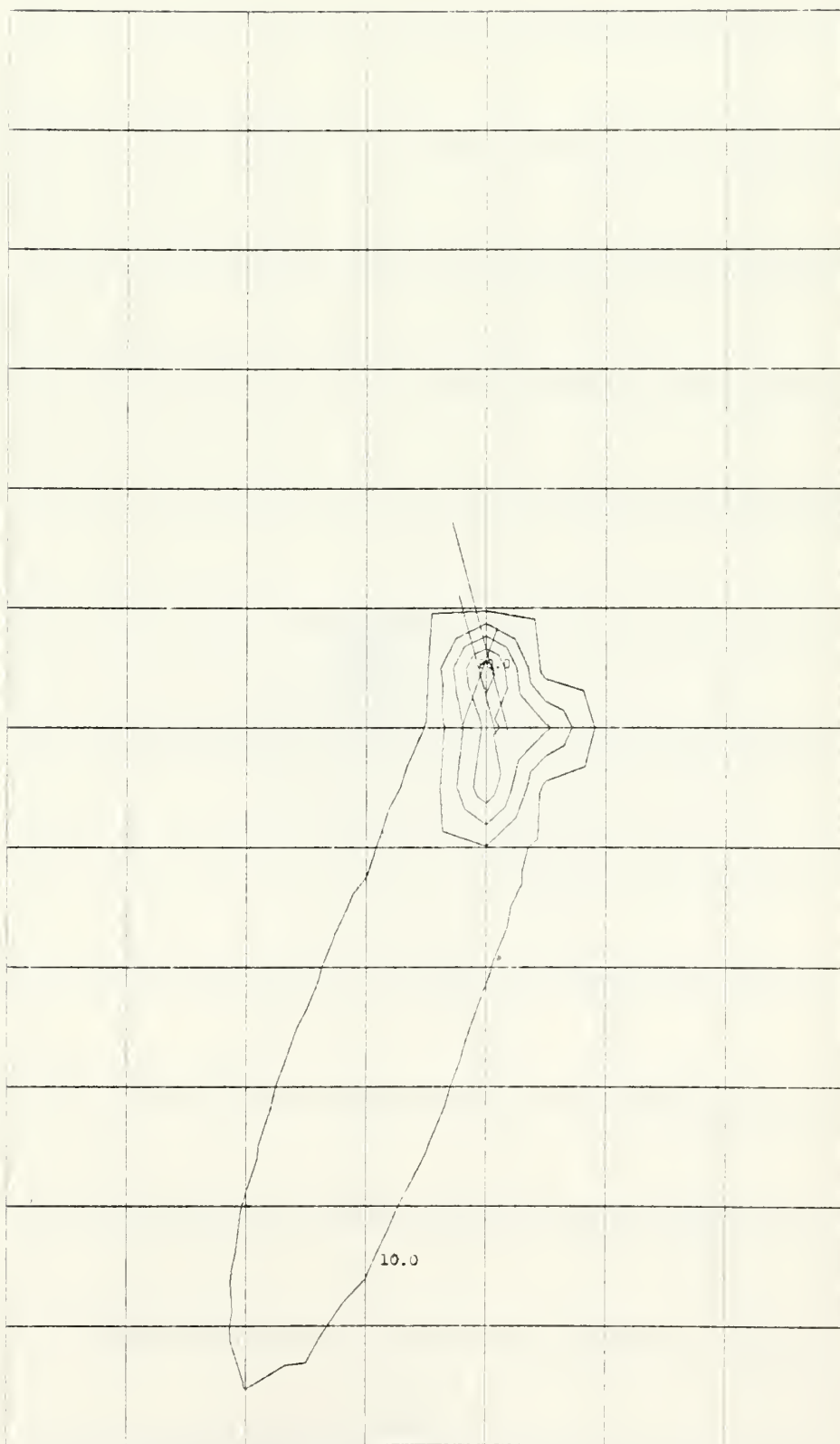
AIRCRAFT PT CONCENTRATION PROFILE (RUN NO. 3)



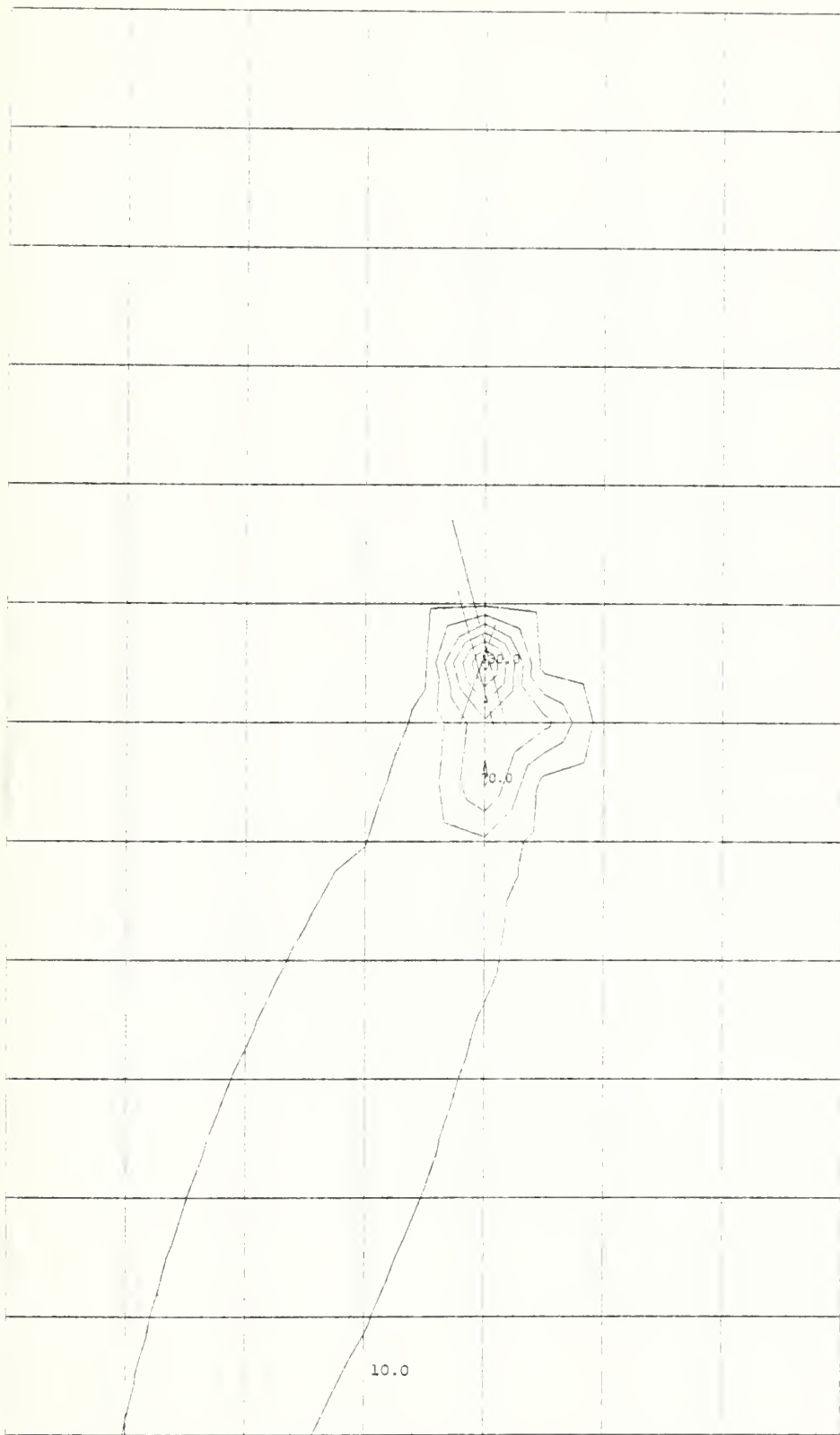
AIRCRAFT CO CONCENTRATION PROFILE (RUN NO. 4)



AIRCRAFT PT CONCENTRATION PROFILE (RUN NO. 4)

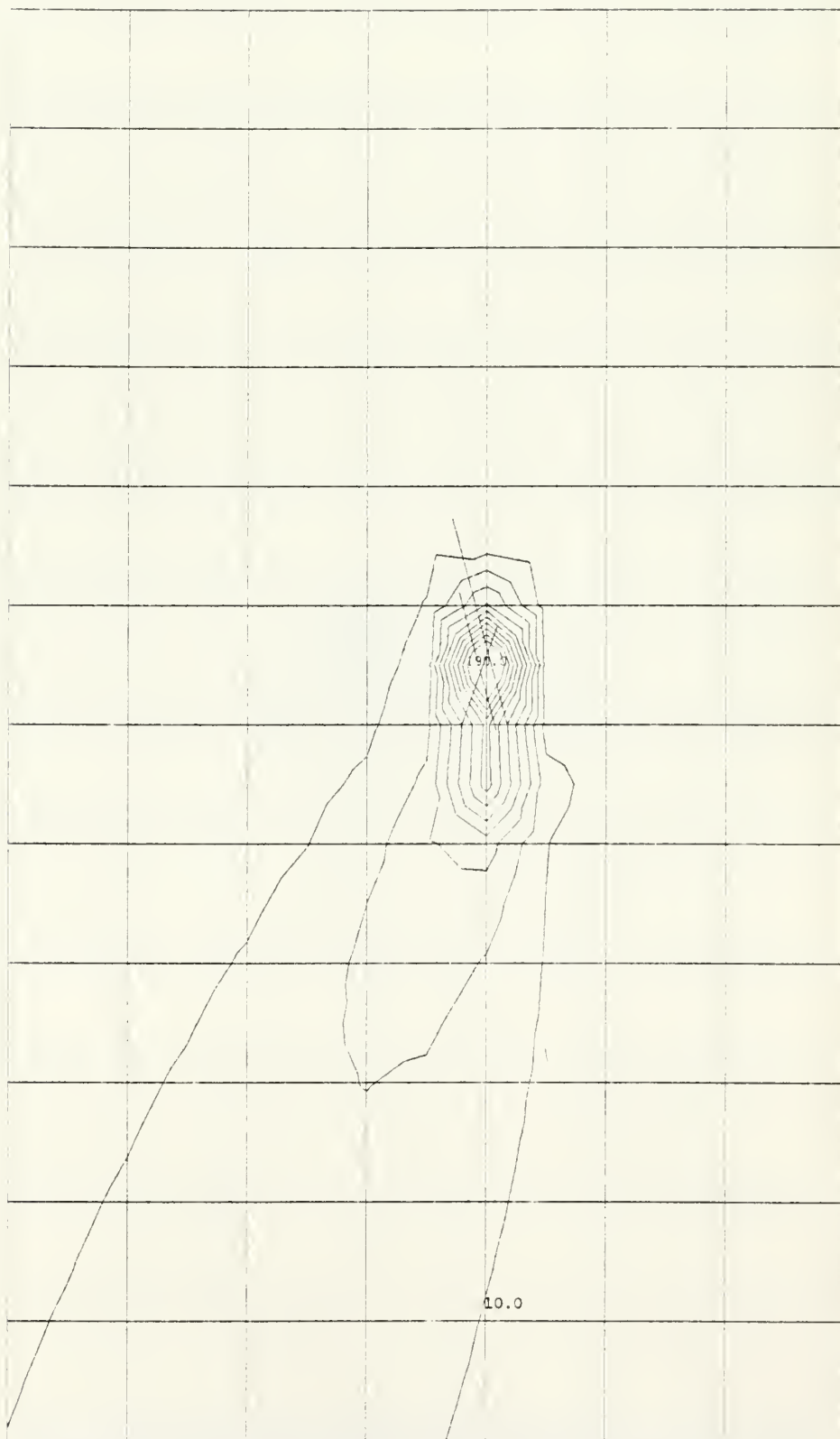


AIRCRAFT CO CONCENTRATION PROFILE (RUN NO. 5)

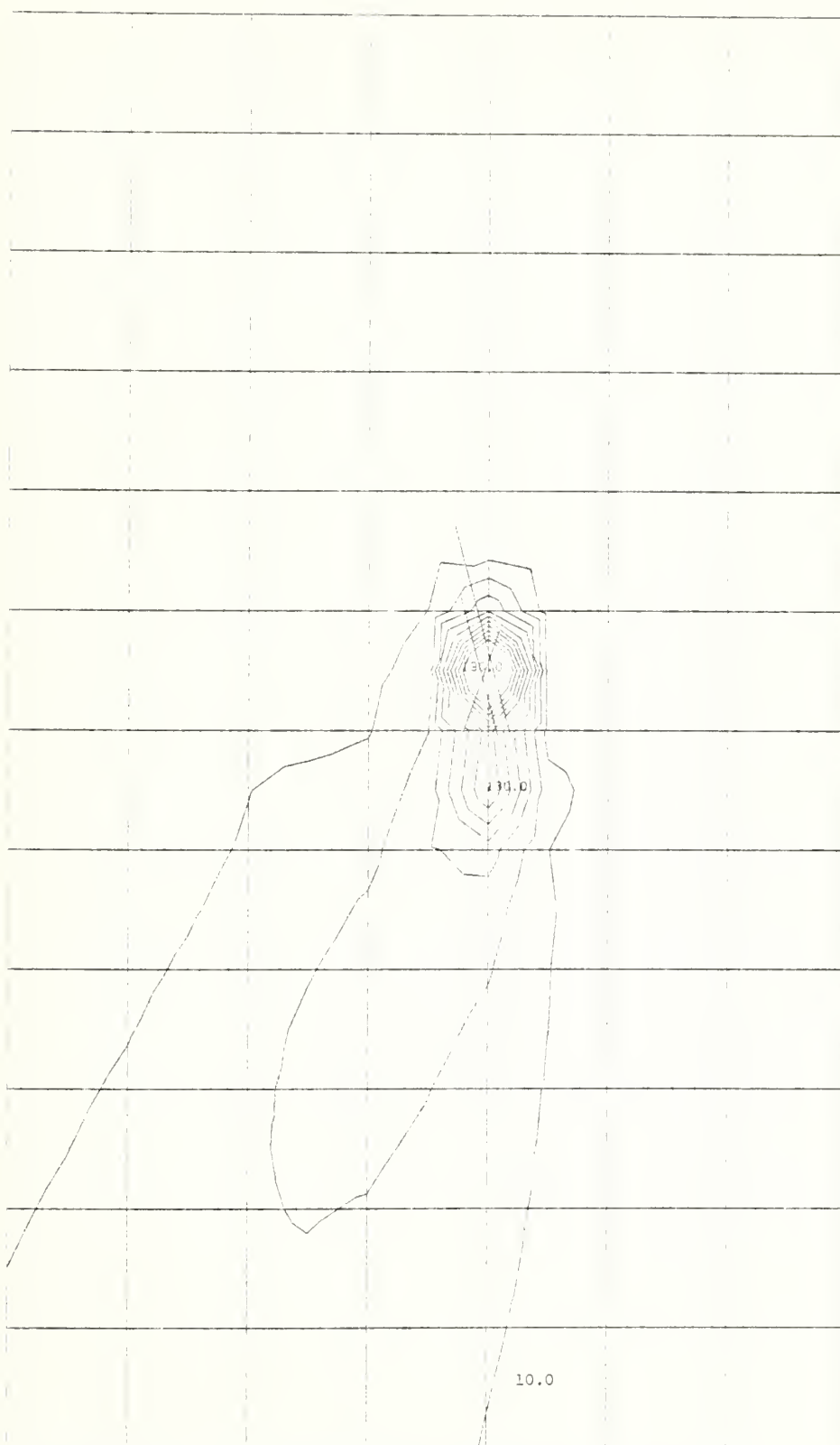


AIRCRAFT PT CONCENTRATION PROFILE (RUN NO. 5)

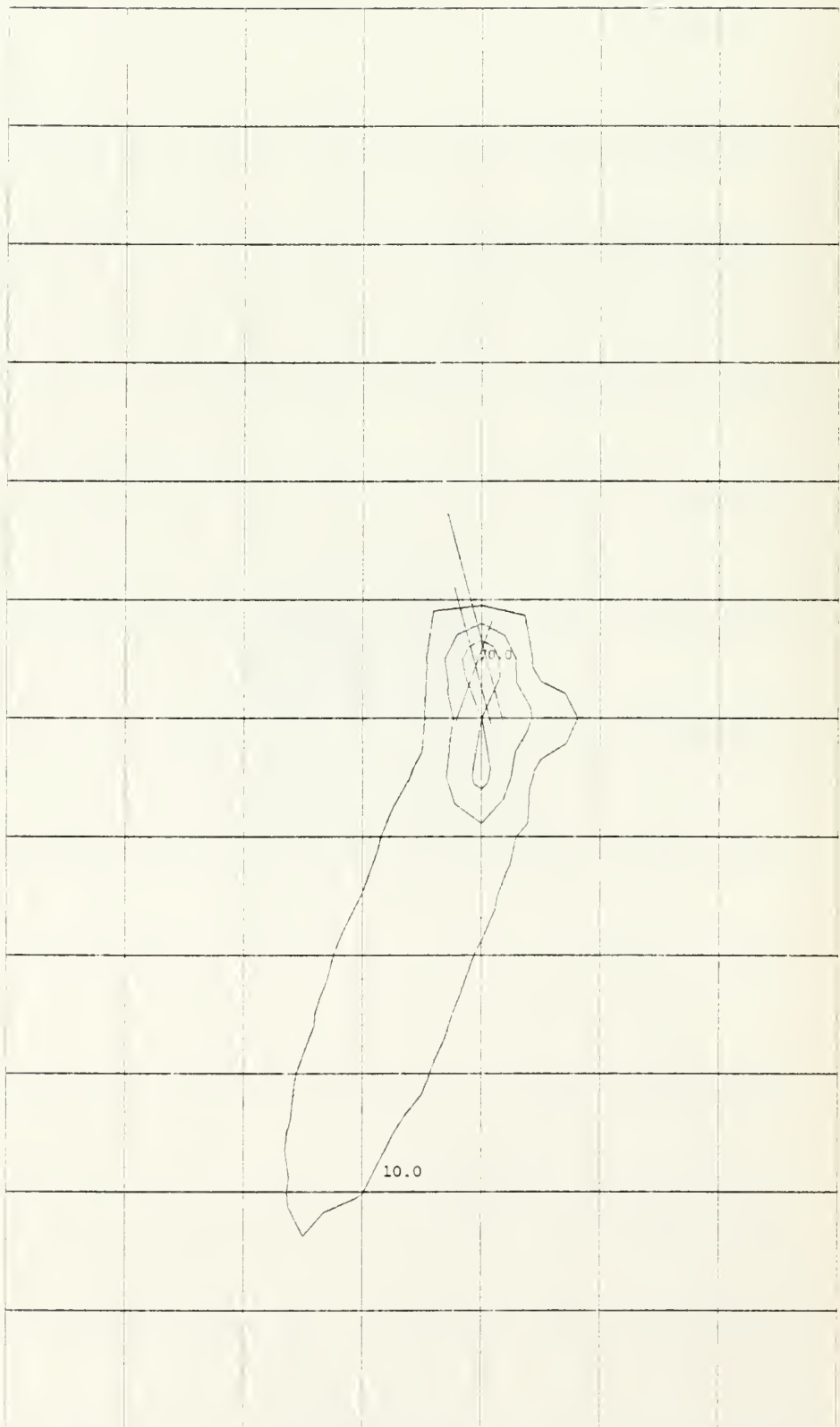




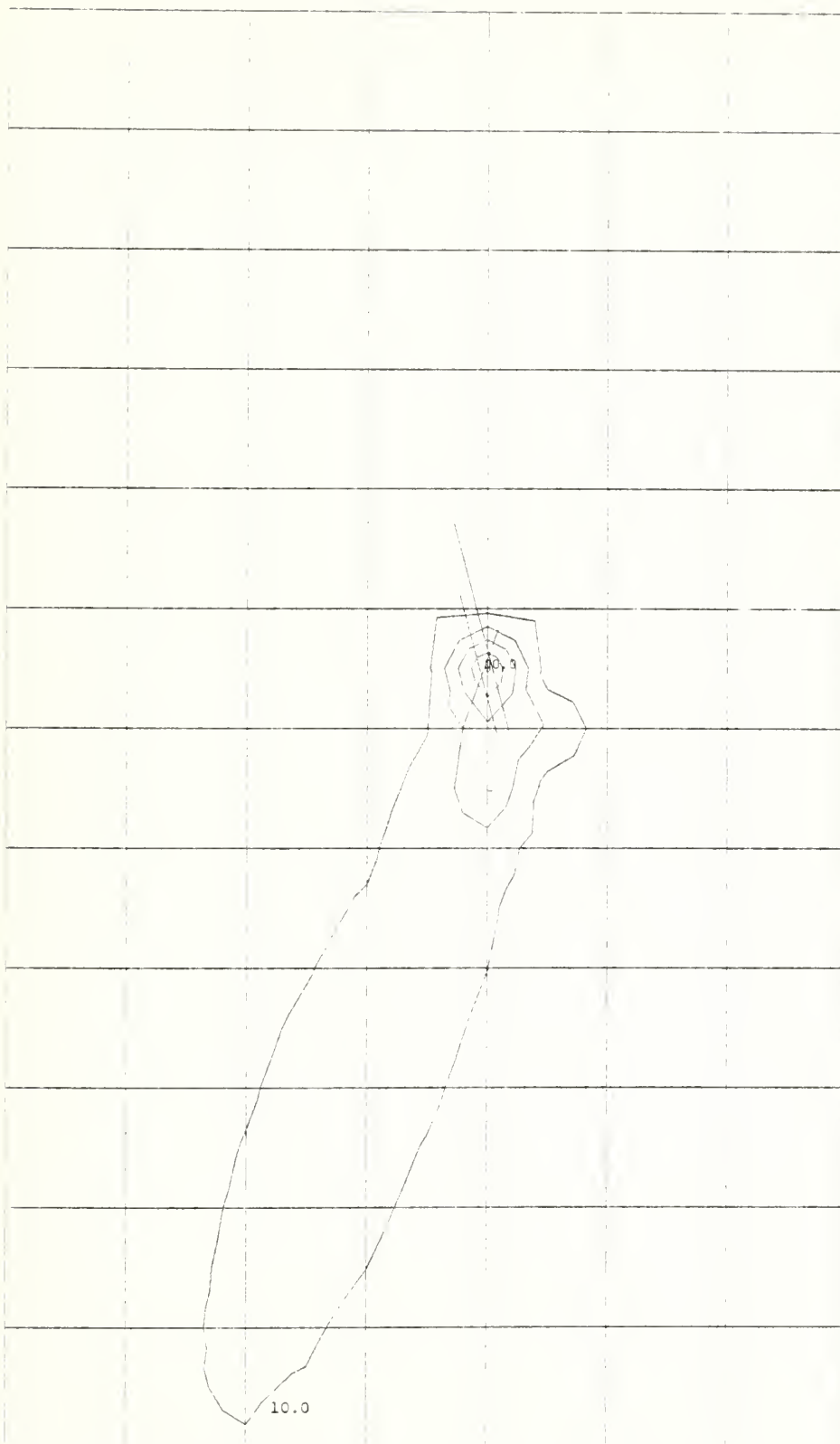
AIRCRAFT CO CONCENTRATION PROFILE (RUN NO. 6)



AIRCRAFT PT CONCENTRATION PROFILE (RUN NO. 6)



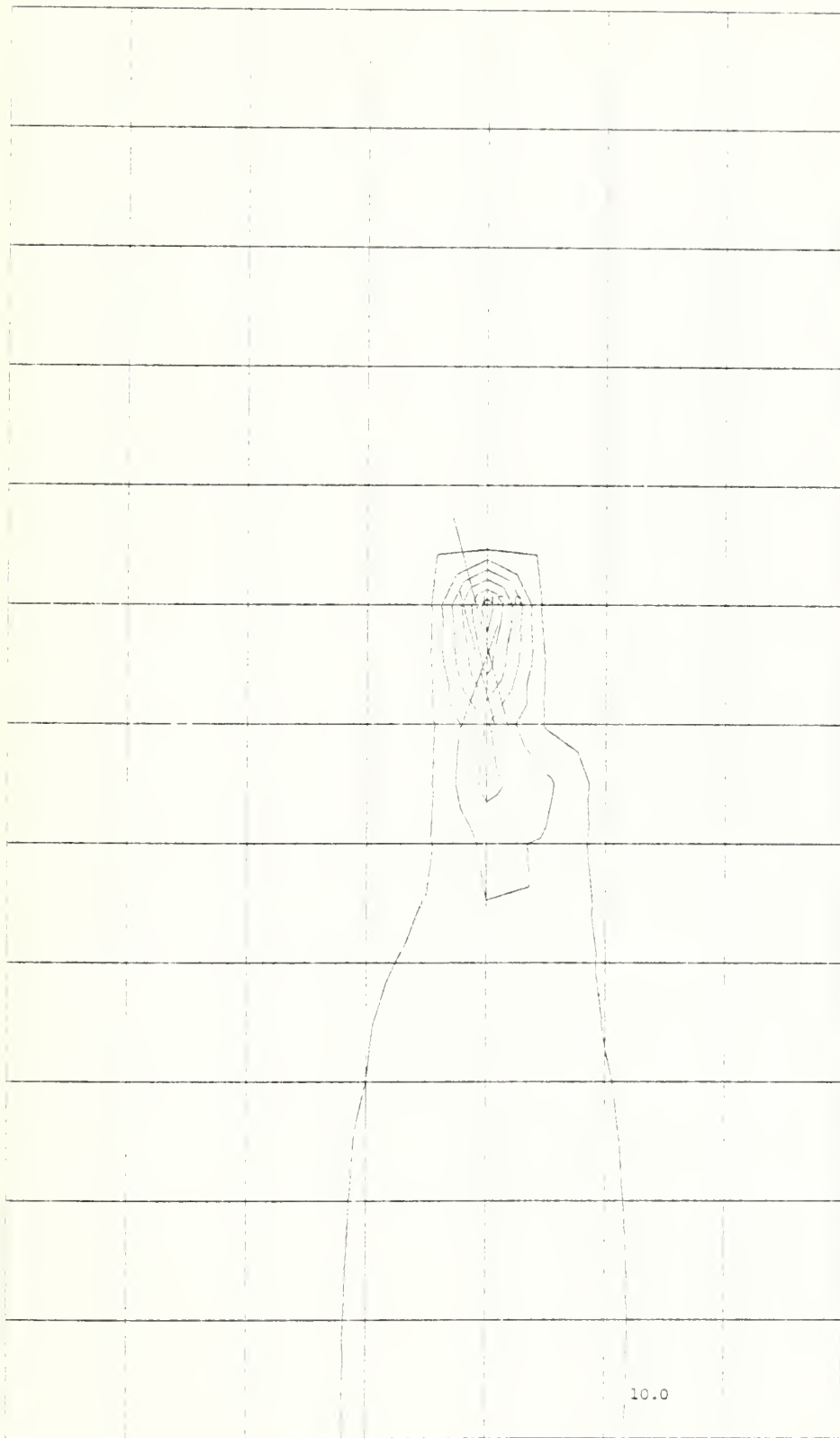
AIRCRAFT CO CONCENTRATION PROFILE (RUN NO. 7)



AIRCRAFT PT CONCENTRATION PROFILE (RUN NO. 7)

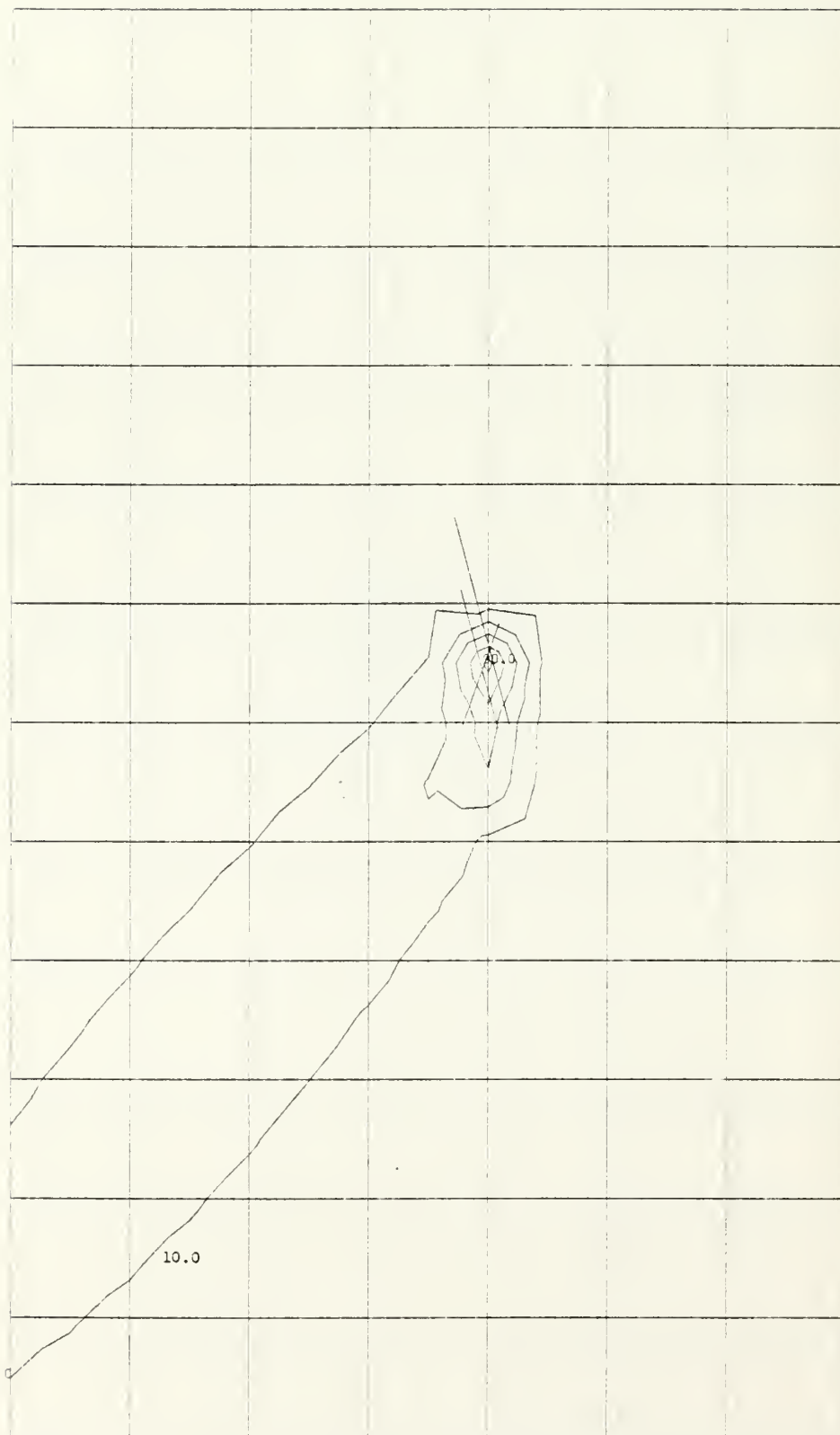


AIRCRAFT CO CONCENTRATION PROFILE (RUN NO. 8)

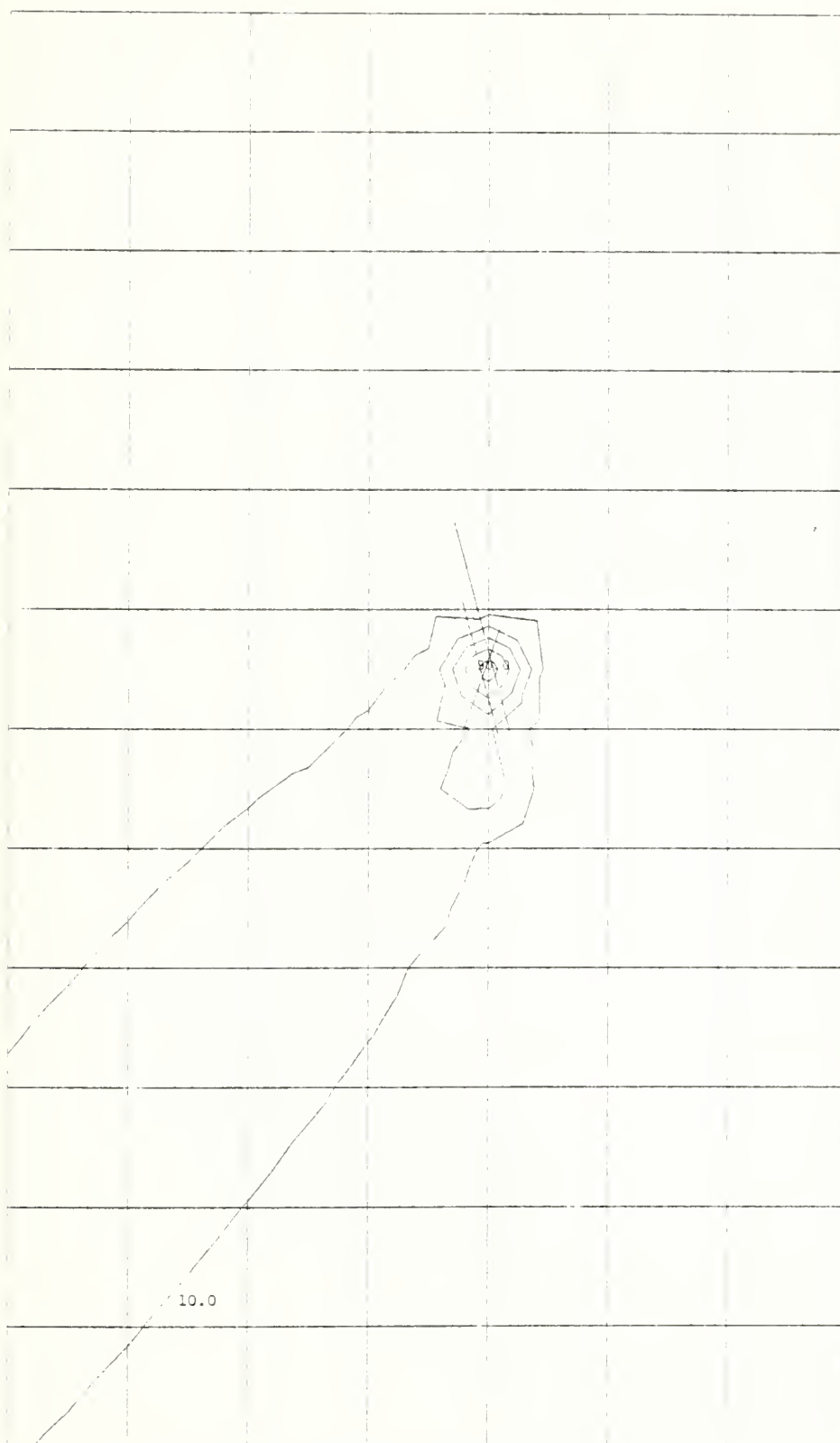


AIRCRAFT PT CONCENTRATION PROFILE (RUN NO. 8)



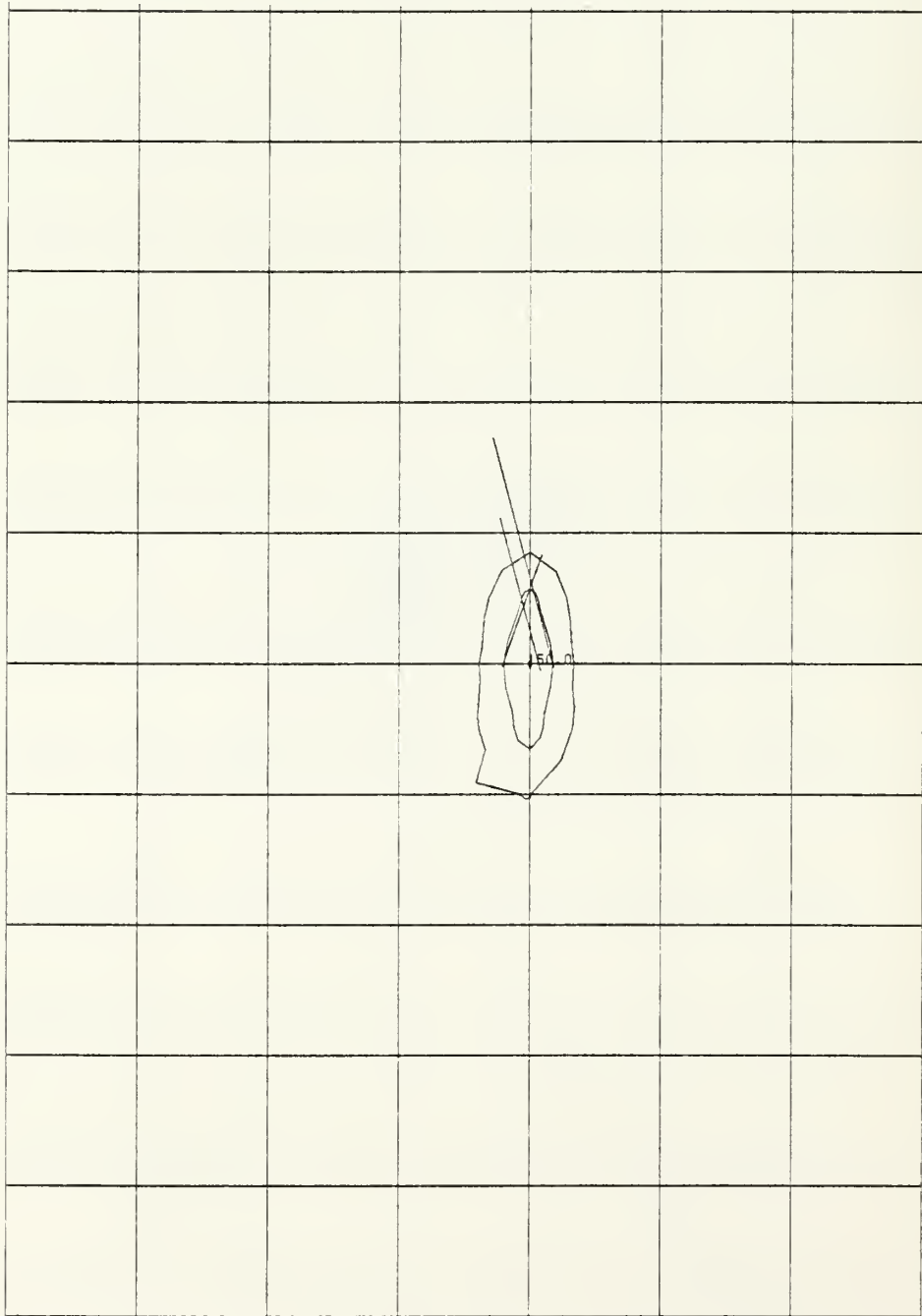


AIRCRAFT CO CONCENTRATION PROFILE (RUN NO. 9)

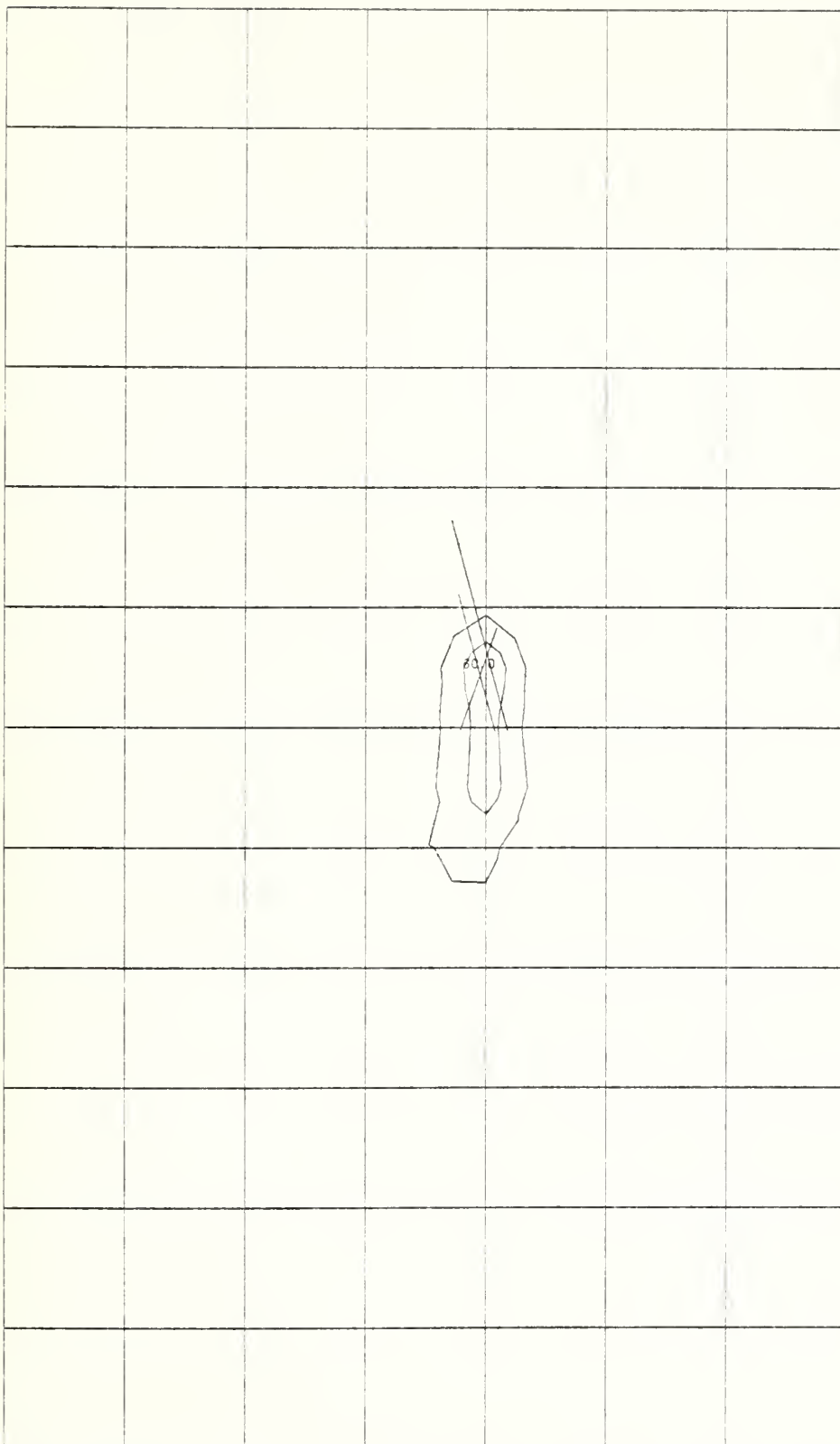


AIRCRAFT PT CONCENTRATION PROFILE (RUN NO. 9)

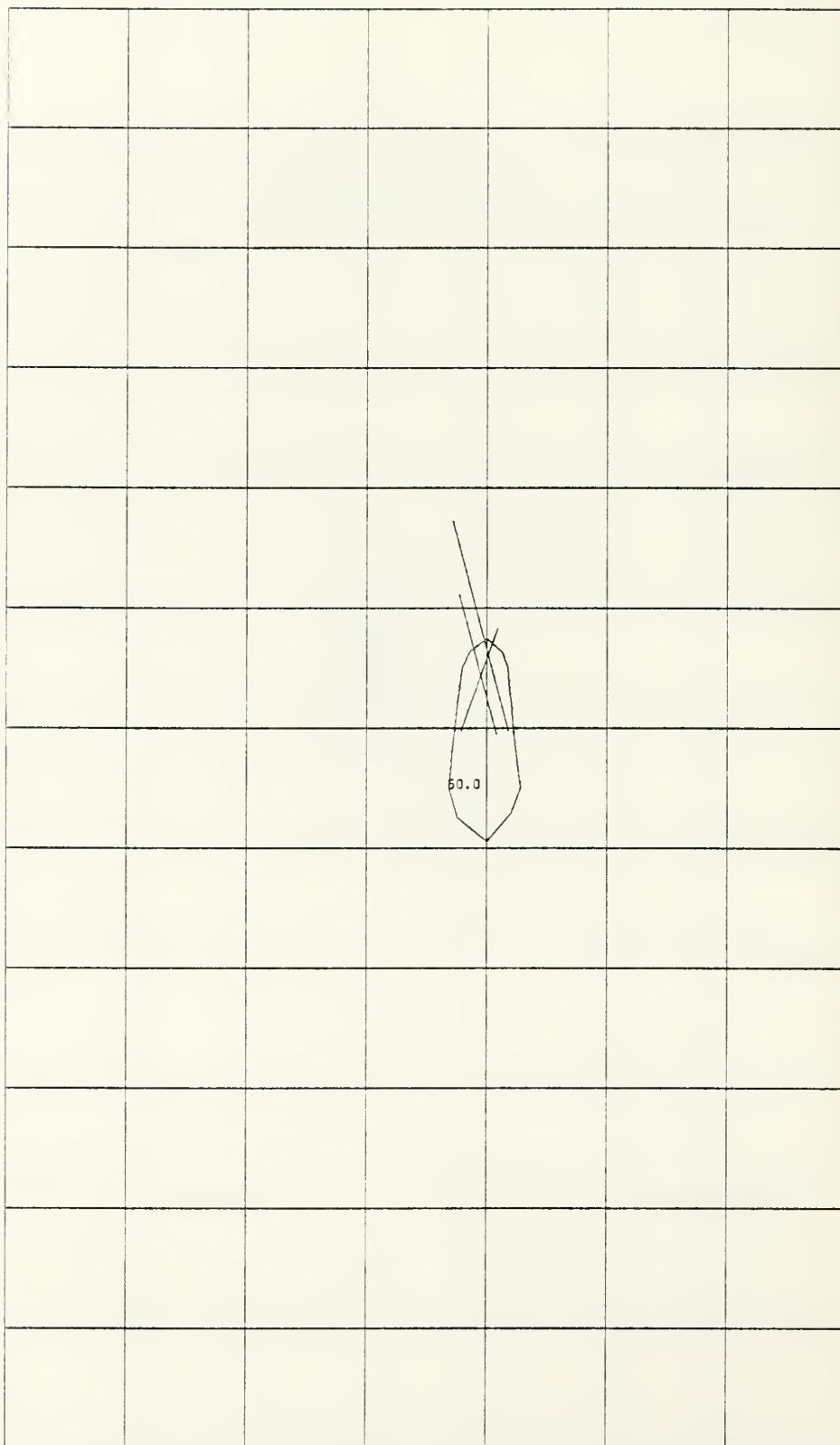
APPENDIX C  
CO AND PT CONCENTRATION PROFILES FROM AIRCRAFT SOURCES  
(INTENSIVE STUDY)



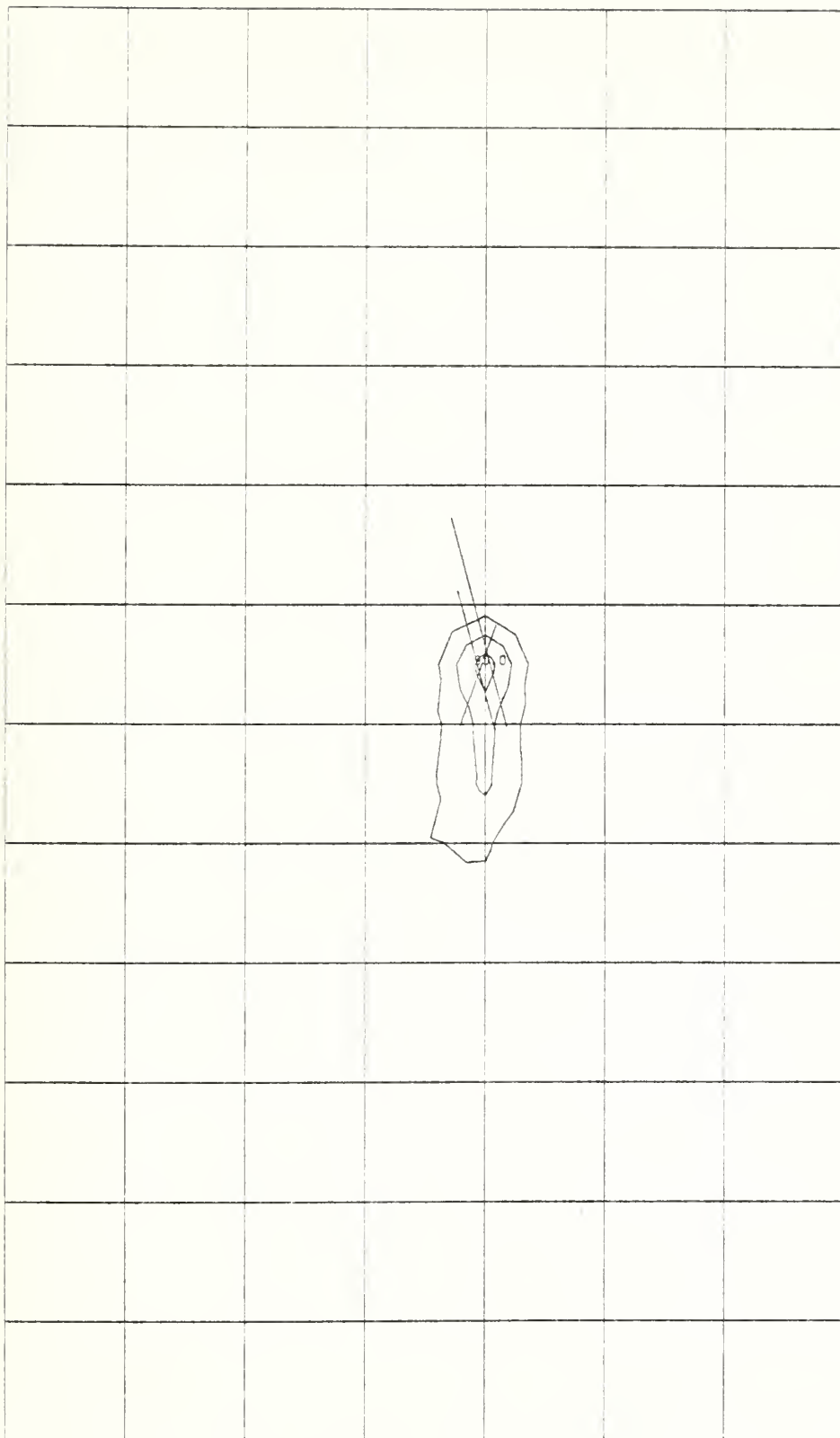
AIRCRAFT CO CONCENTRATION PROFILE (1 AUG 1300-1400)  
INCREMENTED FROM 50.0  
(Scale = 50  $\mu\text{gm}/\text{m}^3$  per contour)



AIRCRAFT PT CONCENTRATION PROFILE (1 AUG 1300-1400)  
INCREMENTED FROM 30.0  
(Scale =  $30 \mu\text{gm}/\text{m}^3$  per contour)

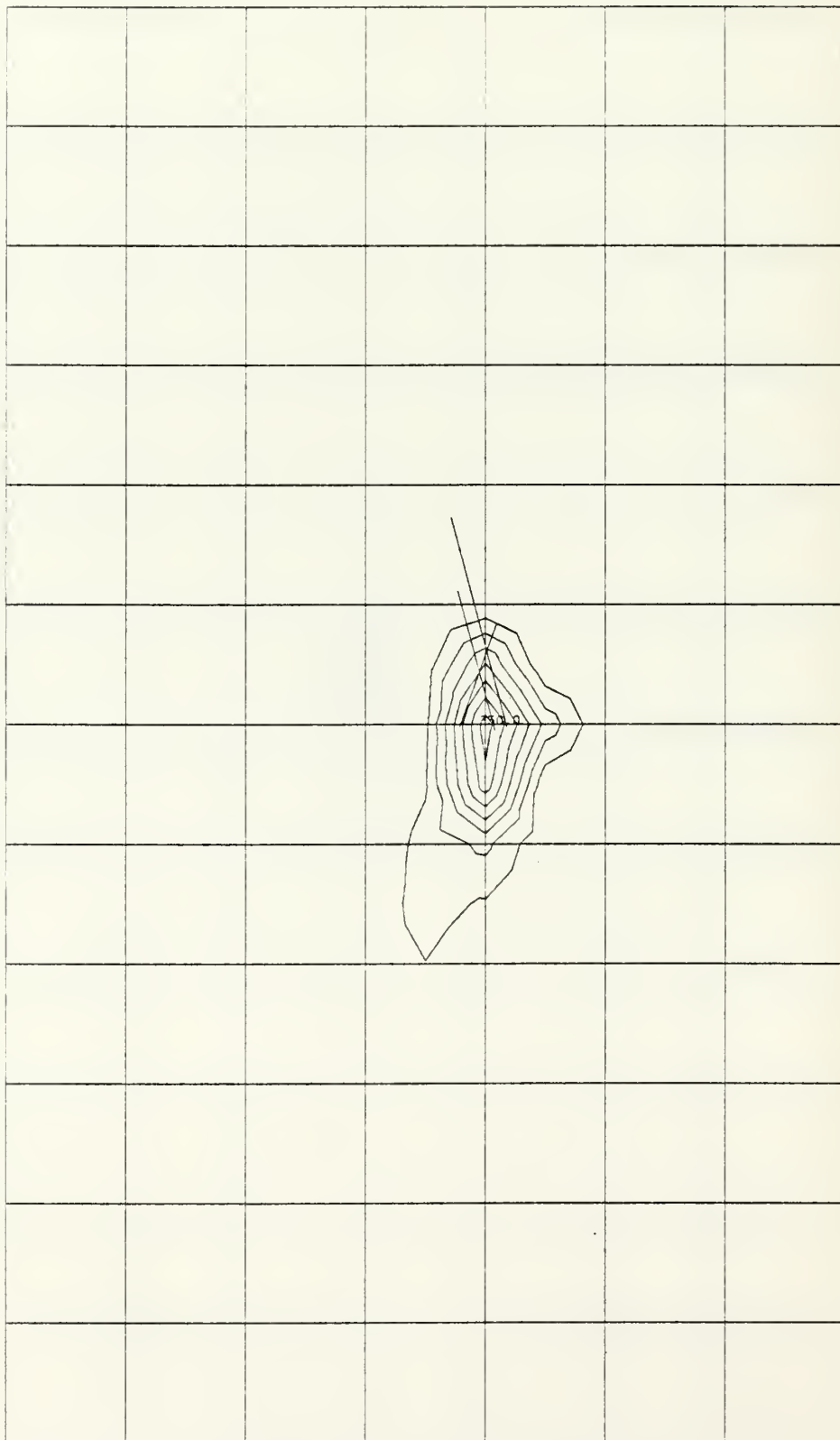


AIRCRAFT CO CONCENTRATION PROFILE (1 AUG 1400-1500)  
INCREMENTED FROM 50.0



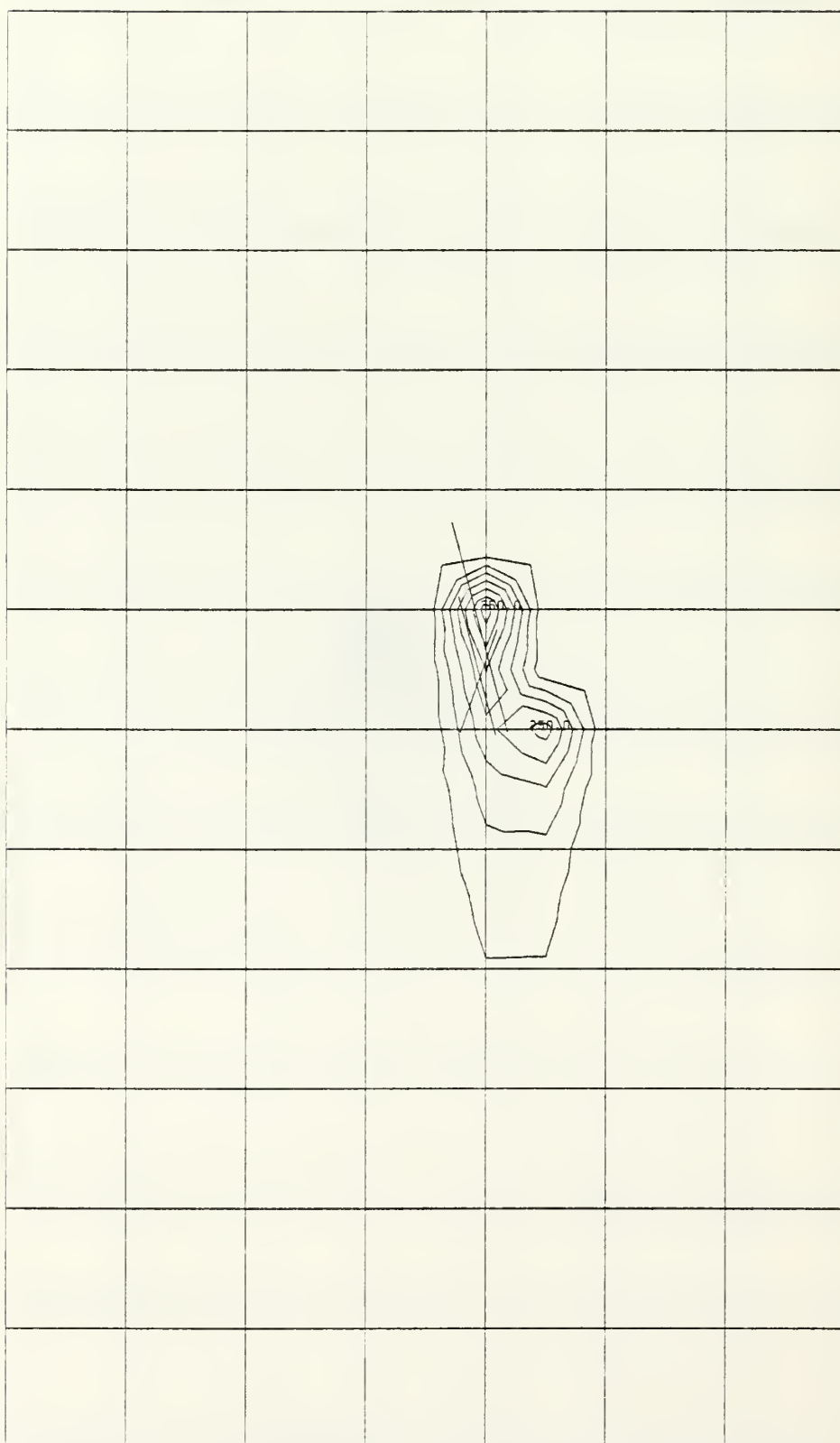
AIRCRAFT PT CONCENTRATION PROFILE (1 AUG 1400-1500)  
INCREMENTED FROM 30.0



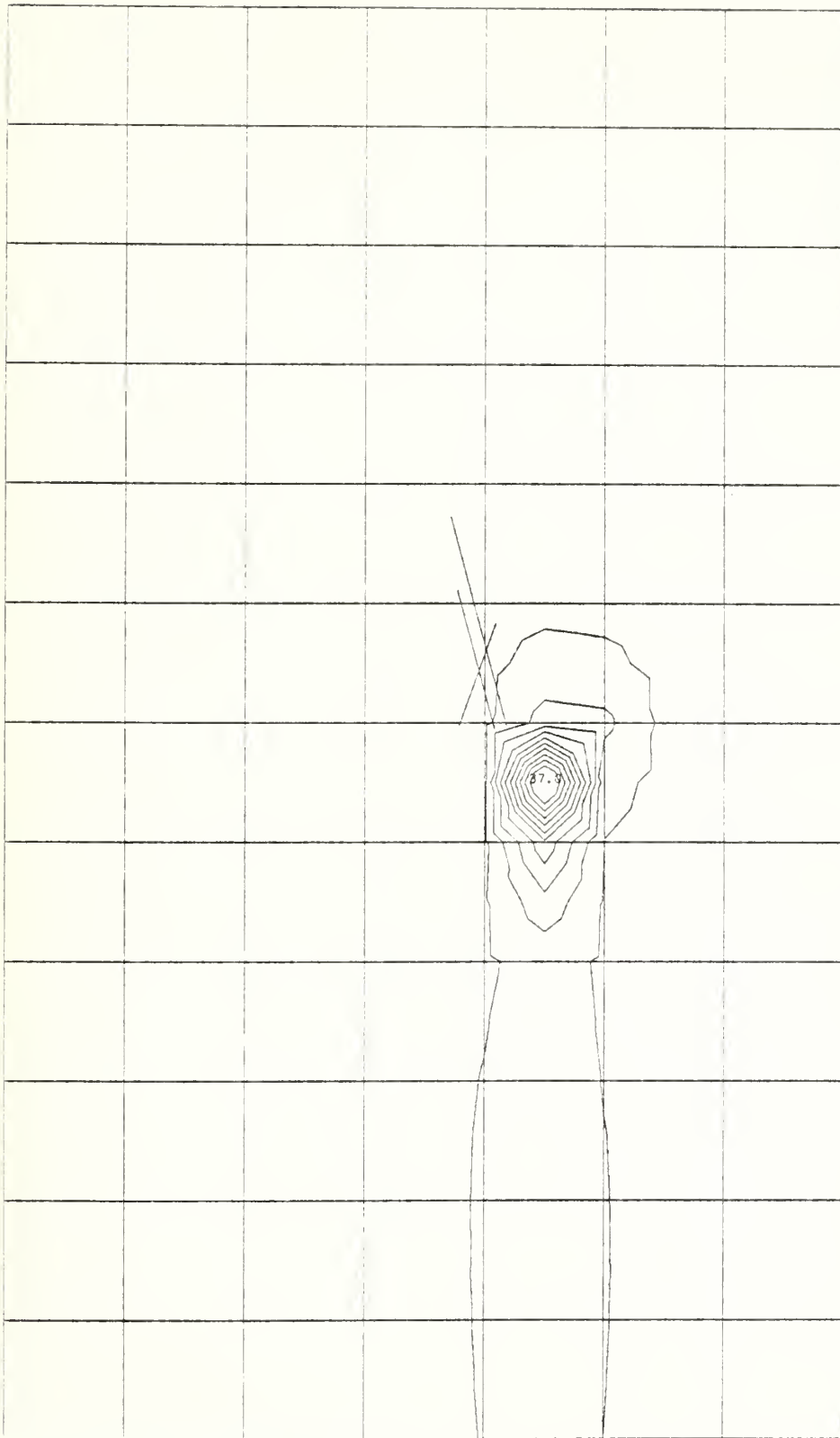


AIRCRAFT CO CONCENTRATION PROFILE (2 AUG 1400-1500)  
INCREMENTED FROM 50.0

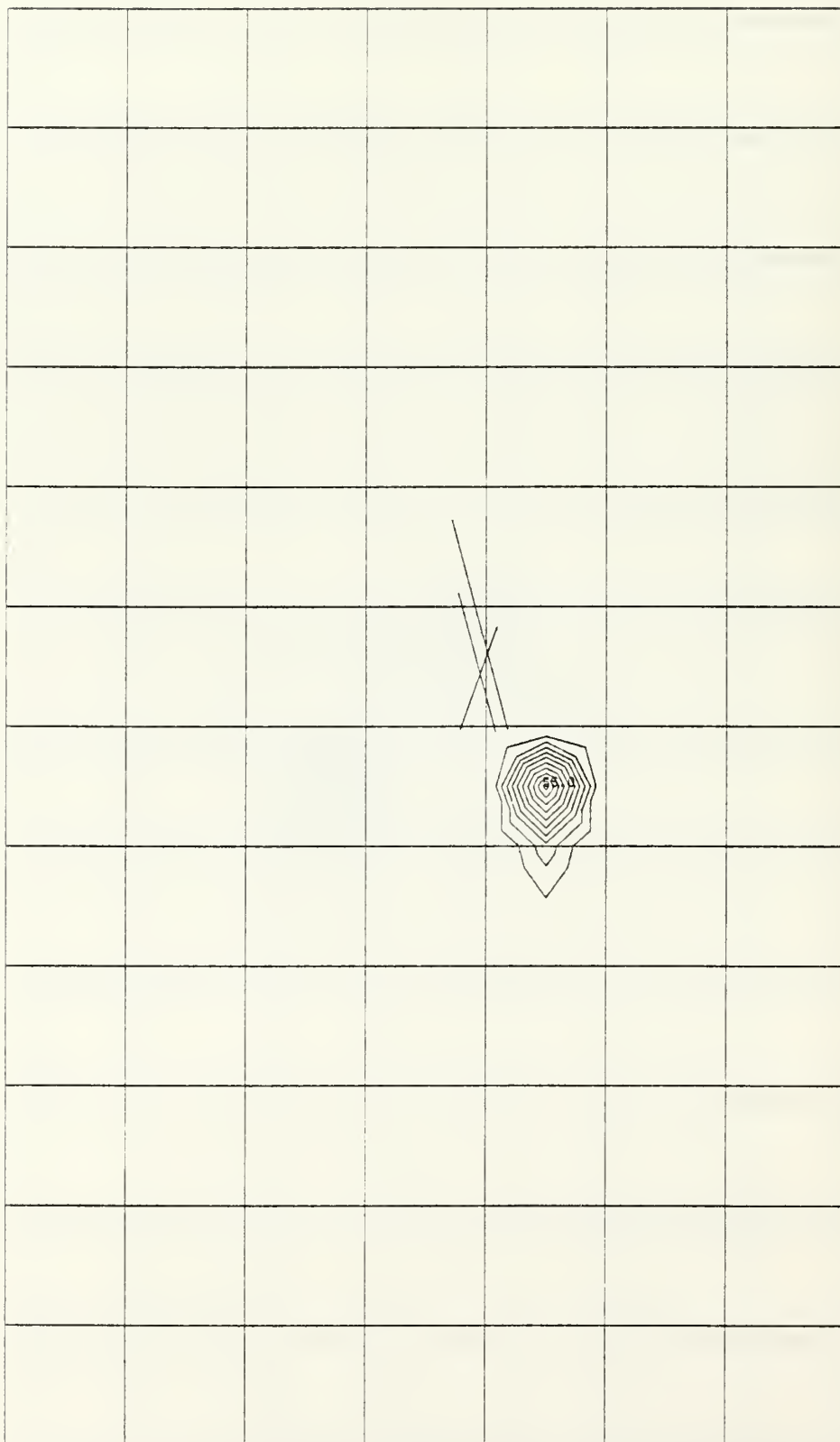




AIRCRAFT CO CONCENTRATION PROFILE (2 AUG 1500-1600)  
INCREMENTED FROM 50.0



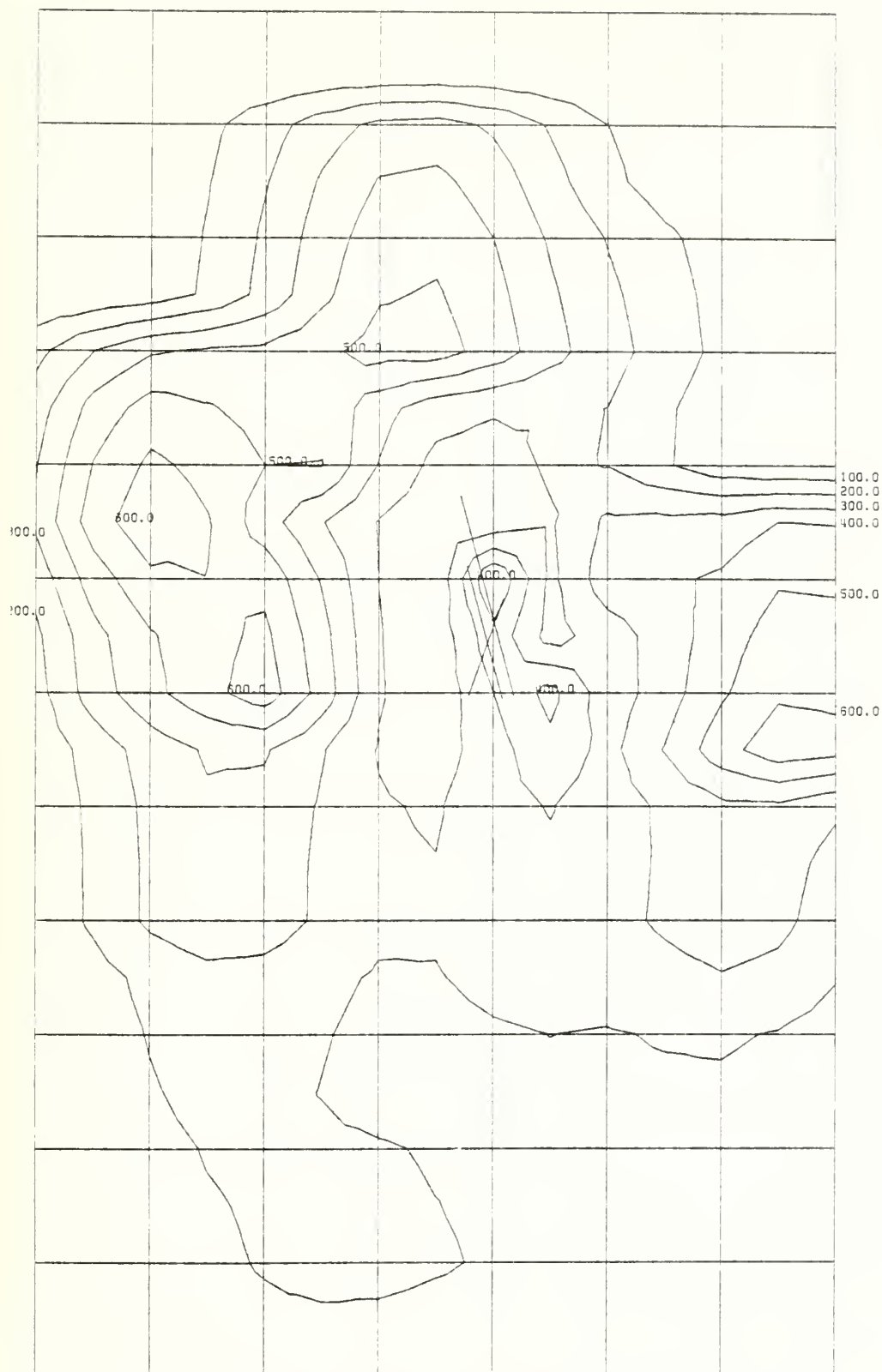
AIRBASE CO CONCENTRATION PROFILE (2 AUG 1500-1600)  
INCREMENTED FROM 1.0  
(Scale =  $4 \mu\text{gm}/\text{m}^3$  per contour)



AIRBASE PT CONCENTRATION PROFILE (2 AUG 1500-1600)

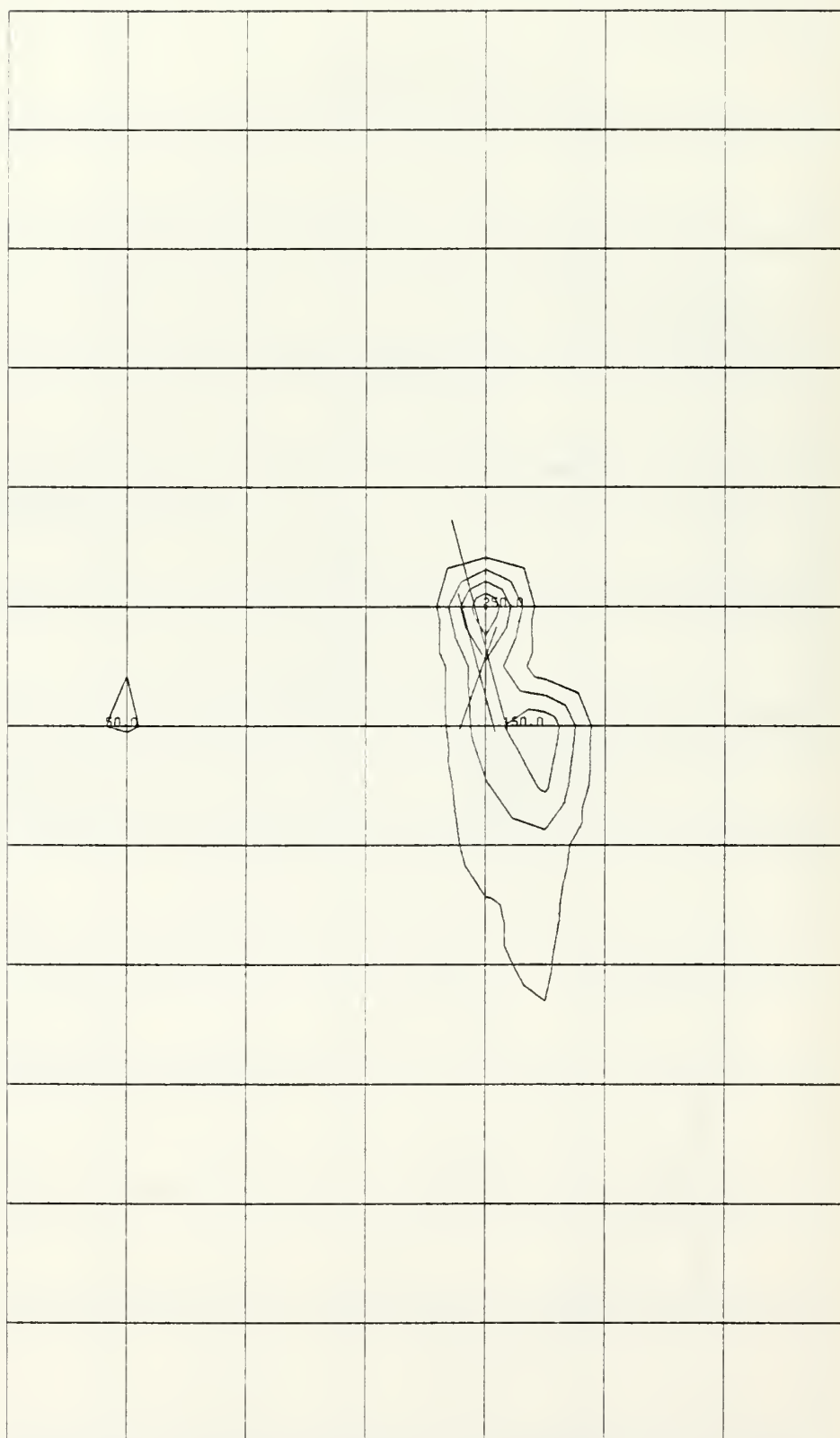
INCREMENTED FROM 10.0

(Scale =  $5 \mu\text{gm}/\text{m}^3$  per contour)

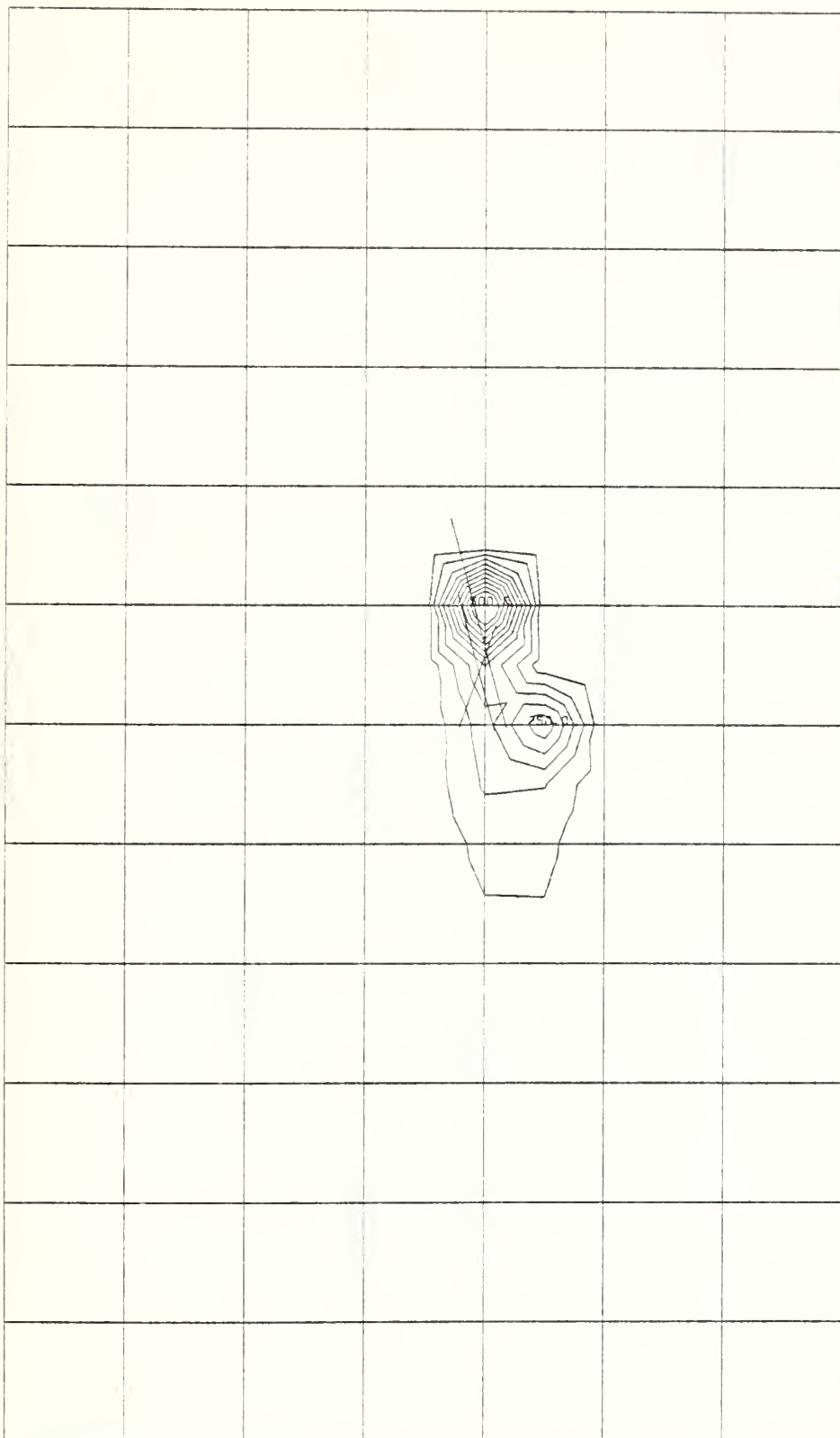


TOTAL CO CONCENTRATION PROFILE (2 AUG 1500-1600)  
INCREMENTED FROM 100.0  
(Scale = 100  $\mu\text{gm}/\text{m}^3$  per contour)

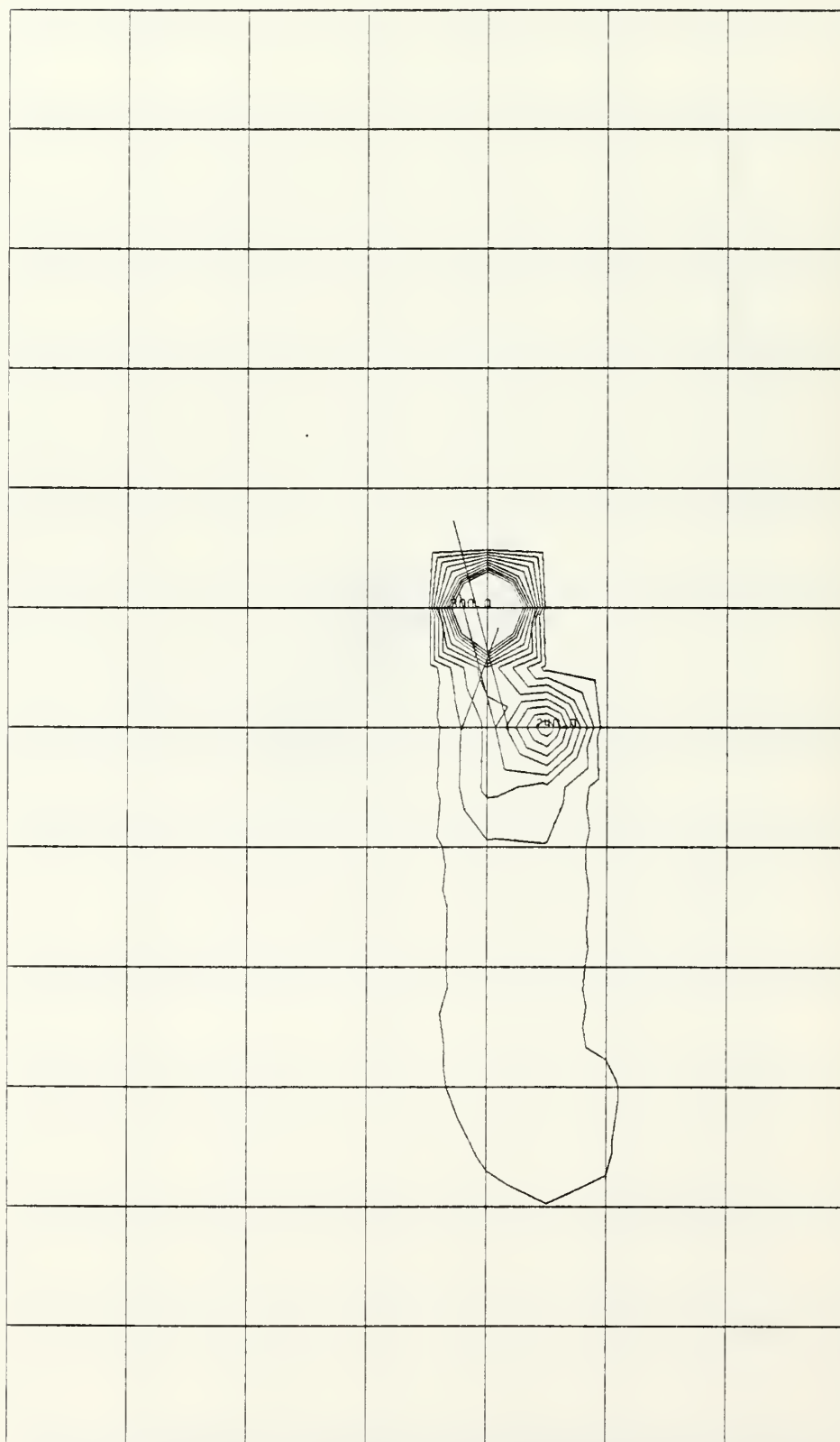




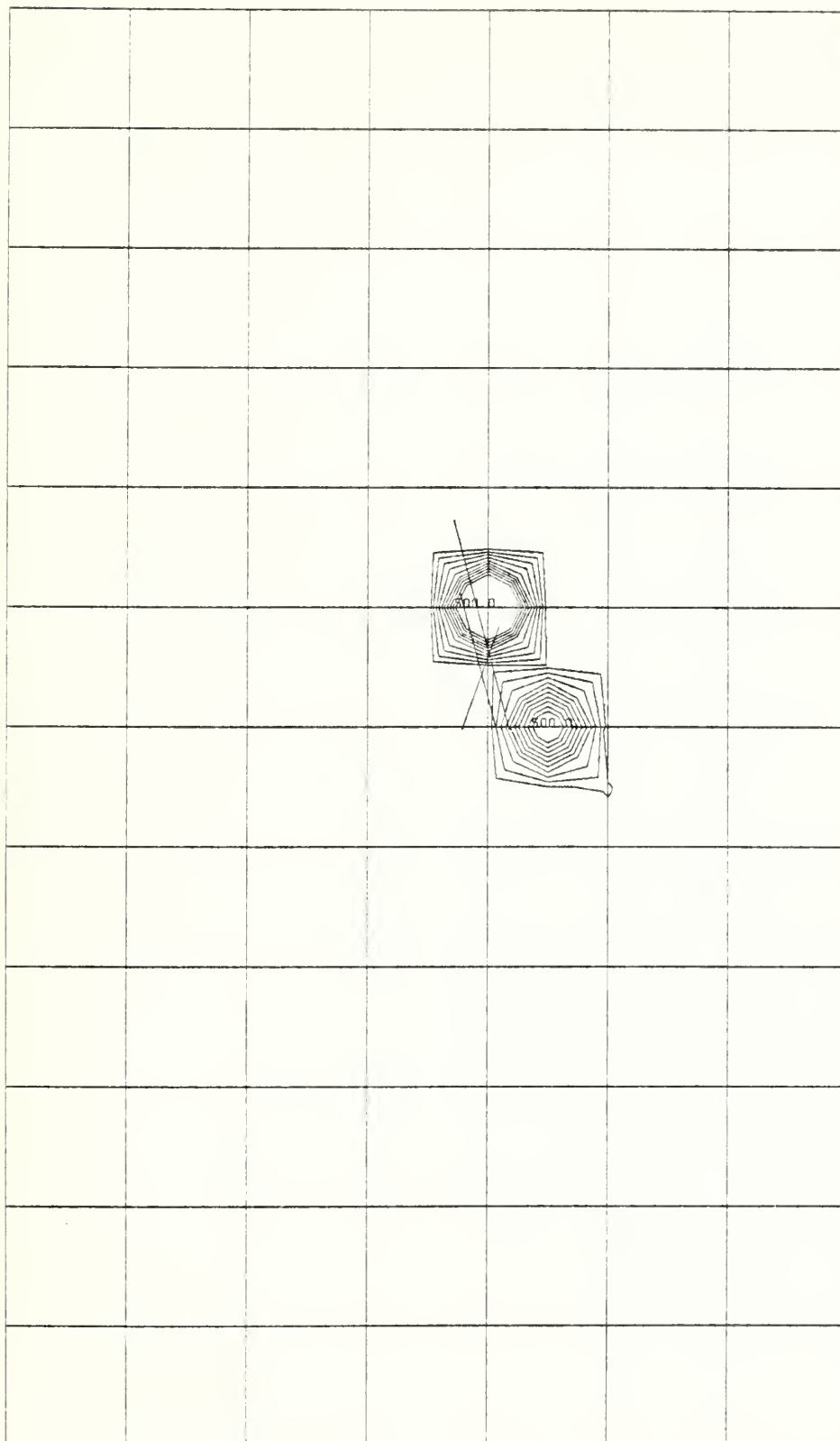
TOTAL PT CONCENTRATION PROFILE (2 AUG 1500-1600)  
INCREMENTED FROM 50.0  
(Scale = 50  $\mu\text{gm}/\text{m}^3$  per contour)



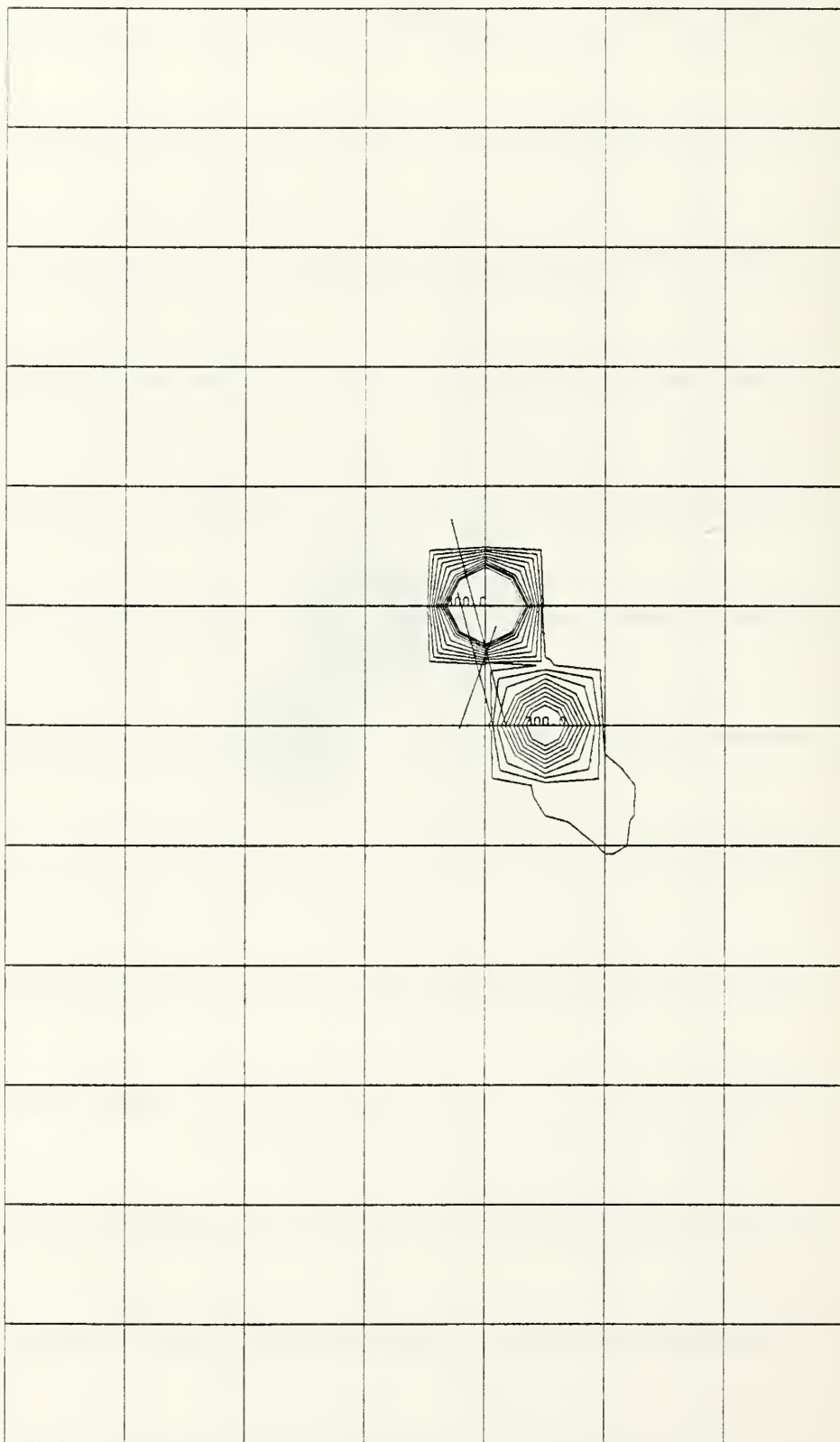
AIRCRAFT CO CONCENTRATION PROFILE (2 AUG 1515-1615)  
INCREMENTED FROM 50.0



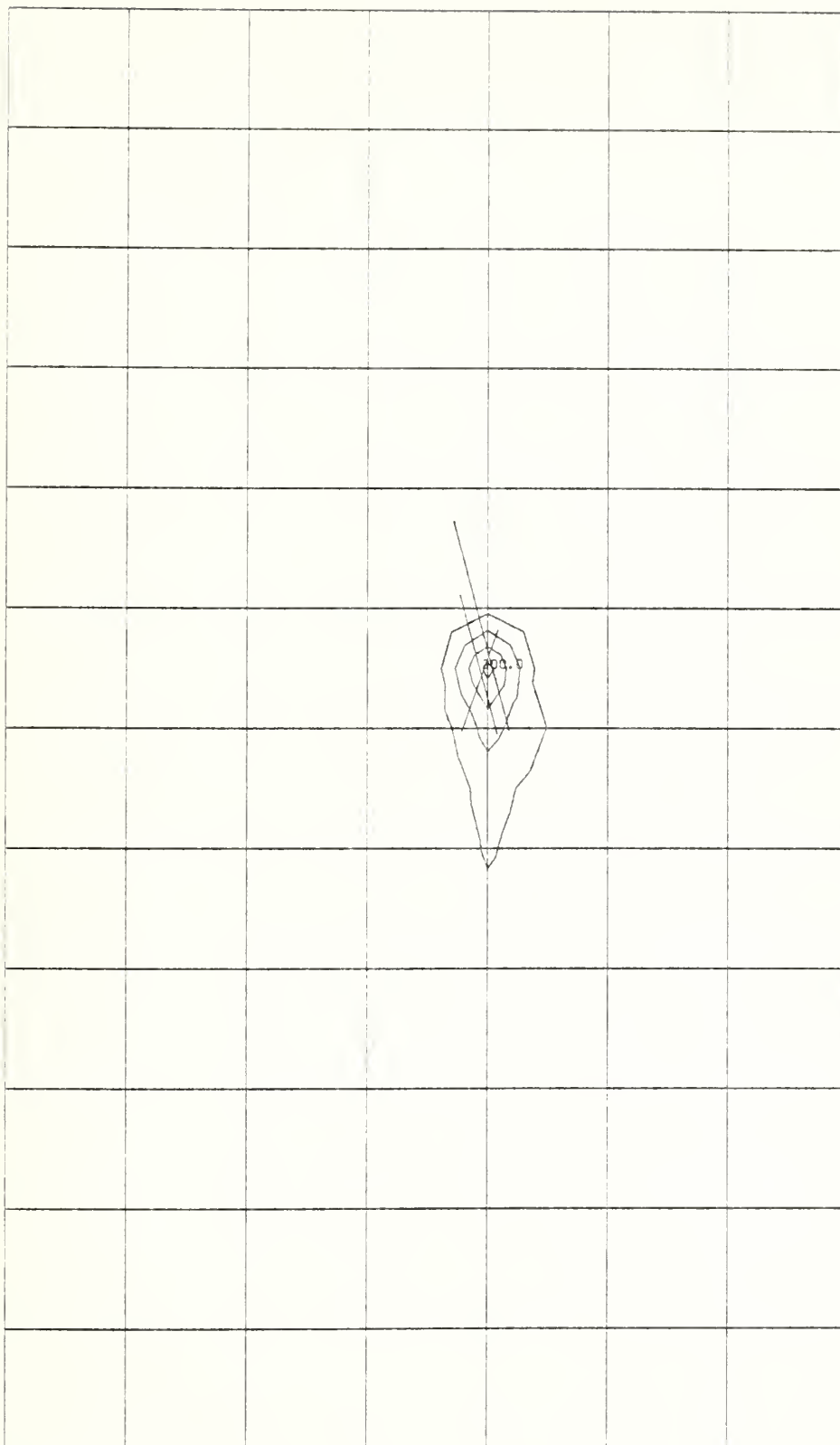
AIRCRAFT PT CONCENTRATION PROFILE (2 AUG 1515-1615)  
INCREMENTED FROM 30.0



AIRCRAFT CO CONCENTRATION PROFILE (3 AUG 1100-1200)  
INCREMENTED FROM 50.0

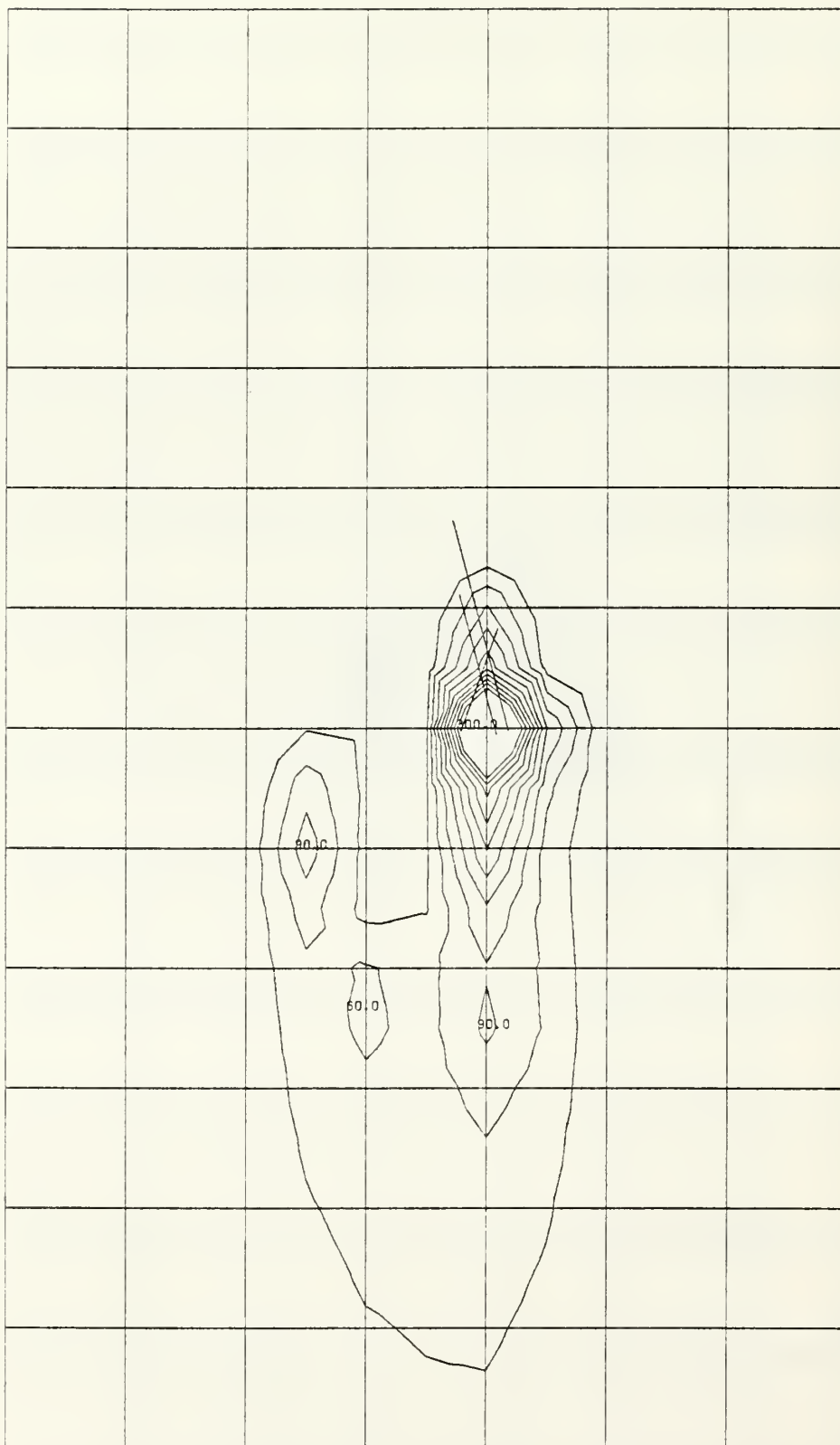


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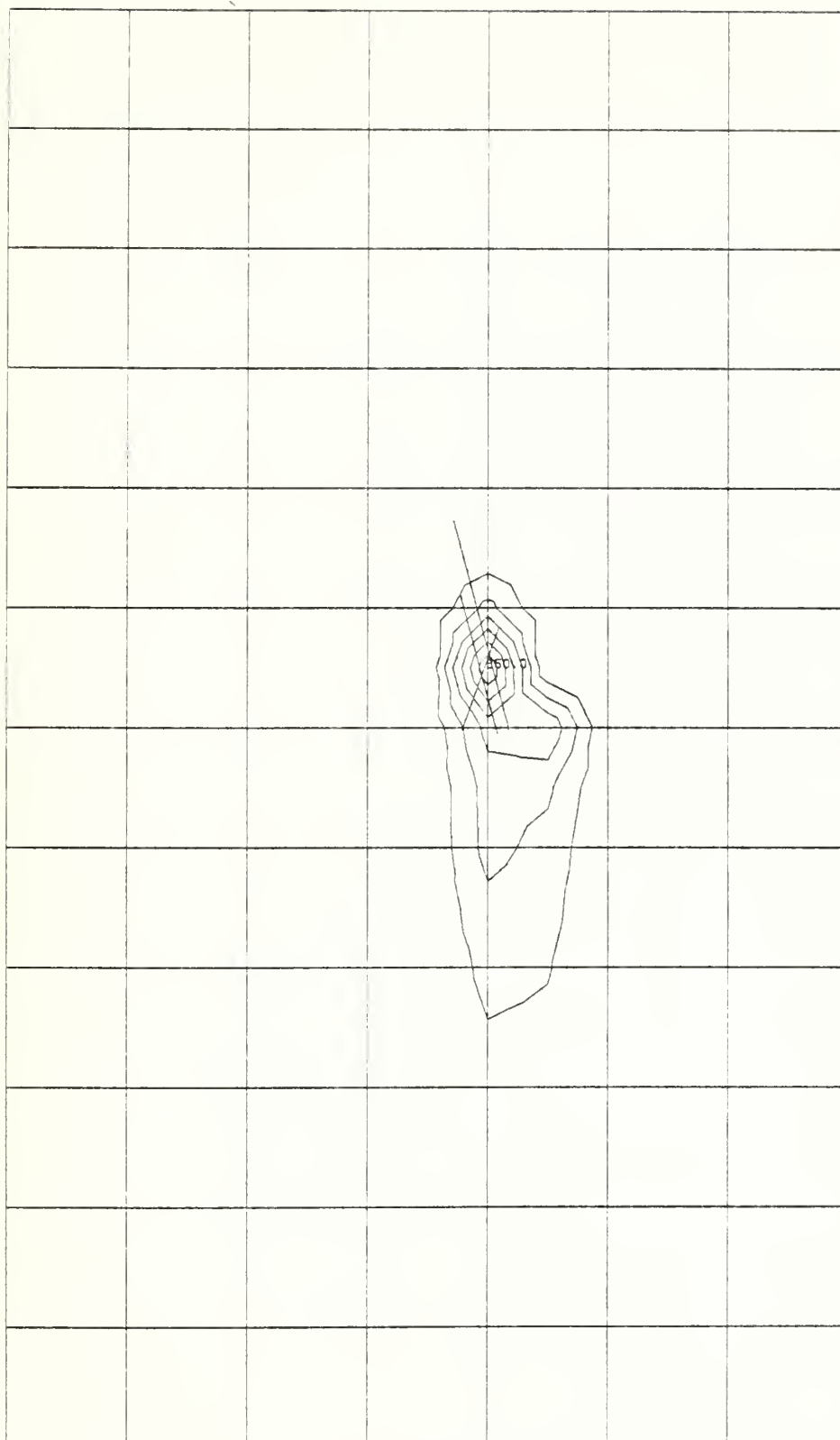


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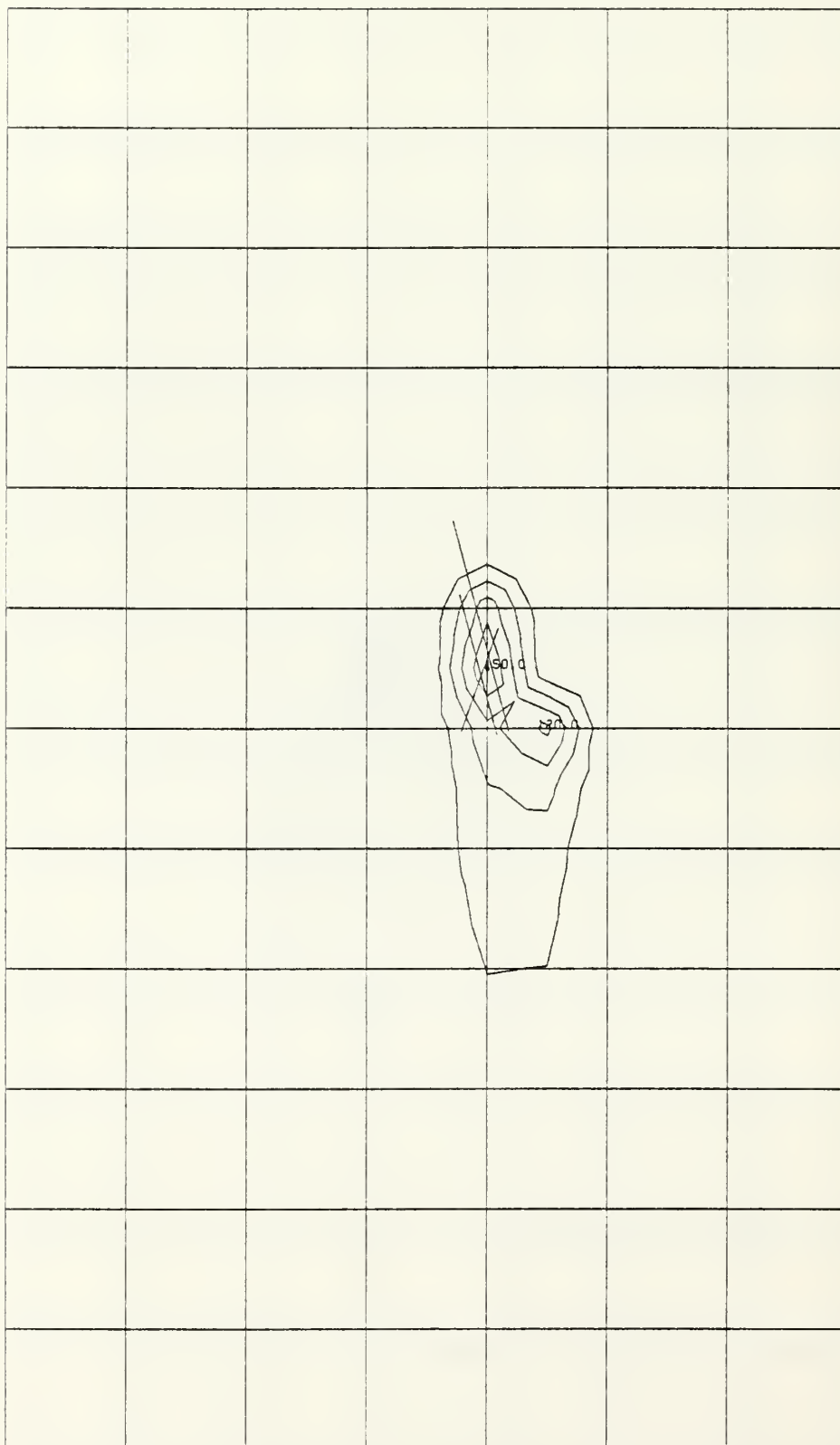




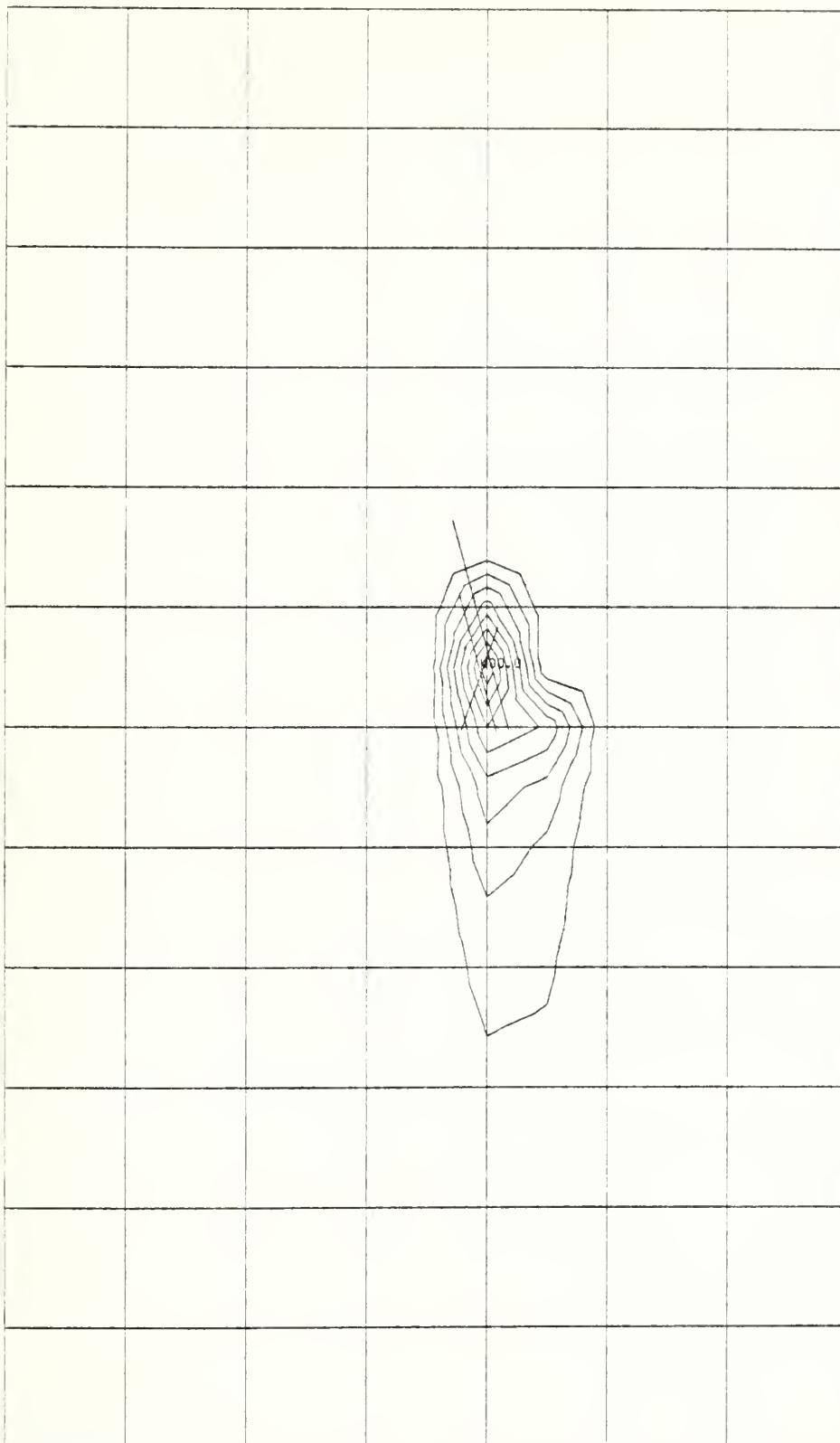
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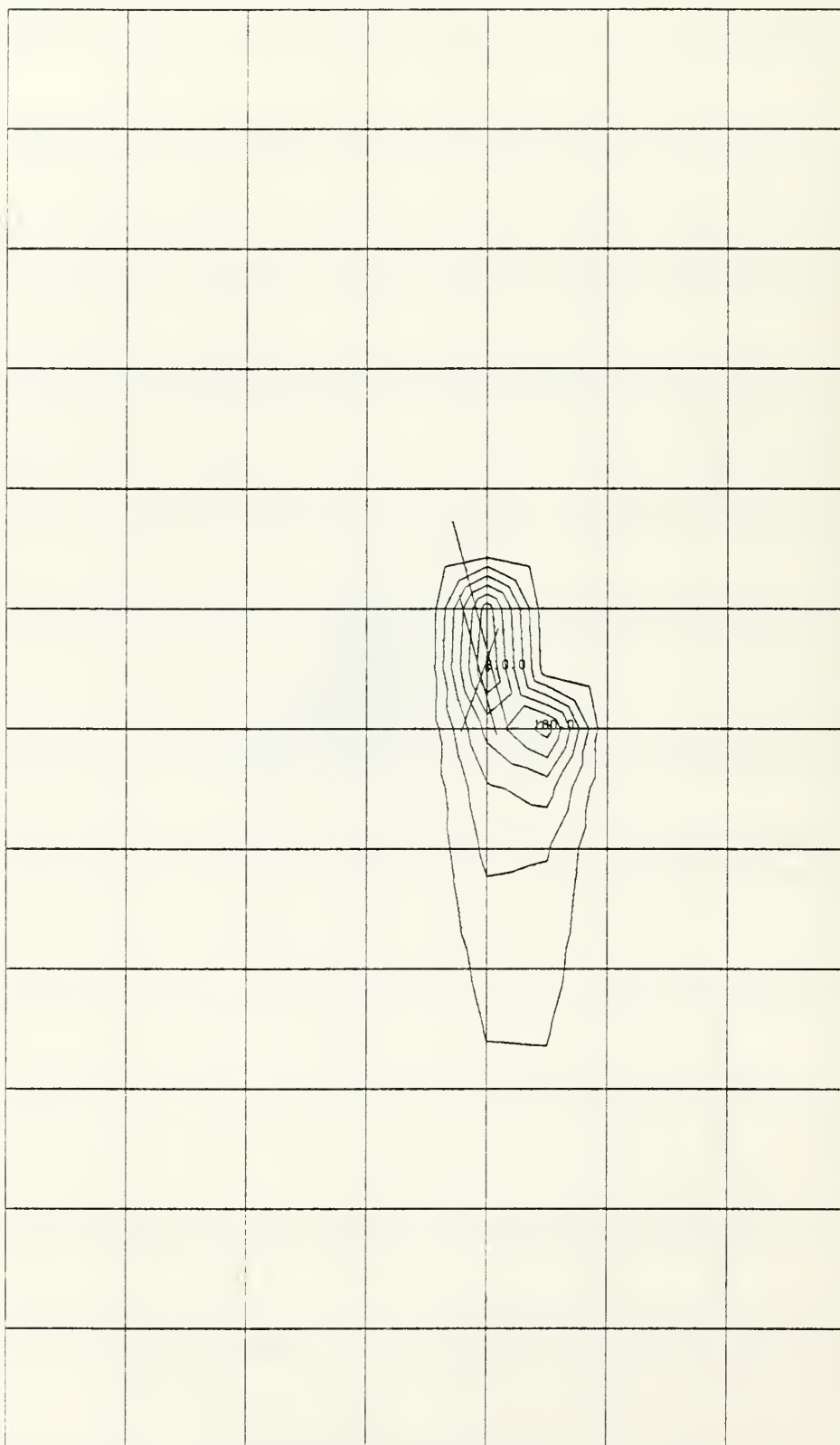
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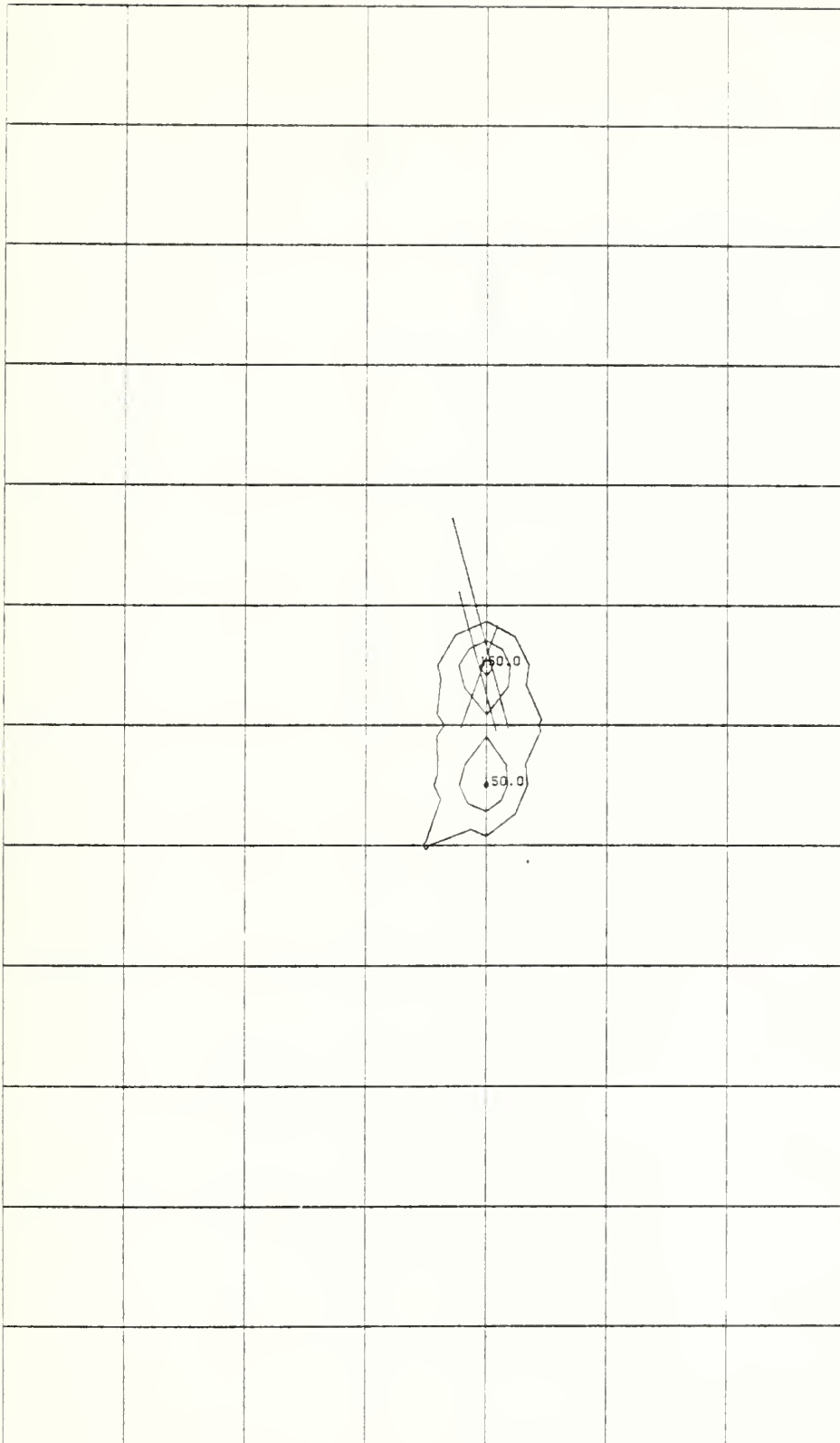
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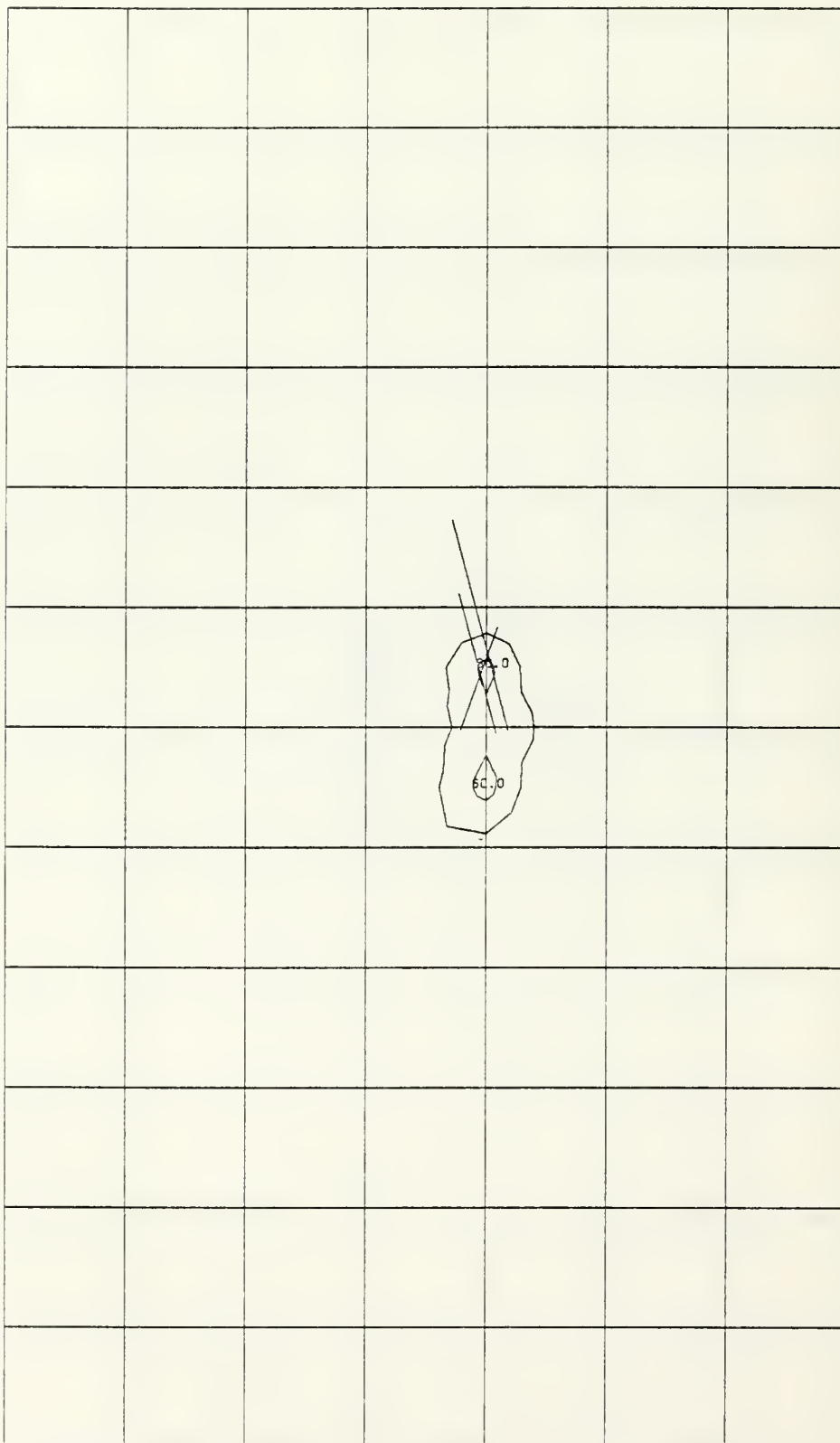


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